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GEOTECHNICAL EVALUATIONS OF
HALIÇ'S SEDIMENTARY LAYERS

by

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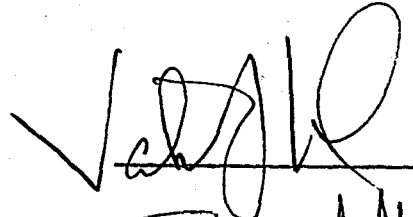
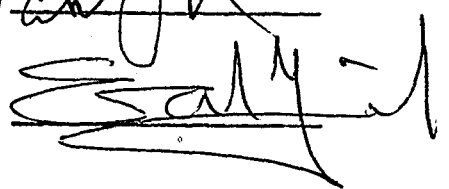

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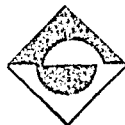
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Mahir KÖSELER

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ÖZET

Haliçteki yumuşak zemin tabakalarının varlığı, dip çamurunun taranması esnasında büyük boyutlarda geoteknik problemler ortaya çıkarır. Bu yüzden bu tabakaların taranması esnasında oluşabilecek kritik durumları önlemek için bazı geoteknik hesaplamalar yapmak zorunludur.

Bu tezde ilk olarak Haliç'in genel jeolojisi ve zemin durumları incelenir. Haliç boyunca I2 kesit halinde jeolojik oluşum(zemin durumu) verilir. Ayrıca bu tabakalarla ilgili geoteknik özellikler verilir. Haliç ve çevresindeki çevre problemleri ve Haliç'in taranması durumu araştırılır. Haliç'teki tabakaların çok yumuşak ve zayıf olmasından dolayı, kıyıların stabilitesi taranma yapılmadan önce araştırılması gerekir. Bu sebeple şev stabilitesi hakkında kısa bilgi ve bununla ilgili computer program(KÖSELER-I) geliştirildi.

Sonuç olarak, bazı jeolojik ve geoteknik sonuçlar ve taranma esnasında ve öncesinde oluşabilecek kritik durumları önlemek için neler yapabiliriz hakkında bazı tavsiyelerde bulunulacaktır.

ABSTRACT

GEO TECHNICAL EVALUATIONS OF HALIÇ'a SEDIMENTARY LAYERS

The presence of soft layers in Haliç create a great deal of geotechnical problems during the dredging of Haliç. It is necessary to make geotechnical evaluations to prevent critical situations during dredging.

The general geology and soil conditions in the area are studied. Geological formation along Haliç is given by geological cross-sections. Geotechnical properties of these layers are documented. The environmental problems in the vicinity of Haliç and dredging of Haliç are investigated. Since the layers (bottom sludge and underlying clay formation) are very soft and weak, stability of the shores should be considered before dredging. So stability of slopes is studied and the computer program for slope stability (KÖSELER-I) are given.

Some geological and geotechnical conclusions and recommendations such as what can we do to prevent critical situations that may arise before dredging and during dredging are given.

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CHAPTER 1

INTRODUCTION

Geotechnical problems ,having serious effects on people and buildings,generally require alarge amount of investment and have to be handled urgently. On the other hand,the nature of the problems varies depending on the type of the sources and environmental conditions,and that variations mostly makes necessary to study geological study and the geotechnical properties of the site.

Generally,environmental problems are to be handled and solved together with geoteehanical problem.In fact,each geotechnical problem at the inhabited sites,has a tendency to be an environmental problem. The outcomes of geotechnical problems such as erosion,slope stability and dredging have an importance for people.The large amount of investment and urgency is necessary for the solution of such kind of problem

Haliç is 7.5 kilometers long natural inlet of the Bosphorous strait.The maximum width is 900 meters at the mounth,which is between Sarayburnu and Tophane Mosque,and the minimum width is 150 meters on the upstream side at the outlet of Alibey and Kağıthane Creeks.Its surface area is a total of 2.6 million square meters.Maximum depth in Haliç is 36 meters and it shallows down to a few meters deep near Kağıthane Cre

Haliç has been a center of attraction and recreation in former times.It has a very significant historical back ground, and is surrounded by buildings dating from Ottoman and Roman days.



FIG. I.I General view from Azapkapı

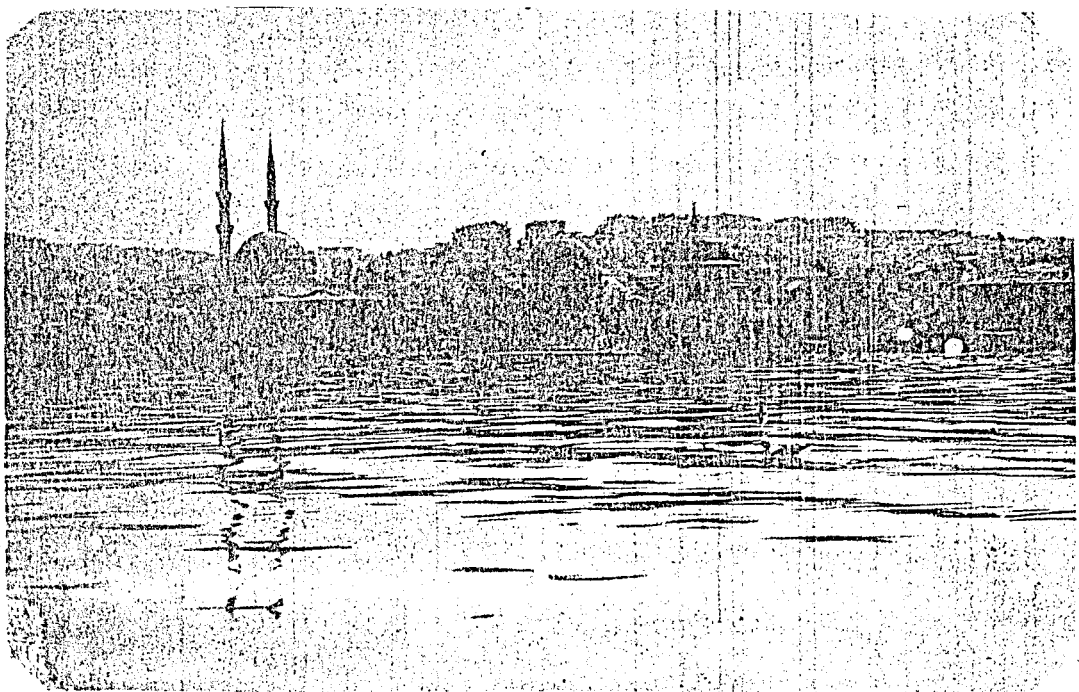


FIG.I.2 Historical view from Eyüp

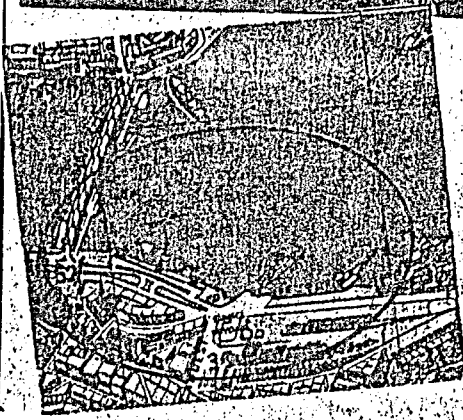
Over the years, industrial and domestic wastes, erosion, uncontrolled fill and garbage, shipyard wastes and sewage have polluted Haliç. So it has developed into an unbearable and unhealthy condition. Additionally, soft layers encountered in the vicinity of Haliç create special geotechnical problems to the area.

The soil conditions in Haliç will cause some geotechnical problems during dredging. Therefore, prior to any construction, development, alteration of conditions and dredging the existing soil conditions and soil properties should be determined. In chapter II, the general geology of the area is documented. All previous borings drilled in the area are given. The soil conditions are determined based on the available information. The average soil properties are estimated based on many measurements reported previously.

In chapter III, environmental problems of Haliç and water pollution is summarized. Also volume and location of previous dredgings and types are given.

The presence of soft fills brings a great deal of geotechnical problems to the area. The considerable amount of increase in thickness of this formation towards the sea causes stability problems, (Fig. I.3, Fig. I.4). The geotechnical conditions in the vicinity of Haliç make necessary for a preliminary study of slopes before and during dredging. In chapter 4, stability of slopes are studied. Also computer program for slope stability (KÖSELER-I) is developed. It makes easier to solve and compute problems.

Based on the findings and the results of this study recommendations for future construction and to prevent critical situations during dredging are summarized in chapter 5.



Halic'in, planda gösterildiği gibi, özellikle Eminönü ile Sirkeci arasındaki bölümden kayma daha belirgin şekilde oluyor. Sirkeci'deki arabalı vapur iskelelerinden birinde kayma yüzünden büyük çatlamlar meydana geldi. İstanbul Üniversitesi Yer Bilimleri Fakültesi öğretim üyesi Prof. Dr. Mehmet Akartuna, kullanılmaz duruma gelen iskelede incelemeler yaptı (yukarda). (Ali BOSTANCI)

Halic kıyıları denize kayıyor

Piza kulesi
gibi
binalar



Halic'in Eminönü kıyısında bulunan ve "Yağ iskelesi" olarak bilinen kesimdeki 100'e yakın binanın denize kaydığı bildirildi. Duvarlarında derin çatlaklar meydana gelen ve denize eğilerek Piza Kulesini andıran binalarda oturulamayacağı ileri sürüldü.

Yağ iskelesinin denize kaydığı tespit edildi

HALIÇ YUTUYOR!

Fig.1.3 , 1.4 News from Turkish Newspapers about sliding of Halic shores. (Milliyet, 1981 and Hürriyet, 1980)

CHAPTER II

GEOLOGY AND SOIL CONDITIONS

2 . 1 INTRODUCTION

In following chapters, the environmental problems and the relations with geotechnical problems in the vicinity of Haliç will be explained. In order to find reasonable solutions of the stability problems and to make reliable investments, geological conditions should be known. In this chapter geological conditions and geotechnical considerations in the vicinity of Haliç will be given. The extend of soil layering along Haliç will be given. Also geotechnical properties of each soil layer will be summarized.

2 . 2 GEOLOGY









The geology in the vicinity of Haliç has been studied by many investigators. One of them, Penck (1919), was first to recognize the graywackes, "Thrace series", as the oldest formations in the area. They belong to the Lower Devonian to Upper Devonian periods of Paleozoic era. After that Packelman (1925) changed that as upper Devonian. But the existence of various litological and paleontological zones in the Thrace series was indicated by later research. They belonged to the Lower Carboniferous (Upper Paleozoic) period of the same era.

Recently, a complete geological map of Haliç and its vicinity was given by Sayer (1976), Figure 2.1. It is seen from this figure that the oldest rocks in the area, in Upper Paleozoic (Lower Carboniferous) age and consist of shales and graywackes.

LÇEK SCALE

0 1000 1500 2000 m.

A RETLER
e g e n d

-  Fay
Fault
-  Doğrultu ve eğim
Strike and dip
-  Alüvyon ve dolgu
Alluvium and fill
-  Mactra'lı kalker
Mactra limestone
-  Kil, marn
Clays and marls
-  Kum, çakıl
Sands and gravels
-  Kumtaşı, kil, marn
Sandstones, clays, marls
-  Kalker, Grovak, Killişist
Limestone, Gryw., Shales
-  Killişist, Grovak
Shales and greywackes
-  Silisli şist
Silicified shales
-  Andezit, Diabaz
Andesite, Diabase

Bakarköy Formasyonu Bakarköy Formation	SARMASIEN Sarmatian
Güngören Formasyonu Güngören Formation	
Çukurçeşme Formasyonu Çukurçeşme Formation	TORTONIEN Tortonian
Çamurluhan Formasyonu Çamurluhan Formation	
Cebeciköy Kalk., Gümüş D.Fm. Cebeciköy Lmst., Gümüş D.Fm.	DİNANSIEN Dinansian
Trakya Formasyonu Thrace Formation	
Battalimanı Formasyonu Battalimanı Formation	

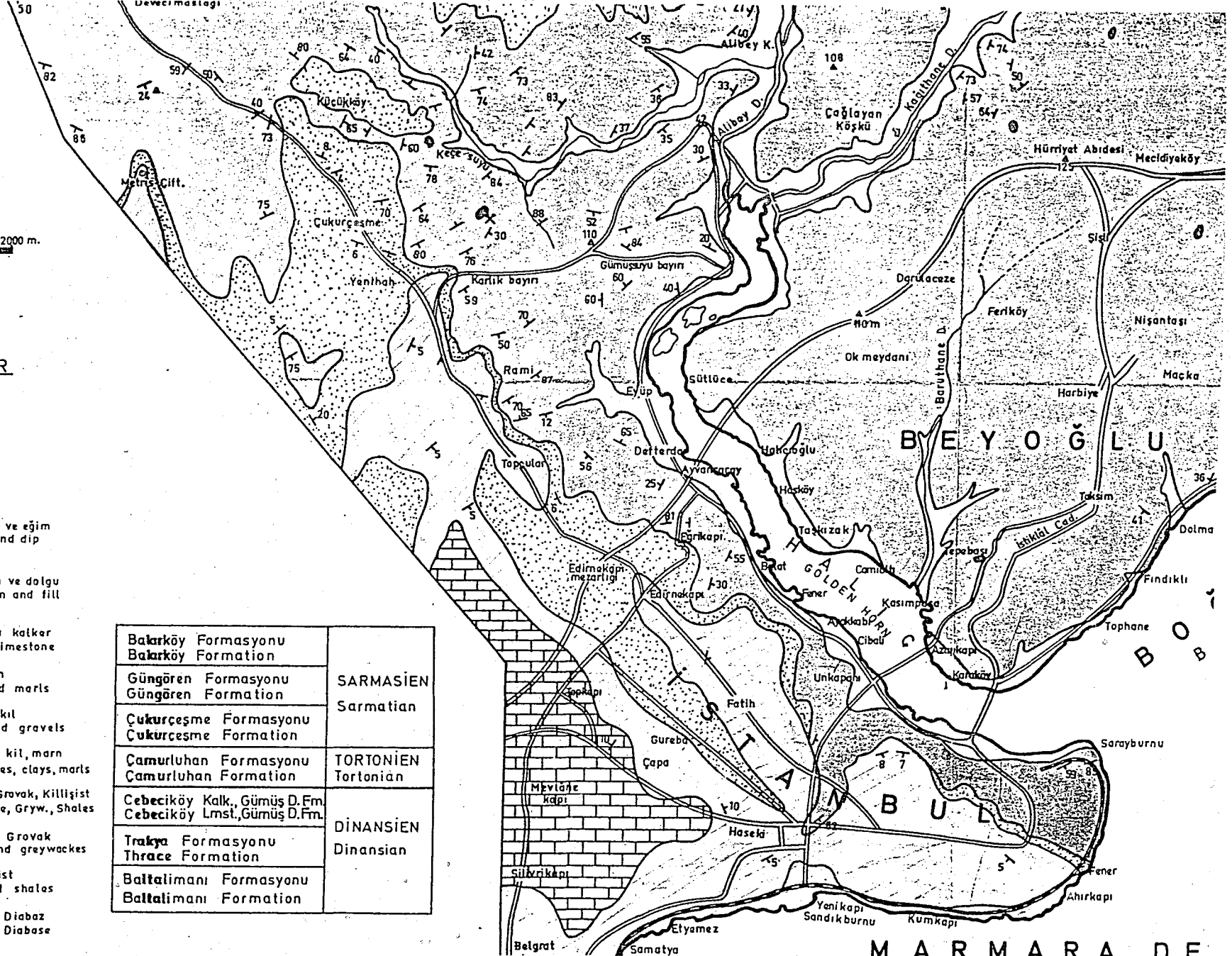


Fig. 2.1 Geological map of Halic and its vicinity (Sayar, 1976)

7

At the southern part of Haliç on the top of the Paleozoic formations the middle and upper Miocene formations of sand and gravels, clays and marls matrix limestones are encountered. Along the shore lines and below the water of Haliç and Creeks however, the quaternary alluviums are found.

A . UPPER PALEOZOIC (Lower carboniferous)

Most of the information concerning this information is obtained from comparatively shallow borings and excavations a few meters deeps at various places in the Istanbul Area. In the detailed studied of recent years , the paleozoic formations in the vicinity of Haliç are classified.

Baltalimanı Formation :

This formation is observed at both sides of Northern part of the Bosphorus and around İçerenköy. It consists of black silicified and intensively folded shales.

Trakya Formation :

Found in a large part of the area and consist of graywackes and shales. Some parts are decomposed by atmospheric effects taking on a green - grey or yellow-brown colour. The alternation of layers of coarse and fine grains shows the sedimentary structures such as cross-bedding, slumping etc.

Cebeciköy Limestone:

This formation found on top of Trakya Formation covers an area of about 1,000,000 square meters around Cebeciköy. It consists of crystallized massive limestones and dolomatic limestones containing numerous calcite veins.

Gümüşdere Formation :

It is observed that near Cebeciköy Formation and consist of shales, silicified shales and tuff.

B . MIDDLE AND UPPER MIOCENE

The formations belonging to the middle and upper Miocene are not common in the vicinity of Haliç. But middle Miocene (Tortonien) formation is encountered in a limited area near Çamurhan, 7 to 8 kilometers from Eyüp. The formation consists of grey coloured marls, sands, yellow coloured clays, micaons sand stones, and grenish sandy clays. The thickness of the formations was found to be 30 to 40 meters.

To the south and south west of Haliç the Paleozoic base is overlain by a thick upper Miocene (Sarmacien) formation. It is thickness reaches 150 meters at places. Upper Miocene was divided into three units by Sayar (1976). Each unit has the name of the area where the characteristics of the unit is observed.

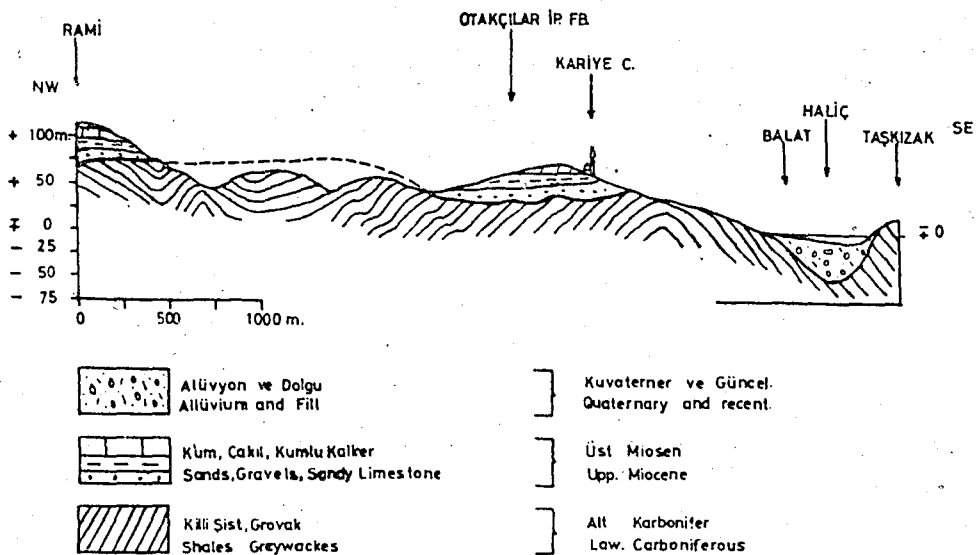


Fig 2.2 Geological cross-section between Rami-Taşkızak(Sayar, 1976)

1) Sand and gravel beds of Çukurçeşme formation consists of fine sand bands and lenses.

2) Marl and green clay beds of Güngören formation are generally found on top of the sand and gravel beds. At the western part of the walled city marl and clay bed are overlain by limestone beds. Güngören formation consist of vertebrate and mollusc fossils.

3) Limestone beds of Bakırköy formation may easily be recognized by the variety of maetra species they contain. Thick beds of limestone exist in the Bakırköy area.

C. ^U QUATERNARY AND CURRENT SEDIMENTS (Recent) :

The youngest geological formations in the area are alliviums in the beds of creeks and sediments at the shore of Haliç and the bottom of the sea. Artificial fills along the shore will be classified in this group also. These may be classified according to their characteristics as follows:

a) River Alliviums (Flood-plain deposits):

They are observed in the bottoms of the valleys of Alibey and Kagithane Creeks. They are commonly consist of continuous layers of sand and clay laid down during the high-water season.

b) Marine Deposits :

At the shores and the bottom of Haliç on the paleozoic base a silty-clay layer containing marine organism is found. The extent of these sediments might be overlooked since the coast line has been greatly changed over the years. The thickness of this layer varies from 1 to 12 meters at the shores and 40 to 50 meters at the bottom of Haliç.

c) Bottom Sludge (Recent) :

Borings carried out in the middle part of Haliç showed the existence of a mud layer. The thickness of the bottom sludge decreases near the shores. It is formed by sedimentation of eroded materials and pollutant in the water. It is also explained in chapter III.

d) Artificial fills (Recent):

They are found at the shores and around Haliç just below the ground level. They consist of stones, bricks, pieces of concrete, wood, rubble, etc. The thickness of that decreases away from the shore line. Between Galata and Unkapanı Bridges, the thickness of artificial fills are 30 - 40 meters.

2 . 3 SOIL CONDITIONS

There have been many geotechnical investigations related to various constructions at the vicinity of Haliç. The locations of some of the boreholes drilled for the determination of soil condition in these investigations are shown in Fig. 2. and table 2.I

These boreholes are shown in Appendix A.

Also a list of these borings with their references are given in table 2.I. 12 typical geotechnical cross-sections, along Haliç, determined from the results of these borings are given^{as} Figures in Appendix.

TABLE 2.1

LIST OF GEOTECHNICAL BORINGS LOCATED IN THE VICINITY
OF HALIÇ

Boring Group No	LOCATION	REFERENCE
I	Silahtaraga Power Plant	Peynircioğlu, 1975
2	Istanbul Mill , Sütluçe	Peynircioğlu, 1965
3	Golden Horn Bridge	S. Maden, 1975
4	Istanbul Sewage Project	Temel Araştırma, 1982
5	Istanbul Sewage Project	CAMP-TEK-SER-1974
6	Taşkızak Shipyard, Hasköy	Special Report
7	Camialtı Shipyard, Kasımpaşa	Special report
8	Haliç Shipyard, Azapkapı	Special report
9	Draper Market, Unkapanı	Sayar, 1962
10	Social Security Department Complex, Unkapanı	Peynircioğlu, 1973
11	Chamber of Commerce House, Eminönü	Peynircioğlu, 1973
12	Preliminary Subway Study	Sayar, 1962
13	Preliminary Subway Study (1978)	General Dir. Of Highway
14	Silahtaraga Steel Plant, Alibeyköy	Special Report

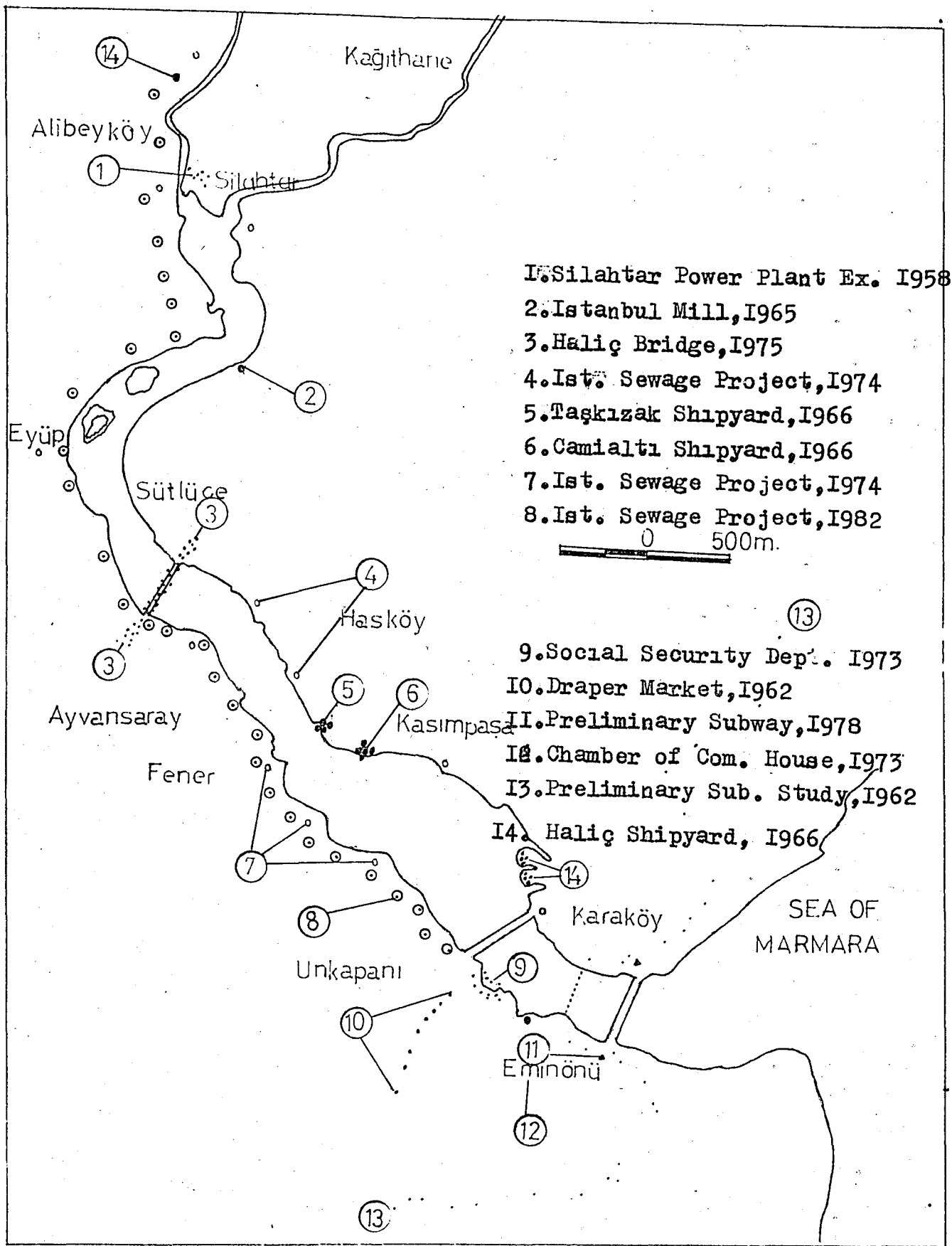


Fig.2.3 Geotechnical Borings Located In
The vicinity of Haliç

A. BEDROCK FORMATION

It is seen from cross-sections the depth of the bedrock formation varies considerably at various locations and the dipping of the bedrock surface towards the sea varies between 20 and 45 degrees. This steep slope is the main cause of lateral movements across the shore.

The graywackes and shales contain local fault zones with various strike planes and dip angles. The layers which are close to the surface are highly weathered and fractured. The colour of the weathered parts are yellow and brown.

The thickness of the weathered zone of the graywackes and shales is not homogenous, but varies from place to place. The thickness of the weathered zone of the graywacke, in Eminönü, 30 meters. (Sayar, 1975) It decreases along upper part of Haliç. As a result, the graywacke formation is mainly fissured and upper part is decomposed.

The engineering properties of the graywackes and shales have been investigated by many researchers. The engineering properties and unconfined compressive strengths of graywacke samples, from two different locations, are given table 2.2, (Toğrol, 1975).

Table 2.4

STRENGTH TEST ON GRAYWACKE SAMPLES (Togrol, 1975)

	Zeyrek Under-ground Passage Construction	Test pit near Istanbul Technical Univers.	Zincirlikuyu Office Building Construction
Depth, m	4-6	0-2	6-10
γ_n , gr/cm ³	2.36-2.46	2.38-2.54	2.42-2.54
γ_s , gr/cm ³	2.74	2.78-2.82	2.78-2.80
w, %	7.3-8.3	2.31-8.05	5.92-7.23
n, %	0.175-0.185	0.142-0.170	0.142-0.195
e, %	0.212-0.227	0.166-0.205	0.170-0.242
γ_{dry} , gr/cm ³	2.23-2.26	2.32-2.40	2.26-2.40
s, %	98.5-100.0	32.5-100.0	83.5-97.6

γ_n , Natural Unit Weight

n, Porosity

γ_s , Unit Weight of solid particul.

e, Void Ratio

s, Degree of Saturation

w, Water Content

B . SEDIMENTARY LAYERS-QUATERNARY AND RECENT
ALLUVIUMS

I) Artificial fills:

The thickness of such fills decreases with increasing distance from the shore. Along Haliç shores, artificial fills vary in thickness from a few meters to almost 40 meters. The artificial fill contains gravels, sand, boulders, silt, shells, wooden pieces, concrete and all kind of city debris.

The existence of this uncontrolled fill is very important from various points:

i) The thickness of the fill increases towards the sea. Therefore, it causes uneven settlements for buildings constructed on top of the fill layer.

ii) The properties of this fill is not known and varies considerably from one point to another. The properties of some of them are given in table 2.5.

iii) The existence of this layer in land alter the grey silty clay properties due to consolidation of silty clay under the the weight of the fill.

Fig. 2.4 Borings taken from Haliç Shipyard (special report, 1966)

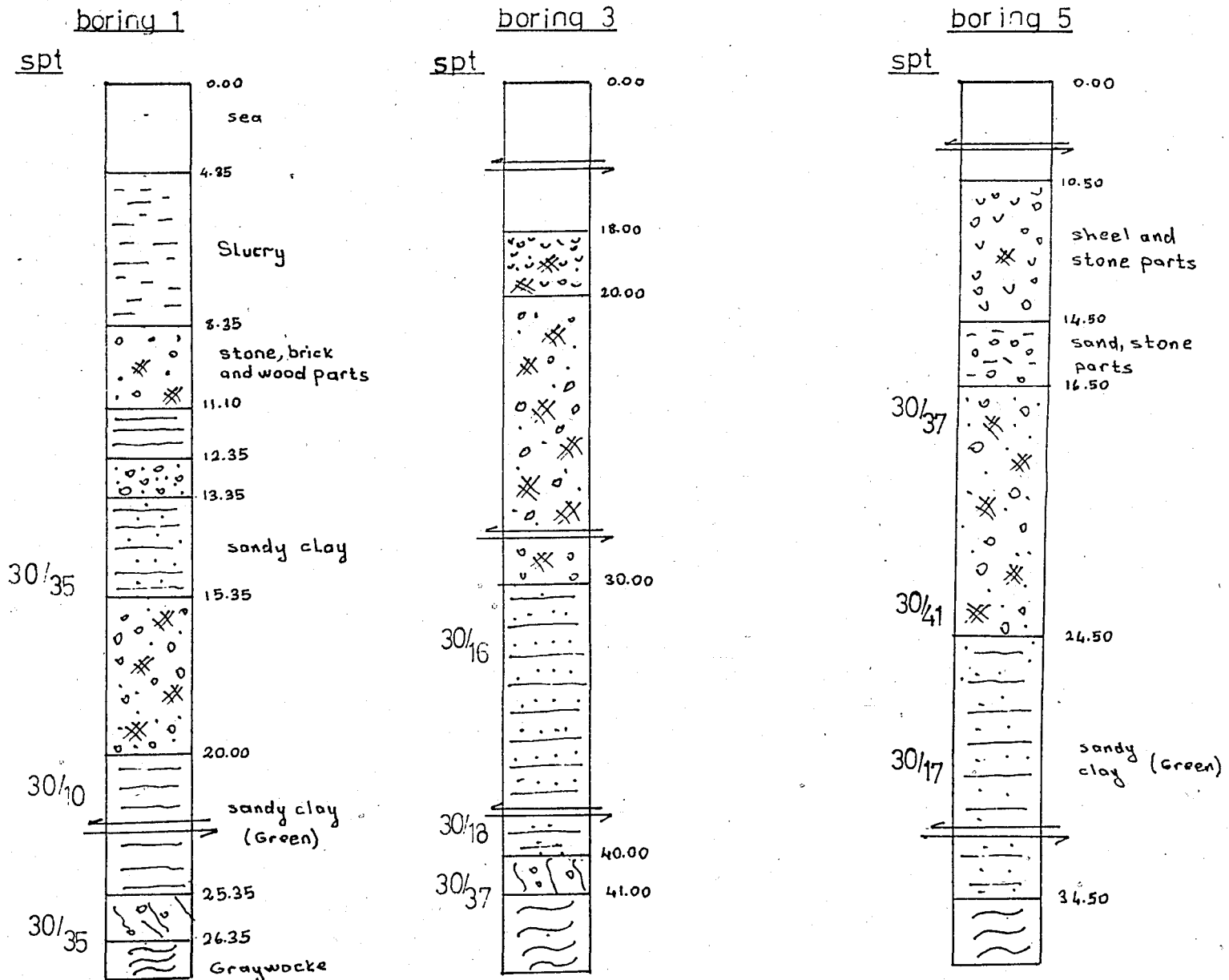


Fig.2.5 Borings taken from Taskızak Shipyard (special report, 1980)

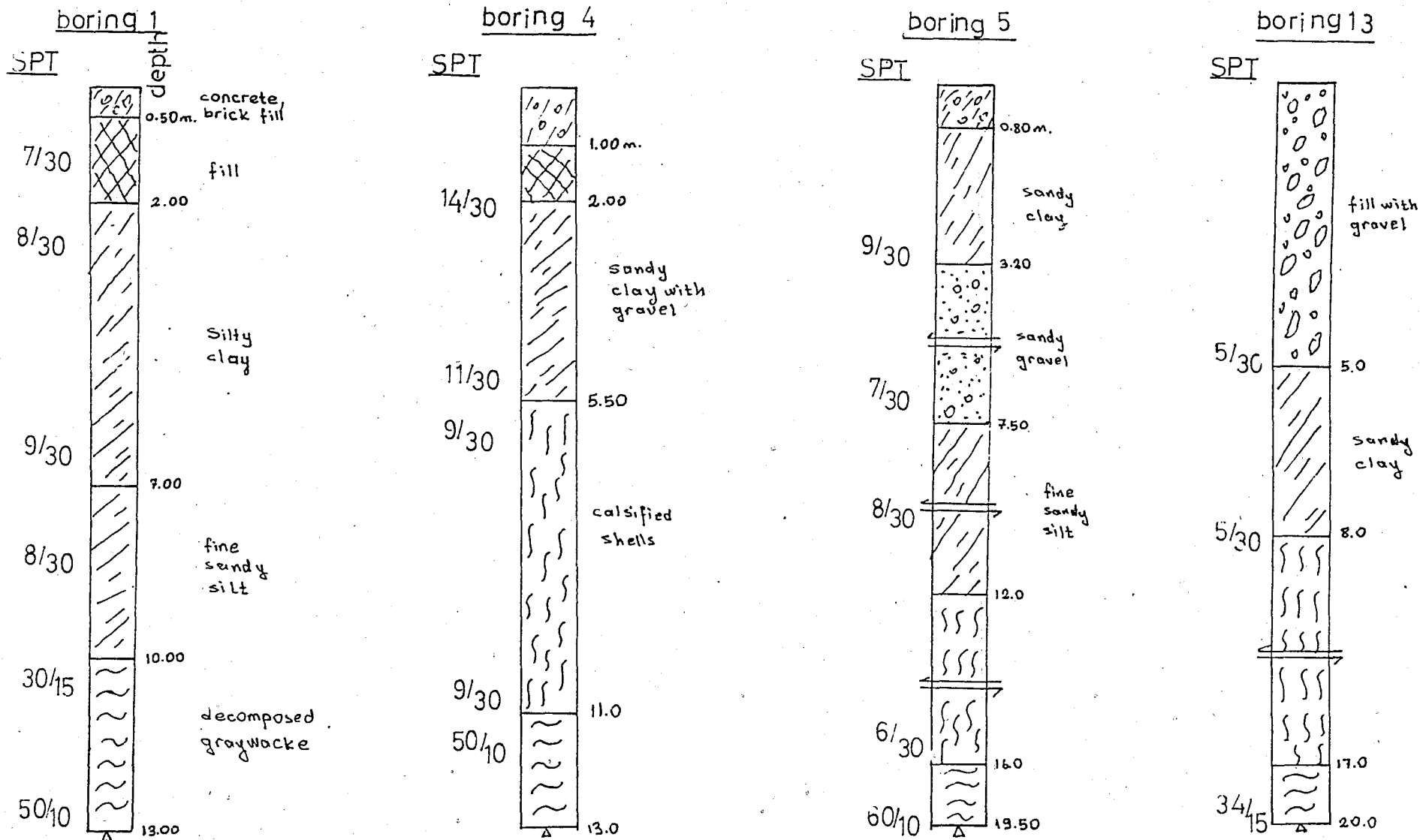


Table 2.7

LAB. REPORTS TAKEN FROM TAŞKIZAK SHIPYARD BORINGS

(Special Report, 1980)

	Boring No:1 (Depth 3m.)	Boring No:4 (Depth 3m.)	Boring No:5 (Depth 3m.)	Boring No:13 (Depth 3m.)
W_n (%)	21.4	18.4	21.3	22.0
W_l (%)	30.9	28.0	27.1	32.7
W_p (%)	19.0	15.00	19.6	22.3
I_p (%)	11.9	13.4	7.5	10.4
I_c (%)	0.85	0.74	0.77	1.03
ϕ_u (°)	12 (.)	7 (..)	-	27 (.)
c_u	0.60 (.)	0.30 (..)	-	0.20 (.)
W_n (%)	20.4 (.)	20 (.)	-	20.60 (.)
γ_n	1.97(.)	2.07(..)	-	1.97(.)

(.) Quick Shear Test

(..) Triaxial Test

2) Sedimentary Layers :

The sedimentary layers which are found under the artificial fill consists of sandy, clayey silts, contain large amount of organic matter and shells. The thickness of this layer varies from 6.0 meters, near Galata Bridge, up to 35.0 meters, near the Creek outlets. (Kumbasar and Ülker, 1975)

This formation contains organic matters in high percentage and the water content is around Liquid Limit.

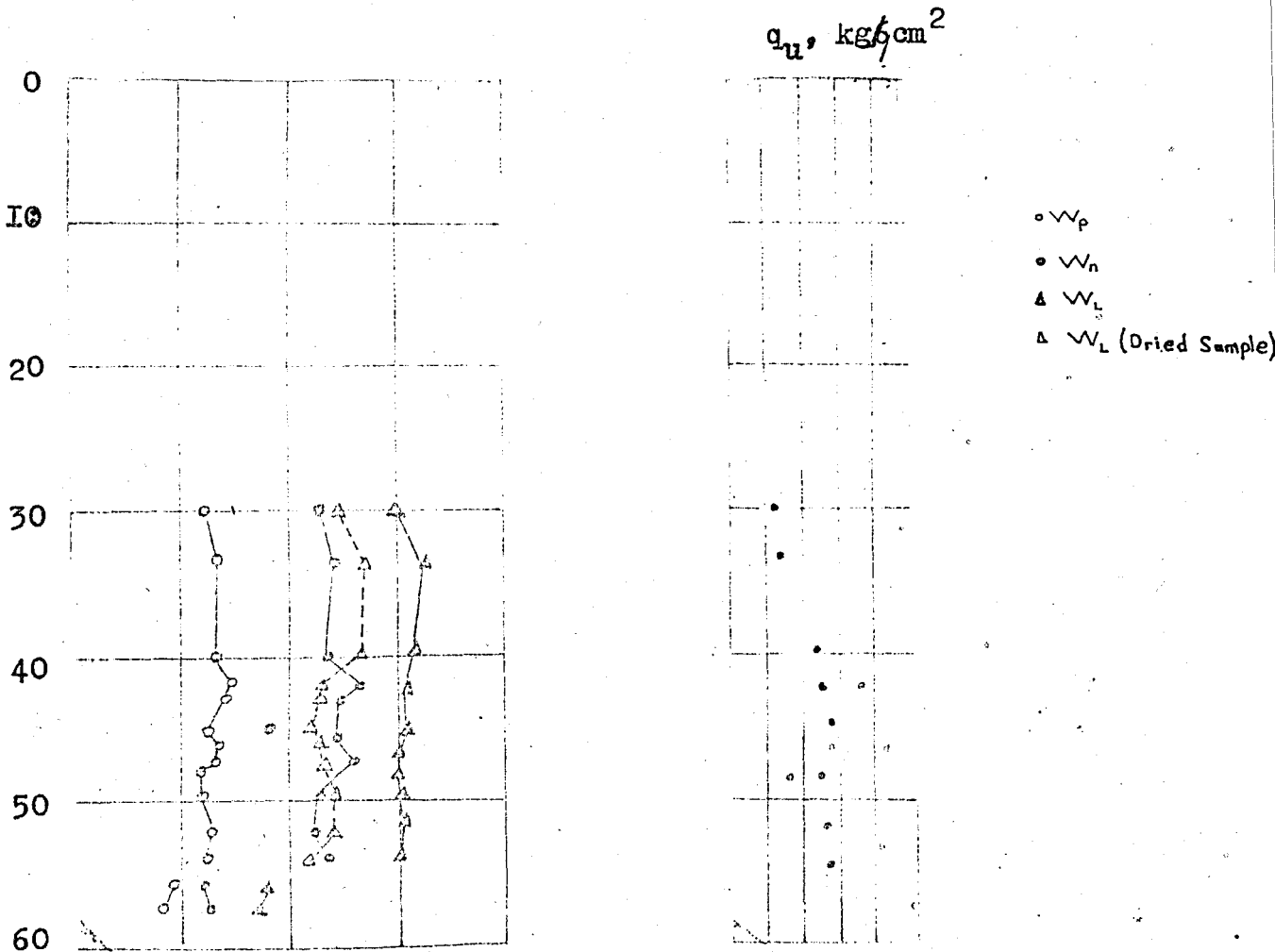


Fig Unkapanı, Properties of samples (Peynircioğlu, 1961)

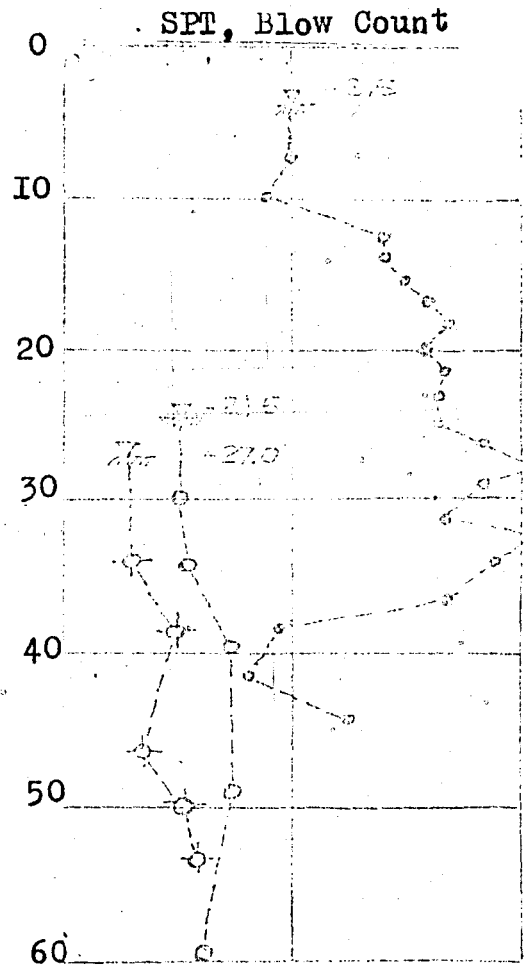
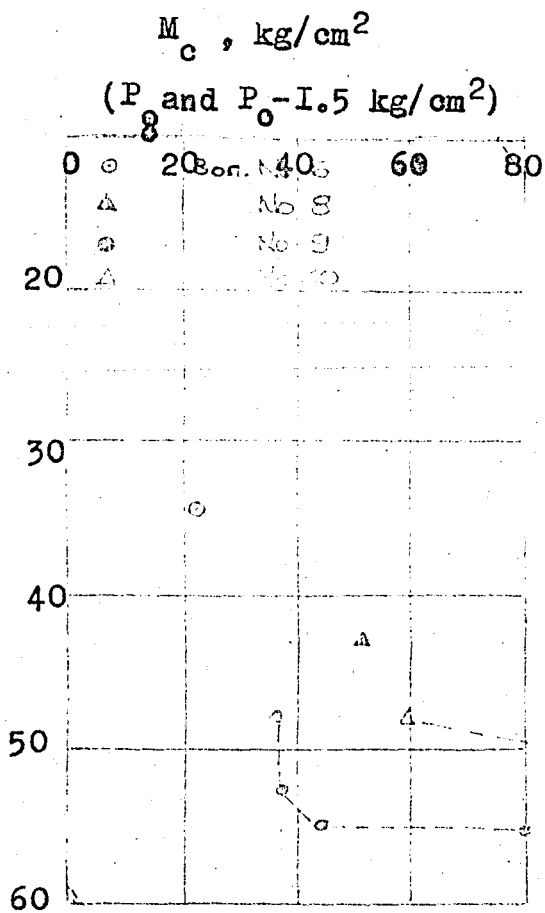


Fig. 2.6 Unkapanı, Properties of samples (Peynircioğlu, 1961)

Borings which were carried out at Silahtaraga Power Plant shows that Natural Water Content is nearly equal to liquid limit. (Table 2.8)

Table 2.8

Properties of samples taken from Silahtaraga
Power Plant, Togrol, 1967

Sample	Depth, m	W_n (%)	W_l (%)	c , kg/cm ²
3/6	9	82	96	0.10
3/10	17	79	94	0.10
4/1	5	88	91	0.13
9/7	20	67	83	0.10
9/6	18	73	77	0.10
7/8	18	61	61	0.10
7/6	14	60	60	0.10
1/4	8	92	56	0.05
7/5	12	61	55	0.12
9/3	12	46	51	0.20
7/1	4	55	45	0.45
1/1	2	39	38	0.40

Also, typical variation of test results on samples obtained from boring No: I at Hasköy Şark Değirmenleri site is given in Table 2.9 . (Toğrol, 1967)

No. of Samp.	Depth (m.)	W_L (%)	W_p (%)	I_p (%)	W_n (%)	q_u kg/cm ²
I	I3	68	34	34	54	0.7
2	I6	73	35	39	53	0.7
3	I8	72	35	32	53	0.7
4	20	75	37	40	60	0.4
5	22	72	35	35	61	0.6
6	24	77	35	42	62	0.3
7	26	76	36	40	61	0.7
8	28	70	36	34	55	0.8
9	30	63	32	31	50	0.8
IO	33	64	34	30	50	I.0

There are great amount of information related to the properties of sedimentary layer. These values from various sources are systematically compiled and represented in Table 2.10 .

Table 2.10

Average Properties of Samples

Obtained at Various Sites

Location	Depth (m.)	W_L (%)	W_P (%)	W_n (%)	q_u (kg/cm ²)	Reference
Eyüp, Hasköy, Süt lüce	0-60	60-80	30-40	50-75	0.15-1.	Peynirci, 1962
Sütlüce, Ist. Mill	-	85-90	40-45	60	0.2-0.3	Toğrol, 1975
Taşkızak Shipy.	12-35	50	27	50-66	0.64	Spe. Report
Unk., Old Found.	30-60	50-60	25	50	0.2-1.	Peynirci, 1961
Silahtarğa Power Plant	0-30	40-95	31	70	0.2-1.	Peynirci, 1961
3. Haliç Bridge	0-60	50-65	20-27	50-65	0.4-0.8	Dada, 1970
Extension of Power Plant	-	67	31	67	0.1-0.2	Toğrol, 1975
Hasköy Şark Mills	0-50	70-80	35	50-60	0.5-1.0	Peynirci, 1965

W_n , Natural Water Content

W_L , Liquid Limit

W_P , Plastic Limit

q_u , Unconfined Compressive Strength

The oedometer tests indicate that the clay is in a Normally Consolidated state. The sensitivity of the clay ranges between 3 and 6 which indicates that a large deformation of the clay can cause a decrease in the strength of the soil layer (Toğrol, 1975).

Also, Tests conducted on the samples obtained from Taşkızak Shipyard Borings are seen in table 2.II .

Table 2.II

Laboratory Test Results on Samples Obtained from Taşkızak Shipyard, (Special Report, 1980)

	Boring I (10.90)	Boring 4 (5.00m.)	Boring 5 (16.50m.)	Boring I3 (18.50m.)
W_n	15.0	21.5	22.9	20.7
W_L	32.3	34.3	37.0	34.2
W_p	21.7	18.8	18.6	17.6
I_p	10.6	15.5	18.4	16.6
I_c	1.63	0.83	0.77	0.81
γ_s	-	-	2.86	-
ϕ_u (.)	-	-	0	1
c_u (.)	-	-	0.50	0.68
γ_n (.)	-	-	2.06	2.1
ϕ_u (..)	-	-	21	27
c_u (..)	-	-	0.50	0.20
γ_n (..)	-	-	1.74	1.97

CHAPTER III

WATER POLLUTION AND DREDGING OF BOTTOM SLUDGE

3.1 WATER POLLUTION

The history of the water pollution in the vicinity of Haliç goes back to 15th century. The problem was erosion on the hills of Kağıthane and Alibeyköy Creeks and accumulation of eroded material on the bottom of Haliç. After 1950, industrial settlements have started in the vicinity of Haliç and environmental pollution has been observed.

The water body in Haliç is the mostly polluted part of vicinity. The rate of pollution increased by increase of population and industrial settlement and the problem developed into an unbearable and unhealthy conditions.

The main causes of the water pollution may be stated as follows:

I. Industrial Wastes: About hundred plants are giving their wastes directly to Haliç and Creeks. The water pollution due to industrial activities is equal to the pollution due to 3 million population, (Kor, 1975). Industrial wastes are polluting Haliç physically, chemically, and biologically. Values of basic parameters of water pollution at certain locations in Haliç are given in table 3.1 Karpuzcu (1974), Baykut (1946) and Kor (1963) .

Table 3.I

VALUES OF BASIC PARAMETERS ON WATER POLLUTION

Location	Water Depth	Turbidity (cm)	Temperature in April	Dissolved Oxygen (mgr/lt)	Heavy Metals		BOD (mgr/lt)
					Zn	Cd	
Kağıthane Creek	1.0	20	20	1.1	0.21-.73	0.0	-
Alibeyköy Creek	0.9	24	24	1.4	0.03-.11	0.0	10.0
Eyüp-Sütlüce	3.1	20	18	0.35	-	-	15.0
Haliç Bri.	3.3	22	18	0.30	0.05-.07	0.05	8.5
Atatürk Bridge	27.5	100	15	1.9	-	-	-
Galata Bridge	26.0	130	14	4.0	0.02	0.05	3.5

2. Domestic Wastes : The other important pollutant of the water in Haliç is domestic wastes of 600.000 population in the vicinity. Most of the districts in the vicinity are in lack of a proper sewage system. A new sewage system is designed by DAMOC (1971) and it is modified by CAMP-TEKSER (1975). The wastes which cannot be treated biologically must be treated previously in discharging plants. Haliç district has the third priority in the construction schedule of the project. Therefore, the water pollution by domestic wastes will continue for a period of time, (Fig. 3.I) .

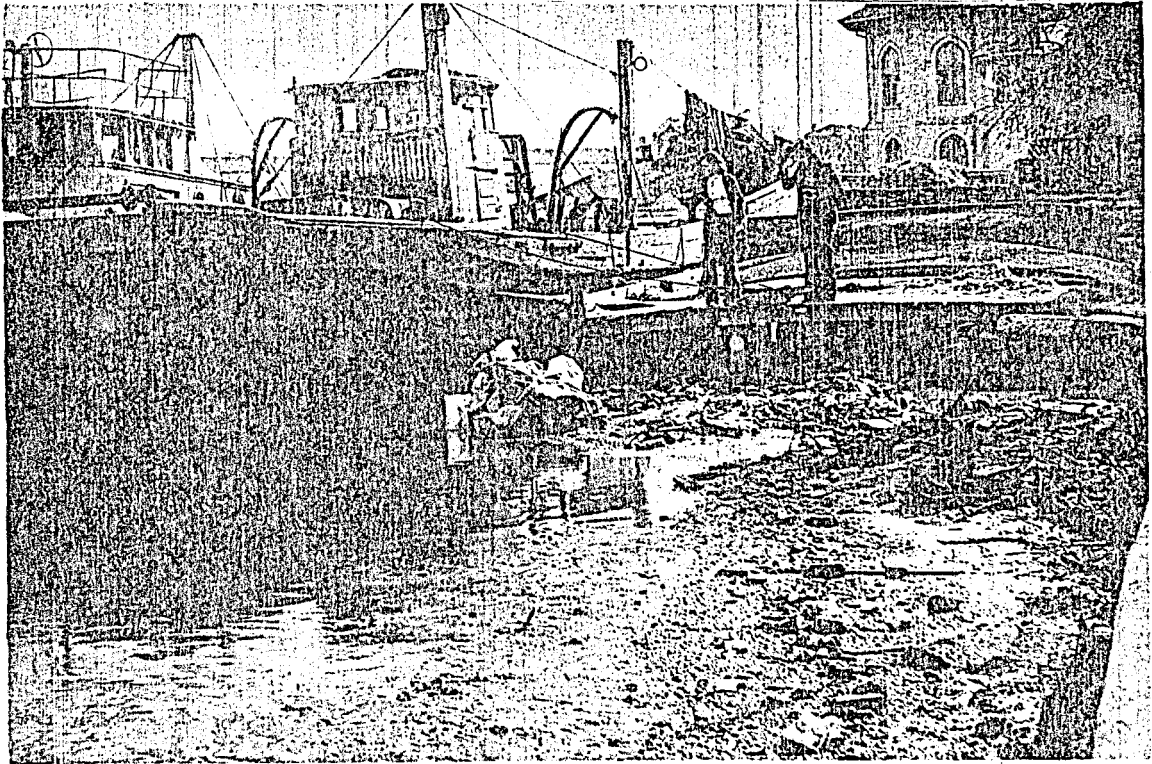


Fig. 3.I Domestic wastes on the shore at Eyüp

3. Erosion and Sedimentation : Fine materials of the steep hills of Alibey and Kagithane Creeks are transported during rainy seasons and sedimented at the bottom of Haliç at a rate of 10 cm. per year and constitute almost all of the sedimented material. These sediments are called Bottom Sludge and contains organic materials and heavy metals. These contents contribute also to the pollution of the water and the geotechnical problems of the area, (Fig.3.2).

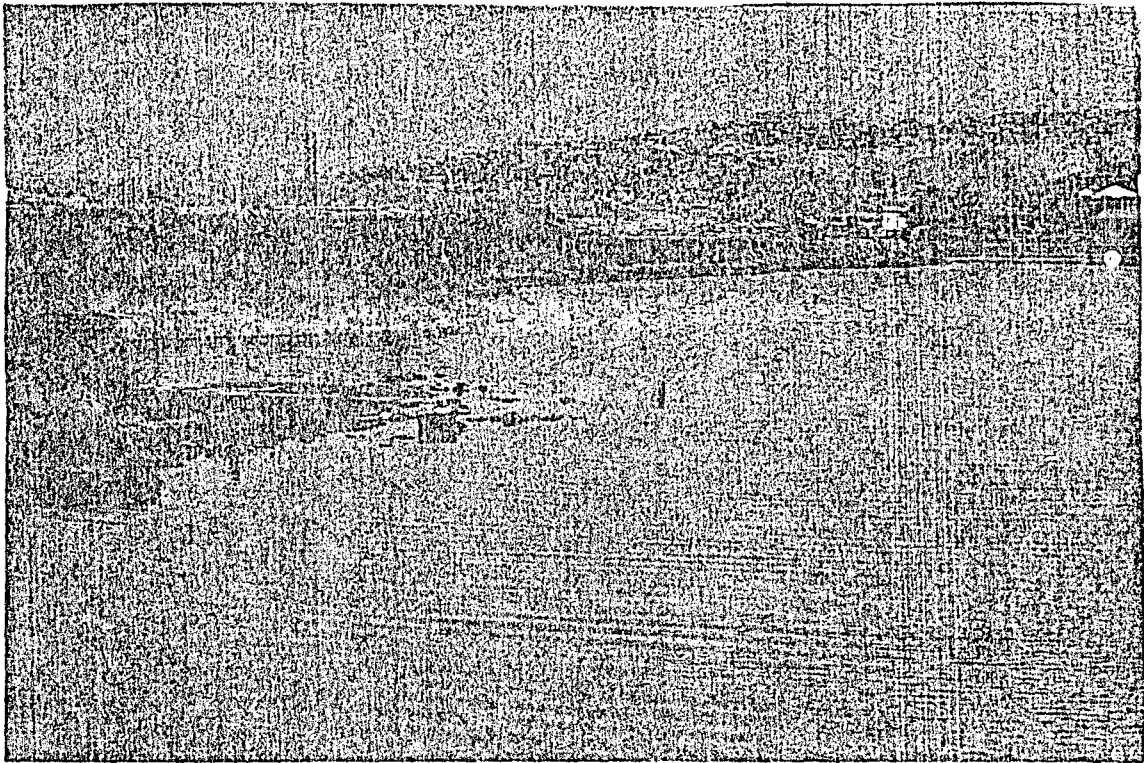


Fig.3.2 Sedimentation in Haliç, near Sütluce

4. Ships and Wrecks: Ships are polluting the water by their wastes and abandoned wrecks impede the circulation of water in Haliç, (Fig.3.3).

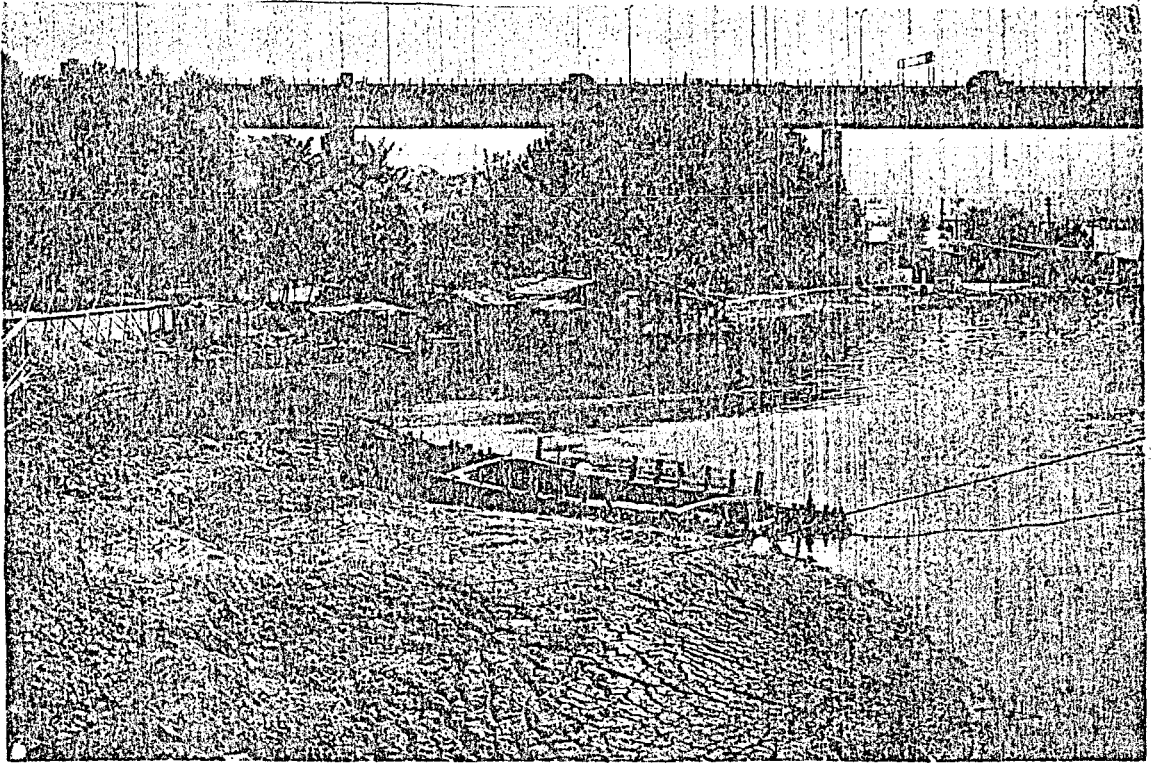


Fig. 3.3 An abandoned wreck on the shore

3.2 DREDGING OF BOTTOM SLUDGE

Based on numerous measurements at various times it has been determined that sedimentation of fine materials is on the order of 10 cm. per year. Therefore, it may be concluded that due to sediments a total of 260.000 m³ of fine material is transported by the creeks to Haliç every year.

The bottom sediments have basically three undesired features :

1. They contribute to the pollution of the water.
2. They impede sea transportation to the area.
3. They contribute a great deal to the geotechnical problems of the area.

These sediments are almost in a liquid state in the upper 5 to 7 meters zone and have unit weight of $\gamma = 1.10$ to 1.15 t/m^3 (Becan, 1974)

The geographical location of Haliç is providing many facilities in the sea transportation if the industrial plants keep their existence in the area, the sea transportation on Haliç will be the cheapest way for the transportation of raw materials and goods.

The present conditions are not suitable for an efficient sea transportation in Haliç. So the dredging of bottom sludge to obtain sufficient depth and to prevent pollution of water are necessary. But the geotechnical conditions in the vicinity of Haliç makes a preliminary study about stability of shores necessary.

There are many types of dredging equipment for different materials to be dredged. Over $1.000.000 \text{ m}^3$ of dredging was done in previous years in Haliç, (Table 3.2).

The amount of accumulation of sedimented material will decrease to 200.000 m^3 per year after the completion of Alibeyköy Dam construction. The amount of material to be dredged is about 2.5 million m^3 in Haliç, (Arıcan, 1976). Therefore, total volume of material will be 3.5 million m^3 at the end of the next four years.

Table 3.2

Volume and Location of Previous
dredgings in Haliç (Arıcan, 1976)

Location	Year	Volume, m ³
Sütlüce-Silahtar	1961	494.000
Hasköy-Halıcıoğlu	1965	250.000
Alibey Creek	1965	25.000
Eyüp - Silahtar	1974	330.000
TOTAL	-	1.094.000

Since the bottom sludge and underlying clay formation are very soft and very weak, stability of these formations should be evaluated. Also the stability of shores should be considered before dredging, (See chapter 4 and 5).

CHAPTER 4

SLOPE STABILITY

4.1 INTRODUCTION

Every mass of soil located beneath a sloping ground surface or beneath the sloping sides has tendency to move downward and outward under the influence of gravity. If this tendency is counteracted by shearing resistance of the soil, the slope is stable. Otherwise a slide occurs.

The failure of a mass of soil located beneath a slope is called a "Slide". Usually, slides are due to excavation or to undercutting the foot of an existing slope. Slides may occur in almost every conceivable manner, slowly or suddenly.

4.2 SLIDES IN COHESIVE SOILS

A cohesive material having a shearing resistance, s ,

$$s = c + p \tan \phi \dots\dots\dots(4.1)$$

- where c denotes cohesion
- p denotes normal stress
- ϕ denotes angle of shearing resistance.

can stand with a vertical slope at least for a short time, pro-

vided the height of the slope is somewhat less than critical height, H_c . If the height of a slope is greater than H_c , the slope is not stable unless it makes an angle with the vertical. If the height is very great compared to H_c , the slope will fail unless the slope angle is equal to or less than ϕ .

If the failure occurs along a surface of sliding that intersects the slope at or above its toe (Fig. 4.Ia), the slide is known as a "Slope Failure". On the other hand, if the soil beneath the level of the toe of the slope is unable to sustain the weight of the overlying material, the failure occurs along a surface that passes at some distance below the toe of the slope. A failure of this type is known as "Base failure", Fig(4.Ib).

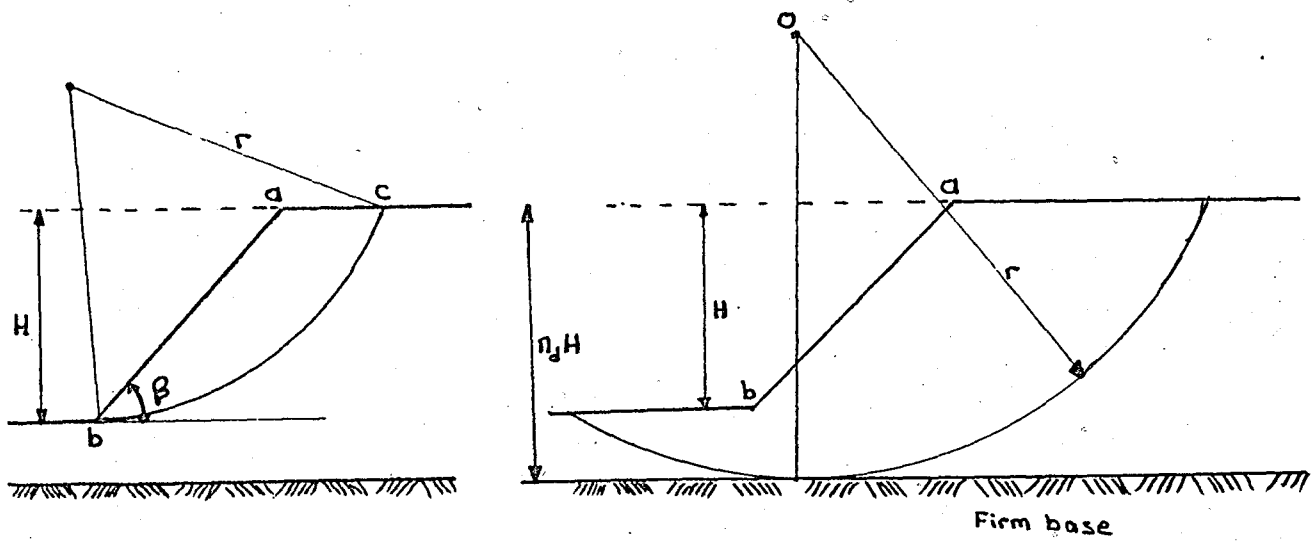


Fig. 4.I Position of critical circle for (a) slope failure (b) Base failure

4.3 PROCEDURE FOR INVESTIGATING STABILITY OF SLOPES

The general procedure is to determine the position of the surface of the sliding, to estimate the weights of the various parts of the sliding mass that tended to procedure or to oppose the slide; and to compute the average shearing resistance, s , of the soil necessary to satisfy the conditions for equilibrium of the mass.

In order to investigate whether or not a slope on soil with known shear characteristics will be stable, it is necessary to determine the diameter and position of the circle that represent the surface along which sliding will occurs. This circle known as the " Critical Circle ", must satisfy the requirement that the ratio between the shearing strength of the soil along the surface of sliding and the shearing force tending to produce the sliding must be a minimum.

After the diameter and position of the critical circle have been determined, The Factor of Safety, F , of the slope with respect to failure may be computed.

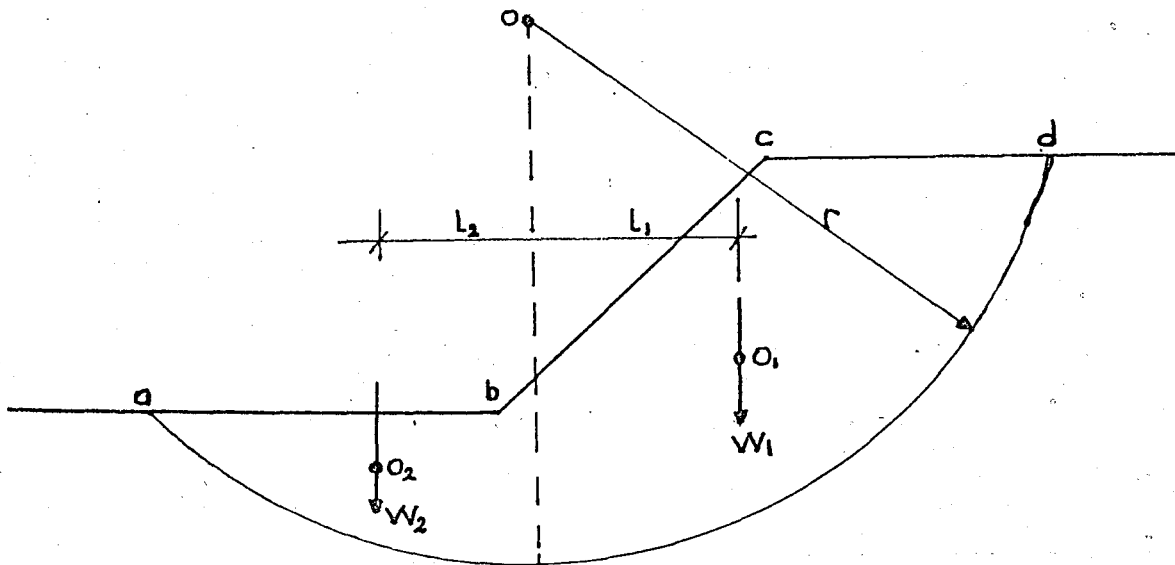


Fig. 4.2 Slope Failure

$$F = \frac{sr \widehat{da}}{W_1 l_1 - W_2 l_2} \dots\dots\dots(4.2)$$

Where r denotes the radius of the critical circle
 \widehat{da} denotes the length of the surface of sliding.

The slope stability may be investigated by trial. To make the investigation by trial, different circles are selected, each representing a potential surface of sliding. For each circle, the value of F (Eq.4.2) is computed. The minimum value represents the factor of safety of the slope with respect to sliding, and the corresponding circle is the critical circle.

4.4 SLOPES ON SOFT CLAY

The average shearing resistance, s , per unit of area of a potential surface of sliding in homogenous clay under undrained conditions ($\phi = 0$) :

$$s = \frac{1}{2} q_u = c \dots\dots\dots(4.3)$$

q_u denotes Unconfined Compressive Strength
 c denotes Cohesion.

If c is known, the critical height H_c of slope having a given slope angle β can be expressed by the equation,

$$H_c = N_s \frac{c}{\gamma} \dots\dots\dots(4.4)$$

where N_s denotes stability factor.

N_s is a pure number. Its value depends only on the slope angle β and on the depth factor n_d (Fig.4.Ib) which express the

depth at which the clay rests on a firm base. If a slope failure occurs, the critical circle is usually a "Toe Circle" that passes through the toe of the slope. However, if the firm base is located at a short distance below base the level of toe, the critical circle may be a "Slope Circle" that is tangent to the firm base and that intersects the slope above the toe.

The position of the critical circle with reference to a given slope depends on the slope angle β and the depth factor n_d .

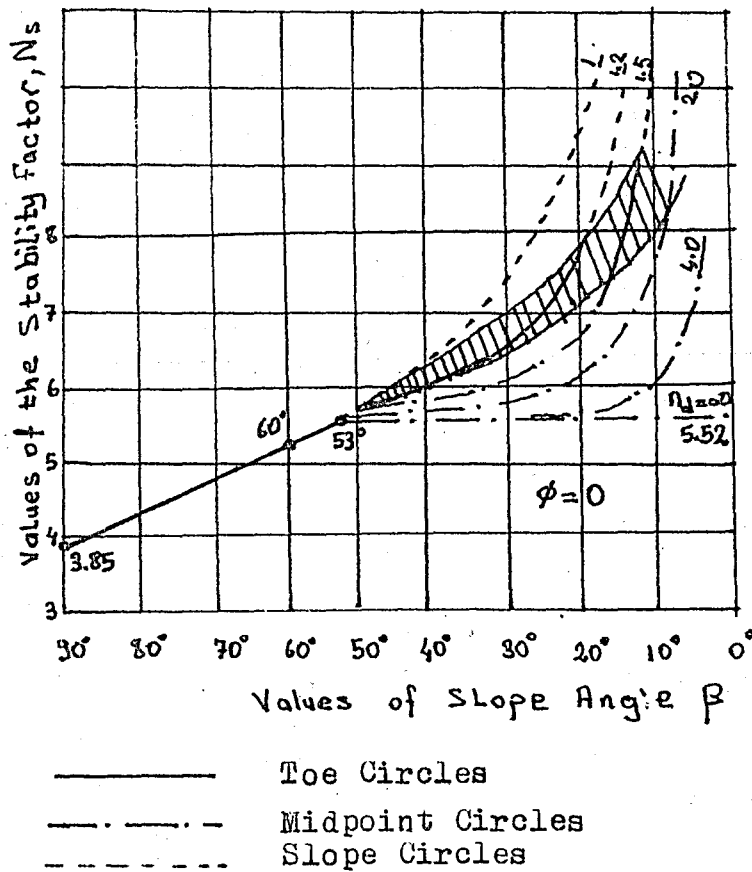


Fig. 4.3 Relation between slope angle and stability factor N_s , for different values of depth factor n_d (After Taylor, 1937)

According to fig.4.3 , the failure of all slopes rising at an angle of more than 53° occurs along a toe circle. If β is smaller than 53° , the type of failure depends on the value of the depth factor n_d and, at low values of n_d , also on the slope angle β . If n_d is equal to 1.0 , failure occurs along a slope circle.

If n_d is greater than about 4.0 , the slope fails along a midpoint circle tangent to the firm base. If n_d is intermediate in value between 1.0 and 4.0 , failure occurs along a slope circle if the point representing the values of n_d and β lies above shaded area in Fig. 4.3 . If the point lies within the shaded area, failure occurs a toe circle.

4.5 THE USE OF THE SLIP CIRCLE IN THE STABILITY ANALYSIS OF SLOPES

A. If slope is located above water table:

If a slope has an irregular surface that cannot be represented by a straight line , or if the surface of sliding is likely to pass through several materials with different values of c and ϕ , the stability can be investigated conveniently by the " Method of Slices " . According to this procedure , a trial circle is selected, (fig 4.4), and the sliding mass subdivided into a number of vertical slices 1,2,3 etc.

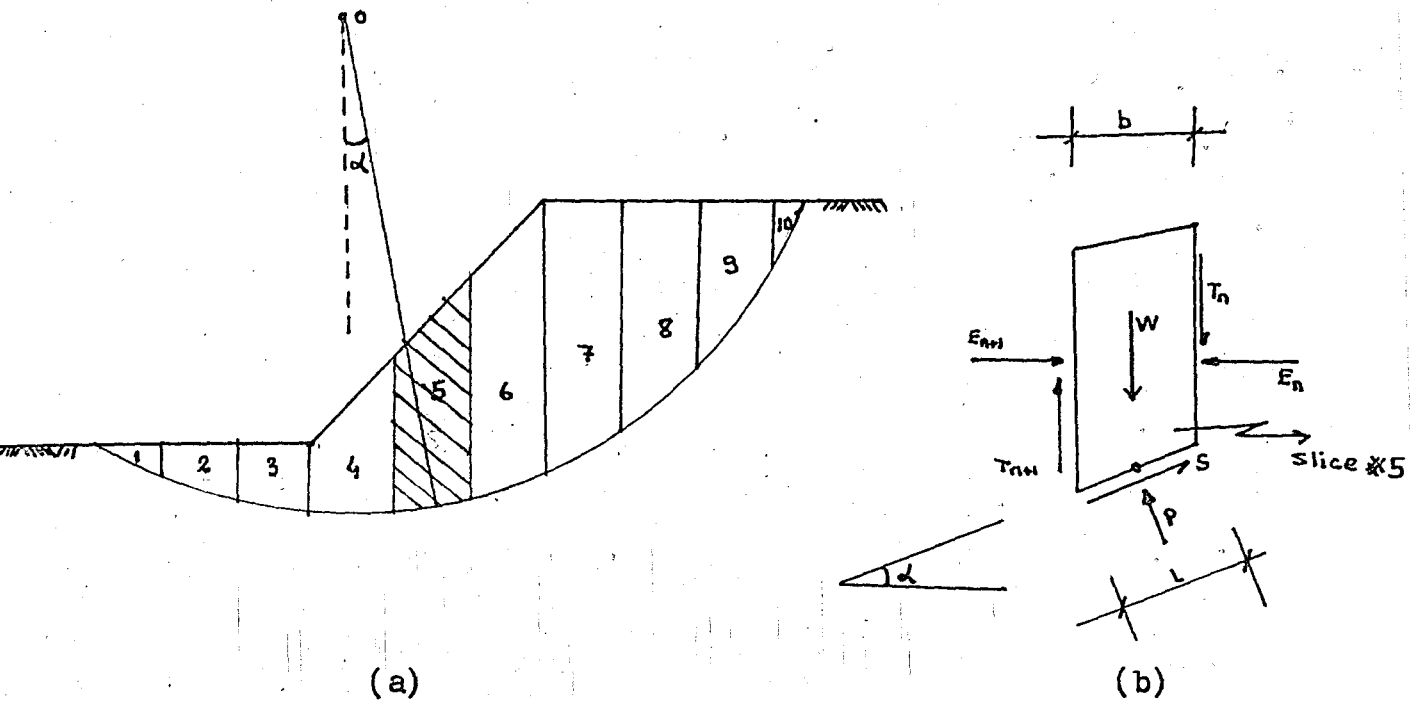


Fig 4.4 Method of slices for investigating equilibrium of slope located above water table

Each slice, such as slice 5 shown Fig 4.4b, is acted upon by its weight W , by shear forces T and normal forces E on its sides, and by a set of forces on its bases. These include the shearing force S and the normal force P .

The forces on each slice must satisfy the conditions of equilibrium. However, the forces T and E depend on the deformation and the stress-strain characteristics of the slice material and cannot be evaluated rigorously. They can be approximated with sufficient accuracy for practical purposes. The simplest approximation consists of setting these forces equal to zero. Under these circumstances, if the entire trial circle is located above water table and there no excess pore pressures?

The equilibrium of the entire sliding mass requires that

$$r \leq W \sin \alpha = r \leq S \quad \dots\dots\dots(4.5)$$

If s is the shearing strength of the soil along t , then

$$S = \frac{s}{F} L = \frac{s}{F} \frac{b}{\cos \alpha} \quad \dots\dots\dots(4.6)$$

and

$$r \leq W \sin \alpha = \frac{r}{F} \leq \frac{s b}{\cos \alpha} \quad \dots\dots\dots(4.7)$$

whence

$$F = \frac{\leq (s b / \cos \alpha)}{\leq W \sin \alpha} \quad \dots\dots\dots(4.8)$$

The shearing strength s , however, is determined by

$$s = c + p \tan \phi \quad \dots\dots\dots(4.9)$$

where p is the normal stress across the surface of sliding l .

To evaluate p we consider the vertical equilibrium of the slice (Fig 4.4b), whence

$$W = S \sin \alpha + P \cos \alpha \quad \dots\dots\dots(4.10)$$

$$P = \frac{P}{L} = \frac{P \cos \alpha}{b} = \frac{W}{b} - \frac{S}{b} \sin \alpha \quad \dots\dots\dots(4.11)$$

therefore

$$s = c + \left(\frac{W}{b} - \frac{S}{b} \sin \alpha \right) \tan \phi = c + \left(\frac{W}{b} - \frac{S}{F} \tan \alpha \right) \tan \phi \quad \dots\dots\dots(4.12)$$

and

$$S = \frac{c + (W/b) \tan \phi}{1 + (\tan \alpha \tan \phi) / F} \quad \dots\dots\dots(4.13)$$

Let

$$m_\alpha = \left(\frac{F + \operatorname{tg} \alpha \cdot \operatorname{tg} \phi}{F} \right) \operatorname{Cos} \alpha \dots \dots \dots (4.I4)$$

Then

$$F = \frac{\sum [c + (w/b) \operatorname{tg} \phi] b}{m_\alpha \sum W \operatorname{Sin} \alpha} \dots \dots \dots (4.I5)$$

Equation 4.I5, which gives the factor of safety, F , for the trial circle under investigation contains on the right-hand side the quantity m_α (Eq.4.I4) which is itself a function of F . Therefore Eq.4.I5 must be solved by successive approximations in which a value of $F = F_I$ is assumed and used for calculation of m_α , whereupon F is then computed. If the value of F differs significantly from F_I , the calculation is repeated. The calculations are facilitated by the chart from which values of m_α can be taken, (Janbu, 1956)

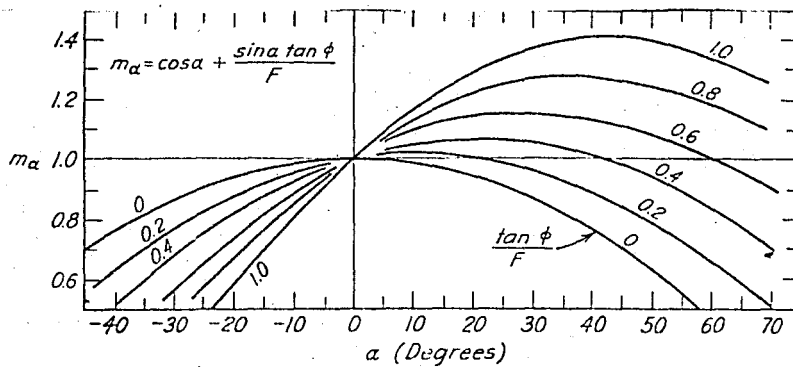


Fig 4.5 Chart for evaluating factor m_α

B. If the slope is partly submerged :

In general, the slope may be partly submerged and there will be pore pressures acting along the trial circle , (Fig 4.6)

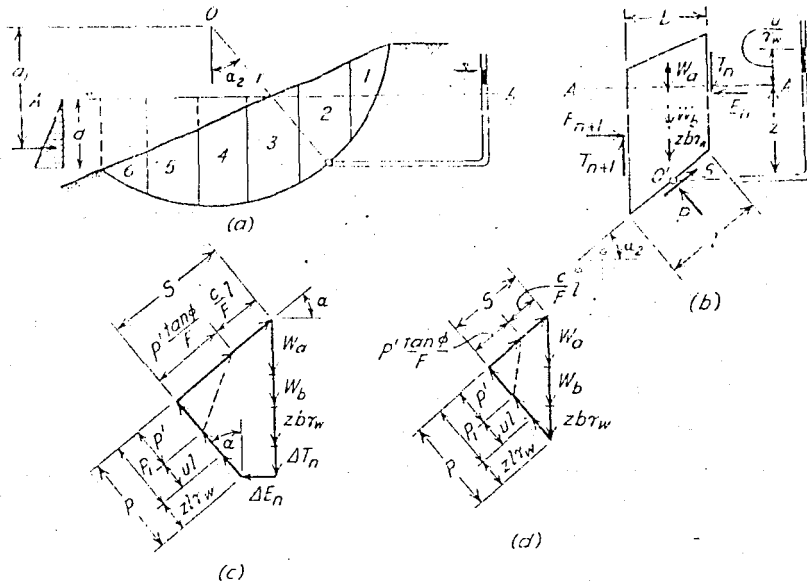


Fig 4.6 Method of slices for investigating equilibrium of slope for partly submerged slopes (d) Force polygon for slice 2 if forces T and E on sides of slice are considered to be zero.

The magnitudes of the pore pressures depend upon the conditions of the problem. In some instances they may be estimated by means of a flow net or field observations. If the level of external water surface is denoted by A-A , the weight, W , of the slice may be written as,

$$W = W_a + W_b + z b \gamma_w \dots \dots \dots (4.16)$$

where W_a is the weight of that part below A-A , And W_b is the submerged weight of the part below A-A and $z b \gamma_w$ is the

weight of a volume of water equal to submerged portion of the slope. If entire slice is located beneath the water level, as slice 3, the weight of the water above the slice must be included in $z b \gamma_w$. The pore pressure at the midpoint O^A of the base of the slice is $z \gamma_w + u$, where u is the excess pore pressure with respect to external water level. If the external water level A-A is located below O^A on the base of the slice, the pore pressure at O^A is h/γ_w , where h is the height to which the water would rise in a piezometer at O^A . If the pore pressure is due to capillarity, h is negative. The shearing stress, t , along the surface of sliding is,

$$t = \frac{s}{F} = \frac{1}{F} (c + \bar{p} t g \phi) = \frac{1}{F} \left[c + \left(\frac{P}{L} - z \gamma_w - u \right) t g \phi \right]$$

whence

$$S = t \cdot L = \frac{1}{F} [cL + (P - zL\gamma_w - uL) t g \phi] = \frac{1}{F} (cL + P' t g \phi)$$

Equilibrium of the entire slide with respect to moments about the centre of the trial circle requires that

$$\begin{aligned} \sum (W a + W_b + z b \gamma_w) r \sin \alpha &= \sum S \cdot r + \frac{1}{2} \gamma_w d^2 a_1 \\ &= \frac{1}{F} \sum (cL + P' t g \phi) r + \frac{1}{2} \gamma_w d^2 a_1 \dots \dots (4.19) \end{aligned}$$

However, the water below level A-A is in equilibrium,

whence

$$\sum z_b \gamma_w r \sin \alpha = \frac{1}{2} \gamma_w d^2 a_1 \dots \dots \dots (4.20)$$

Therefore,

$$\sum (W_a + W_b) r \sin \alpha = \frac{1}{F} \sum (cL + P' \operatorname{tg} \phi) r \dots (4.21)$$

And

$$F = \frac{\sum (cL + P' \operatorname{tg} \phi)}{\sum (W_a + W_b) \sin \alpha} \dots \dots \dots (4.22)$$

$$W_a + W_b + z_b \gamma_w = [z_l \gamma_w + P' + uL] \cos \alpha + \left(P' \frac{\operatorname{tg} \phi}{F} + \frac{cL}{F} \right) \sin \alpha \dots \dots \dots (4.23)$$

and

$$P' = \frac{W_a + W_b - uL - \frac{cL}{F} \sin \alpha}{M_\alpha} \dots \dots \dots (4.24)$$

Substitution of eq. 4.24 in to 4.22

$$F = \frac{\sum [cb + (W_a + W_b - u_b) \tan \phi]}{\sum (W_a + W_b) \sin \alpha} \dots\dots\dots(4.25)$$

It may be noted that the influence of the external water level is fully taken into account by the use of the submerged weight, W_b , and that the excess pore pressure, u , is calculated for the base of each slice. The procedure described in the preceding paragraphs may be modified to take into account the forces T and E between the slices (Bishop, 1955).

4.6 COMPUTER PROGRAM FOR SLOPE STABILITY

This computer program (KÖSELER-I) is developed using Bishop's (1955) Modified Procedure. The program uses a circular -arc failure surface. First the intersection coordinates of soil layers and the potential failure surface are found then the areas, angles, etc., can be calculated.

The program will solve any slope stability problem where the ground surface can be described by a series of straight lines. Any number of lines and soil types can be used. The program allows for describing the pore pressure by use of saturated soil unit weights. The program computes both the total and effective slice weights;

It is necessary in using this program to :

- I. Number all line intersections in increasing X

coordinates from left to right.

2. Number the upper external (closest to arc center) soil lines first in order from left to right. Interior soil lines may be numbered in any order.

3. The different soils in the mass may be numbered in any order.

4. Compute all line intersections accurately to 0.005 to SMLNO=0.01 will properly test coordinates.

The program locates all line intersections inside the trial arc including those lines intersecting the arc. A slice is located on every intersection point. Distances between intersection points are divided according to the slice-width specification (SWIDTH)?

This program will compute in either metric or fps units. Use meters and kilonewtons or feet and pounds. The unit card contains three entries:

M	CM	9.807
FT	IN	62.500

4.7 OPERATION OF COMPUTER PROGRAM

LINE	OPERATION
I-5	Bookkeeping
6	READ TITLE and work units(Two cards)
I3	READ(I5I5) NOL: total number of soil lines NLIT: total number of line intersections(The end of any line whether or not intersected by another line is a line intersection) NOS: number of soil lines in mass(Same soil submerged is counted twice) NOLE: number of top external soil lines ITX-ITY: number of circle centre points in X,Y directions to be analyzed for a single entrance point PCODE: plot subroutine used if > 0 NP: plot control counter DIMEN: control number of slices as 75,80,90 ,etc. LIST: control to obtain extra output(after test run use 0 to converse paper)
I4	READ(5,*) CX,CY: initial trial circle centre coordinates ENTX ENTY: trial circle entrance coordinates DELX,DELY: centre X,Y coordinates increments for each trial SWIDTH: initial slice width(DIMEN may increase value
I5	READ(5,*) SCALE: plotting scale as 20,30 for I inch. HAH : top X coordinates of slope YAY : distributed load on soil($q = 2 \text{ t/m}$)

LINE	OPERATION
27-52	READ problem data on line intersections, soils , etc., and forms arrays for later use, also writes data for checking
28	READ NLI:number of line intersections of each line in turn one entry per card
29	READ (C(I,J),NOLIT(I,N),N<=I,NLI) C(I,J) : line data including line number , number of line intersections for the lines, the X,Y coordinates of the end points left to right(6 entries) NOLIT(I,N): all the line intersection numbers on the i th line including the end values(NLI entries)
30	Gives vertical lines the slope value of BIGNO so computer doesnot divide by 0.0
39-40	READ INTAR(J,K) INTAR(J,K): line intersection X,Y coordinates in increasing intersection numbers
47	READ soil data on DO loop NSLIN(I): number of soil lines defining the boundary of the soil. Include lines terminating at a joint. If a line intersection a soil-boundary between the ends count the soil boundary between the ends, twice G(I): unit weight either saturated or wet PHI(I): ϕ angle COHES(I): cohesion SAT: 1.if saturated,0.if wet
52	READ LINSOL: soil line number , INTL-INTR: intersection number on left and right and of line(if a soil line ter-

LINE

OPERATION

minates to a joint on a soil boundary, that line is included, the joint number is used for both INTL and INTR.

62

Begins DO to test circles

69-I40

Computes trial circle, line intersections, find lines not used LNU(I), those in circle but not intersected by circle

I4I-I96

Sets up arc intersection array ARCINT

I97-22I

Find slice width and checks total number of slices against DIMEN and increments slice width if necessary

222-285

Finds coordinates of all line intersecting slices in slice array SLIC(I,J,K). Note that lines not intersected in a slice area given same coordinates as last line intersected and stacked at a point. This so routine for both coordinates test and area computations can be used using all lines. SLIC array is sorted for decreasing Y coordinates.

286-352

Computes areas of slice parts and weights, both effective and total, sums slice weights, finds ϕ and c for soil touching arc surface

353-39I

Computes safety factor


```

1) 6UL
DIMENSION C(15,6),NOLIT(15,0),SLOPE(15),INTAR(15,2),EFFWT(100
& NSLIN(10),G(10),PHI(10),COHES(10),SLICX(76),SOIL(8,9,4),SAT(10
& ARCINT(20,3),LNU(15),CO(100),ALPHA(100),TITLE(20),SLIC(76,10,2
& P(100),B(100),AREA(100),WEIGH(100),ALLINT(30,3),IBUF(1000)
INTEGER PCODE,DIMEN
REAL INTAR,METER
BIGNO=99999999
SMLNO=0
1000 READ(5,1000)TITLE,UT1,UT2,FU4
FORMAT(20A4/A4,6X,A4,6X,F10.4)
2000 WRITE(6,2000)TITLE
FORMAT(1,15,20A4,/)
READ(5,*)NOL,NLIT,NOS,NOLE,ITX,ITY,PCODE,NP,DIMEN,LIST
READ(5,*)CX,CY,ENTX,ENTY,DELX,DELY,SWIDTH
READ(5,*)SCALE,HAH,YAY
WHOLD=SWIDTH
NOSP1=NOS+1
2001 WRITE(6,2001)NOL,NLIT,NOS,NOLE,ITX,ITY,SWIDTH,UT1
FORMAT(15,15,NO OF LINES',I3,5X,'NO OF LINE INTERSECT='',I3,/,15,
& 'NO OF SOILS='',I3,5X,'NO OF EXTERNAL SOIL LINES='',I3,/,15,
& 'NO OF X INCREMENTS='',I3,5X,'NO OF Y INCREMENTS='',I3,/,15,
& 'INITIAL SLICE WIDTH='',F5.4,5X,A2//)
2003 WRITE(6,2003)
FORMAT(15,15,'THE LINE END COORD MATRIX',/,T4,'LINE NO',T12,'NO I
& T21,'XT',8X,'Y1',8X,'X2',8X,'Y2',6X,'SLOPE',5X,'LINE INTER NO'
C DO 333 I=1,NOL
NLI=NO OF INTERSECT ON ANY LINE MUST HAVE AT LEAST 2 VALUES
READ(5,*)NLI
WRITE(5,*)(C(I,J),J=1,6),(NOLIT(I,N),N=1,NLI)
SLOPE(I)=BIGNO
IF(ABS(C(I,5)-C(I,3))LE 0.001)GO TO 333
SLOPE(I)=(C(I,6)-C(I,4))/(C(I,5)-C(I,3))
333 WRITE(6,2004)(C(I,J),J=1,6),SLOPE(I),(NOLIT(I,KK),KK=1,NLI)
2004 FORMAT(T6,F3.0,3X,F3.0,T15,4(2X,F8.2),G13.6,1X,6I5)
C READ X AND Y COORDINATES TO BUILD LINE INTERSECT ARRAY (INTAR)
WRITE(6,2005)
2005 FORMAT(/,15,'LINE INTERSECT ARRAY',/,T4,'INT NO',T16,'X',T28,
DO 2 J=1,NLI
READ(5,*)(INTAR(J,K),K=1,2)
WRITE(6,2006)J,(INTAR(J,K),K=1,2)
2006 FORMAT(T6,I3,T12,F10.2,2X,F10.2)
C BUILD SOIL INTERSECTION ARRAY USING (INTNO)
WRITE(6,2008)
2008 FORMAT(/,15,'SOIL DATA ARRAY',/,T4,'SOIL NO',T13,'LINE #',T21
& 'LEFT INT',3X,'RT INT',3X,'SAT',3X,'UNIT WT',3X,'PHI',3X,'COH
& ON')
C NUMBER SOILS IN ANY ORDER
DO 5 I=1,NOS
READ(5,*)NSLIN(I),G(I),PHI(I),COHES(I),SAT(I)
NS=NSLIN(I)
DO 5 K=1,NS
READ(5,*)LINSOL,INTL,INTR
SOIL(I,K,1)=LINSOL
SOIL(I,K,2)=INTL
SOIL(I,K,3)=INTR
SOIL(I,K,4)=SAT(I)
5 WRITE(6,2009)I,(SOIL(I,K,MM),MM=1,4),G(I),PHI(I),COHES(I)
2009 FORMAT(15,I3,6X,F3.0,7X,F3.0,6X,F3.0,6X,F2.0,5X,F6.1,3X,F4.1,3
& I)
PCOUN=0
BEGIN LOOP TO TEST TRIAL CIRCLES
100 DO 350 IY=1,ITY
IF(IY.GT.1)CY=CY+DELY
DO 350 IX=1,ITX
PCOUN=PCOUN+1
NCOUN=PCOUN
SWIDTH=WHOLD
IF(IX.GT.1)CX=CX+DELX
C COMPUTE RADIUS OF TRIAL CIRCLE
R=SQRT((ENTX-CX)**2+(ENTY-INTY)**2)
WRITE(6,212)NCOUN,CX,CY,ENTX,ENTY,R
212 FORMAT(/,15,'TRIAL CIRCLE NO',I3,/,15,'CIRCLE CTR COORDS:',2X
& ',2X,'X=',F10.2,2X,'Y=',F10.2,/,15,'ENTRANCE PT. COORDS:',2X,'
& ',F10.2,2X,'Y=',F10.2,/,15,'TRIAL ARC RADIUS=',F10.3,/)
X1=0
DO 8 I=1,NOL
LNU(I)=0
IF(ABS(SLOPE(I))LE 0.001)GO TO 9
CON=C(I,3)-C(I,4)/SLOPE(I)
AA=1.0/SLOPE(I)**2+1.0
BB=2.0*CON/SLOPE(I)+2.0*CX/SLOPE(I)-2.0*CY
CC=CON**2-2.0*CX*CON+CX**2+CY**2-R**2

```

```
DIFF=BB**2-4*AA*CC
IF(DIFF.LT.0)GO TO 20
YPR=(BB+SQRT(DIFF))/(2*AA)
YNR=(BB-SQRT(DIFF))/(2*AA)
```

```
C THIS PART COMPUTE X COORDS
XPR=YPR/SLOPE(I)+CON
XNR=YNR/SLOPE(I)+CON
```

```
GO TO 10
C FOLLOWING STEPS USED FOR HORIZONTAL LINES
```

```
9 DIFF=R**2-(CY-C(I,4))**2
IF(DIFF.LT.0)GO TO 20
XPR=CX+SQRT(DIFF)
XNR=CX-SQRT(DIFF)
YPR=C(I,4)
YNR=C(I,4)
```

```
10 J1=0
J2=0
IF(A3S(SLOPE(I))GE.BIGNO)GO TO 11
IF(XPRGE.C(I,3)AND XPRLE.C(I,5))J1=1
IF(XNRGE.C(I,3)AND XNRLE.C(I,5))J2=1
GO TO 12
```

```
11 IF(SLOPE(I).EQ.66.66.666
66 IF(YPRGE.C(I,6)AND YPRLE.C(I,4))J1=1
IF(YNRGE.C(I,6)AND YNRLE.C(I,4))J2=1
GO TO 12
```

```
666 IF(YPRGE.C(I,4)AND YPRLE.C(I,6))J1=1
12 IF(YNRGE.C(I,4)AND YNRLE.C(I,6))J2=1
IF(J2.EQ.0)GO TO 13
```

```
K1=K1+1
ARCINT(K1,1)=I
ARCINT(K1,2)=XNR
ARCINT(K1,3)=YNR
13 IF(J1.EQ.0)GO TO 7
```

```
K1=K1+1
ARCINT(K1,1)=I
ARCINT(K1,2)=XPR
ARCINT(K1,3)=YPR
GO TO 8
```

```
7 IF(J1.NE.0.OR.J2.NE.0)GO TO 8
C END OF LOOP FOR ARC&LINE INTERSECTIONS
```

```
20 LNU(I)=I
WRITE(6,210)I
2101 FORMAT(/,T5,'XXX LINE',I3,'NOT INTERSECTED BY TRIAL CIRCL')
8 CONTINUE
```

```
DO 400 I=1,NOL
IF(LNU(I).EQ.0)GO TO 400
R1=SQRT((CX-C(I,3))**2+(CY-C(I,4))**2)
R2=SQRT((CX-C(I,5))**2+(CY-C(I,6))**2)
IF(R1.LT.R2AND R1.LT.R2)GO TO 400
LNU(I)=0
```

```
IF(SLOPE(I).EQ.BIGNO)LNU(I)=I
403 IF(SLOPE(I).EQ.BIGNO)WRITE(6,403)LNU(I)
FORMAT(/,T5,'*** LINE',I3,'IS IN ARC BUT VERT AND NOT USED')
WRITE(6,401)I
401 FORMAT(/,T5,'***LINE',I3,'IS NOT INTERSECTED BUT IS IN ARC')
400 CONTINUE
```

```
C FIND WIDTH OF K=TOTAL ENTRIES IN CIRCLE&LINE INT ARRAY
```

```
24 DO 25 KY=1,K1M
IF(ARCINT(KY,2)LE.ARCINT(KY+1,2))GO TO 26
DO 25 KX=1+3
SAVE=ARCINT(KY,KX)
ARCINT(KY,KX)=ARCINT(KY+1,KX)
ARCINT(KY+1,KX)=SAVE
```

```
25 CONTINUE
GO TO 24
26 CONTINUE
WRITE(6,2112)
2112 FORMAT(/,T5,'ARC INTERSECT WITH LINE ARRAY',/ ,T4,'LINE NO'
```

```
8, T19, 'X', T32, 'Y')
WRITE(6,2114)((ARCINT(KZ, JJ), JJ=1, 3), KZ=1, K1)
```

```
2114 FORMAT(T5,F3.0,T13,F10.3,2X,F0.2)
LINE1=ARCINT(1,1)
S1=ARCINT(1,2)
S2=ARCINT(1,3)
WRITE(6,8053)
8053 FORMAT(/,T5,'THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:')
ICOUV=0
```

```
K=1
KK=0
LL=NLI+K
C COMBINE ARCINT & INTAR IN ORDER OF INC. X VALUES
```

```

DO 70 I=1,LL
KK=KK+1
DO 75 J=1,2
75 ALLINT(I,J)=INTAR(KK,J)
IF(I.NE.I) AND ALLINT(I,J).EQ.INTAR(KK,I) GO TO 70
IF(ARCINT(K,2).GE.INTAR(KK,2)) GO TO 70
IF(ICOUN.GT.0) GO TO 70
72 DO 73 L=1,2
73 ALLINT(I,L)=ARCINT(K,L)
IF(K.EQ.K1) ICOUN=1
K=K+1
IF(K.GT.K1) K=K1
KK=KK+1
70 WRITE(6,805) I,(ALLINT(I,J),J=1,2),K,KK
805 FORMAT(T5,'I=',I3,2X,2F12,3,2X,'K=',I3,2X,'KK=',I3)
8052 FORMAT(/,T5,'THE APPLICABLE ARRAY ARCINT FOLLOWS:')
LAL=0
DO 77 I=1,LL
R2=SQRT((CX ALLINT(I,1))**2+(CY ALLINT(I,2))**2)
IF(R2.GT.(R*SMLNO)) GO TO 77
LAL=LAL+1
DO 78 K=1,2
78 ARCINT(LAL,K)=ALLINT(I,K)
WRITE(6,805) LAL,(ARCINT(LAL,J),J=1,2),I,LAL
77 CONTINUE
C CALCULATE THE WIDTH BETWEEN EACH INT. POINT
33 SLICX(1)=S1
SLIC(1,1,1)=S2
SLIC(1,1,2)=LINE1
C DIVIDE WIDTH(L) INTO SLICES OF SIZE
WRITE(6,8057)
8057 FORMAT(/,T5,'FIND SLICE WIDTH AND NO OF SLICES')
98 N=I
NOSLIC=1
KM=1
K=LAL
DO 45 L=1,K
MM=1
IF((ARCINT(L+1,1)-ARCINT(L,1))/LE.SWIDTH) GO TO 46
DO 47 MM=1,100
AM=MM
WIDTH=(ARCINT(L+1,1)-ARCINT(L,1))/AM
IF(WIDTH.LE.SWIDTH) GO TO 49
47 CONTINUE
46 WIDTH=ARCINT(L+1,1)-ARCINT(L,1)
49 NOSLIC=NOSLIC+MM
C CONTROL FOR DIMENSION OF 75 SPACES IN
IF(NOSLIC.LT.DIMEN) GO TO 99
SWIDTH=SWIDTH+0.5
WRITE(6,9999) SWIDTH
9999 FORMAT('0',T5,'*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTE
ED TO',F5.2,1X,A2)
GO TO 98
99 NSM=NOSLIC
DO 51 I=N,NOLE
IF(LNU(I).EQ.I) GO TO 51
101 DO 52 JJ=KM,NSM
SLICX(JJ+1)=SLICX(JJ)+WIDTH
SLIC(JJ+1,1,1)=SLIC(JJ,1,1)+WIDTH*SLOPE(I)
SLIC(JJ+1,1,2)=I
52 DIFF=SLICX(JJ+1)-C(I,5)
IF(ABS(DIFF).GT.0.50,50,48)
50 N=I+1
48 KM=NOSLIC
GO TO 45
51 CONTINUE
45 CONTINUE
C COMPLETE SLICE ARRAY
NOLP=NOL+1
NOLE=NOLE+1
DO 60 I=1,NOSLIC
N=2
ARCY=CY SQRT(R**2-(CX SLICX(I))**2)
DO 59 J=NOL,P,NOL
IF(LNU(J).EQ.J) GO TO 59
SLIC(I,N,2)=J
SLIC(I,N,1)=C(J,4)+(SLICX(I)-C(J,3))*SLOPE(J)
IF(SLICX(I).LT.(C(J,3)-SMLNO).OR.SLICX(I).GT.(C(J,5)+SMLNO)) SLI
E(I,N,1)=0
IF(SLIC(I,N,1).GT.(SLIC(I,1,1)+SMLNO).OR.SLIC(I,N,1).LT.(ARCY
E SMLNO)) SLIC(I,N,1)=0
57 N=N+1

```

```

59 CONTINUE
60 SLIC(I,N,1)=ARCY
60 SLIC(I,N,2)=NOLPT
C SORT SLICE ARRAY IN DECREASING ORDER
21 T6 IF (LIST.NE.0)WRITE(6,21.6)
E) FORMAT(T6,'SLICE#',2X,'X-COORD',4(2X,'LINE NO',2X,'Y-COORD'
MOUN=N
N=MOUN-1
DO 81 KZ=1,NOSLIC
84 NUM=1
DO 85 KY=1,N
IF (SLIC(KZ,KY,1) LE.9.50)GO TO 82
IF ((SLIC(KZ,KY,1)+SMLNO) GE. SLIC(KZ,KY+1,1))GO TO 85
SAVE=SLIC(KZ,KY,1)
SLIC(KZ,KY,1)=SLIC(KZ,KY+1,1)
SLIC(KZ,KY+1,1)=SAVE
SAVE=SLIC(KZ,KY,2)
SLIC(KZ,KY,2)=SLIC(KZ,KY+1,2)
SLIC(KZ,KY+1,2)=SAVE
GO TO 85
82 SLIC(KZ,KY,1)=SLIC(KZ,KY+1,1)
SLIC(KZ,KY,2)=SLIC(KZ,KY+1,2)
85 IF (KY.NE.1)AND (SLIC(KZ,KY,1) SMLNO LE. SLIC(KZ,KY+1,1))NUM=NUM
E+1
IF (NUM.NE.N)GO TO 84
81 IF (LIST.NE.0)WRITE(6,3)KZ,SLICX(KZ),(SLIC(KZ,KY,2),SLIC(KZ
E,KY,1),KY=1,MOUN)
3 FORMAT(T6,I5,9F9.2,/,T20,8F9.2,/,T20,8F9.2,/,T20,8F9.2)
DO 306 I=1,NSMI
SAREA=0.0
WEIGHT=0.0
EFWT=0.0
ISOIL=0
NN=MOUN
IF (LIST.NE.0)WRITE(6,350)I
350 FORMAT(7,T5,'SLICE LINE NUMBER',I4)
DO 303 J=1,NN
DA=(SLIC(I,J,1)+SLIC(I+1,J,1)+SLIC(I,J+1,1)+SLIC(I+1,J+1,1))*
E(SLICX(I+1)+SLICX(I))/2.0
IF (DA LE. SMLNO)GO TO 303
DO 305 II=1,NOSP1
IF (II EQ. NOSP)GO TO 308
IF (ISOIL EQ. II)GO TO 305
N=NSLIN(II)
ICOUNT=0
JCOUNT=0
311 DO 304 JJ=1,N
IF (JCOUNT EQ. 2)GO TO 305
INTL=SOIL(II,JJ,2)
INTR=SOIL(II,JJ,3)
IF (ICOUNT EQ. 1)GO TO 310
IF (SLIC(I,J,2) NE. SOIL(II,JJ,2))GO TO 304
ICOUNT=1
JSOIL=II
IF ((SLICX(I)+SMLNO) GE. INTAR(INTL,I) AND (SLICX(I) SMLNO) LE.
EINTAR(INTR,I))GO TO 310
ICOUNT=0
GO TO 304
310 IF (SLIC(I+1,J,2) NE. SOIL(II,JJ,1))GO TO 304
IF ((SLICX(I+1)+SMLNO) LT. INTAR(INTL,I) OR (SLICX(I+1) SMLNO) GE
EINTAR(INTR,I))GO TO 304
ICOUNT=2
IF (JSOIL NE. II)GO TO 305
ISOIL=II
302 SAREA=SAREA+DA
308 GSUB=G(ISOIL)
IF (SAT(ISOIL) GT. 0.7)GSUB=G(ISOIL)*FU4
EFWT=EFWT+DA*GSUB
WEIGHT=WEIGHT+DA*G(ISOIL)
IF (LIST EQ. 0)GO TO 9092
WRITE(6,351)J,I,DA
351 FORMAT(I10,'DSLICE NO',I2,'OF SLICE ',I3,'WITH DA OF',F10.3)
WRITE(6,352)ISOIL,J,SAREA,WEIGHT,EFWT
352 FORMAT(I15,'SOIL ',I3,'LIES IN DSLICE ',I3,/,T15,'TOTAL AREA
E=',F10.3,3X,'TOTAL WEIGHT=',G10.3,5X,'EFFECT WT=',G10.3)
9092 GO TO 303
304 CONTINUE
IF (ICOUNT EQ. 1)JCOUNT=JCOUNT+1
IF (ICOUNT EQ. 2)GO TO 311
305 CONTINUE
303 CONTINUE
ALPHA(I)=AR SIN(ABS(CX((SLICX(I+1)-SLICX(I))/2.0+SLICX(I)))/R)

```

```

AREA(I)=SAREA
WEIGH(I)=WEIGHT
CO(I)=COHES(ISOIL)
306 P(I)=PHI(ISOIL)
IF(LIST, EQ, 0) GO TO 365
WRITE(6, 354)
354 FORMAT(T5, 'SLICE#', 3X, 'AREA', 3X, 'WEIGHT', 4X, 'COHESION', 3X, 'P
&+I', 3X, 'ALPHA')
DO 307 I=1, NSM1
IF(AREA(I).LE.SMLNO) GO TO 362
WRITE(6, 353) I, AREA(I), WEIGH(I), CO(I), P(I), ALPHA(I)
GO TO 307
352 WRITE(6, 353) I, AREA(I), WEIGH(I)
353 FORMAT(T7, I2, 2X, 3F10.3, F6.2, F9.4)
307 CONTINUE
C SUM OVERTURN MOMENT
365 DO 367 I=1, NSM1
IF(AREA(I).LE.SMLNO) P(I)=0.00
IF(AREA(I).LE.SMLNO) CO(I)=0.00
367 P(I)=P(I)/57.2928
FI=1.0
387 ZUM=0.0
TF=0.0
DO 382 K=1, NSM1
CENTR=(SLICX(K+1)-SLICX(K))/2.0+SLICX(K)
IF((CENTR-CX).LT.0.0) T=WEIGH(K)*SIN(ALPHA(K))
IF((CENTR-CX).EQ.0.0) T=0.0
IF((CENTR-CX).GT.0.0) T=WEIGH(K)*SIN(ALPHA(K))
IF(CENTR-GE.HAH) T=T+YAY*(SLICX(K+1)-SLICX(K))
394 TF=TF+T
IF((CENTR-CX).LT.0.0) A=-1.0*SIN(ALPHA(K))
A=SIN(ALPHA(K))
B(K)=(SLICX(K+1)-SLICX(K))/COS(ALPHA(K))
Z=(CO(K)*B(K)+EFFWT(K)*TAN(P(K)))/(COS(ALPHA(K))+TAN(P(K))*A/FI
382 ZUM=ZUM+Z
FO=ZUM/TF
WRITE(6, 116) FI, FO
116 FORMAT(20X, 'FI=', F10.5, 3X, 'FO=', F10.5)
IF(A3S(FI, FO).EQ.0) 385, 385, 383
385 WRITE(6, 108) NCOUN, FO
108 FORMAT('0', 15X, 'THE SAFETY FACTOR FOR POINT', I3, 'IS', F10.5)
GO TO 360
383 FI=FO
GO TO 387
389 IF(PCODE, EQ, 0 OR, R, GE, CY) GO TO 360
IF(NCOUN, GT, 1) GO TO 405
XAXIS=12.
YAXIS=9.
PSCALE=SCALE
DATA METER/'M'/
IF(UT, NE, METER) GO TO 405
XAXIS=15.
YAXIS=12.
PSCALE=SCALE*2
405 IF(NCOUN, NE, 1) AND (NCOUN/NP*NP, NE, NCOUN) AND NCOUN, NE, ITX*IT
&Y) GO TO 360
360 IF(IX, EQ, ITX) CX=CX+(IX-1)*DELX
STOP
END

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CHAPTER 5

RESULTS AND RECOMMENDATIONS

5.I RESULTS FROM THE COMPUTER PROGRAM

5.I.I Slope Stability Analysis For Existing Soil Profile

Results from the computer program and figures showing various cross-sections are given in figures and tables.

In cross-section (3-3)A, soil I is artificial fill, the thickness of these fills decreases with increasing distance from the shore. The artificial fill contains boulders, gravel, sand, silt, shells, wooden pieces, pieces of concrete, mortar and all kinds of city debris. The determination of engineering characteristics of such fills is very difficult. So soil parameters may be taken as : (Aras, 1978 and Unlü, 1982)

$$\gamma_n : 1.8 \text{ t/m}^3$$

$$\phi : 20^\circ$$

$$c : 2 \text{ t/m}^2$$

Soil II is a sedimentary layer. The sedimentary layers which are found under the artificial fill layer consists of sandy, clayey silts which contain large amount of organic matter and

shells.

To find characteristic parameters for such soils, we will make the following consideration accepting the soil to be normally consolidated. The value of ratio c_u/\bar{p} is found by the formula:

$$s_u/\bar{p} = 0.11 + 0.0037 PI$$

given by Skempton(1975), where s_u denotes the undrained shear strength at a depth where the effective overburden pressure is equal to \bar{p} . PI denotes the plasticity index. The average value of PI may be obtained from table 2.10 to be 35. When this average value is substituted in the equation, s_u/\bar{p} ratio is found as:

$$s_u/\bar{p} = 0.11 + 0.0037 \times 35$$

$$s_u/\bar{p} = 0.24$$

For various depths :

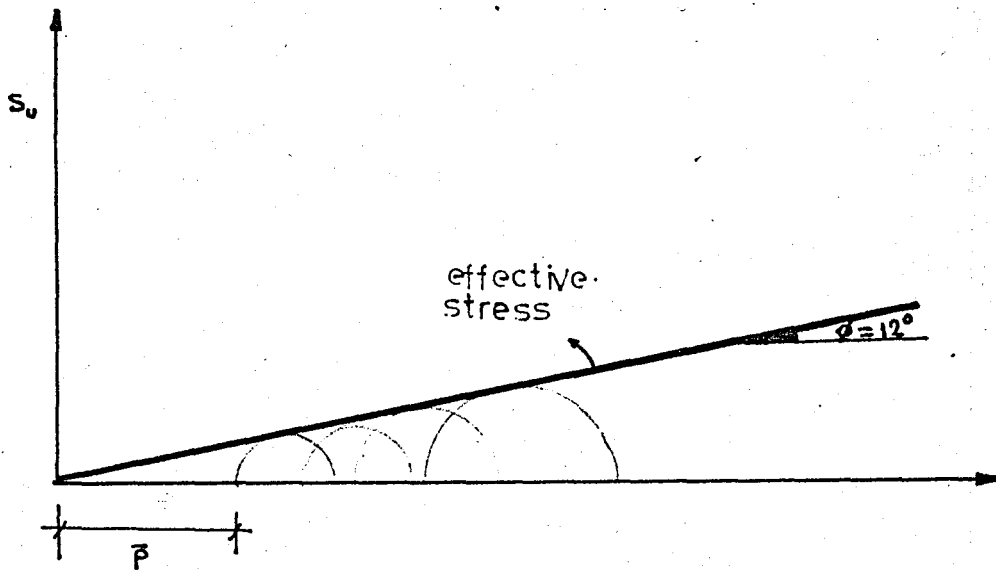
$$30m. \dots\dots\dots s_u = 0.24 \times 30 \times 0.8 = 5.76 \text{ t/m}^3$$

$$40m. \dots\dots\dots s_u = 0.24 \times 40 \times 0.8 = 7.68 \text{ t/m}^3$$

$$50m. \dots\dots\dots s_u = 0.24 \times 50 \times 0.8 = 9.60 \text{ t/m}^3$$

$$60m. \dots\dots\dots s_u = 0.24 \times 60 \times 0.8 = 11.52 \text{ t/m}^3$$

If we plot these values, we will obtain the angle of friction, $\phi = 12$ and the cohesion $c = 0$.

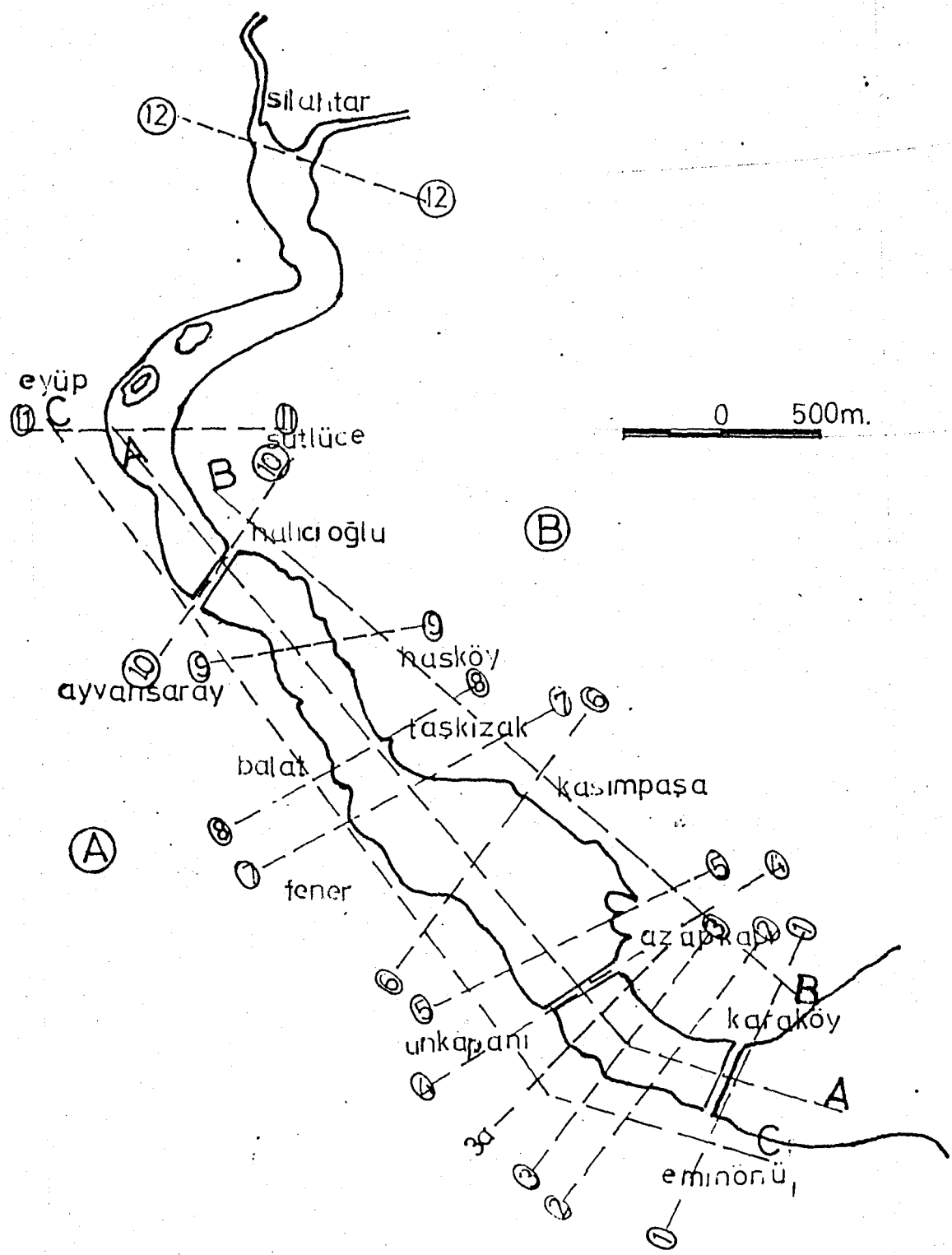


Soil III is decomposed graywacke. The engineering characteristics of this layer is given in table 2.2 .

As was stated before when a circle center and a entrance point is given as data to the computer program, it analysis further 8 potential failure circles by keeping the position of the entrance point constant , and changing the center of the circle in the X and Y directions. In the table only the slope circle which gives the minimum factor of safety for this set is given. So altogether $12 \times 9 = 108$ circles have been investigated.

If we run the computer program for cross-section (3-3)A , We will obtain the following results:

Circle NO	Circle center Coord		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	I22	I38	2I7	I05	I.73
b	84	II9	I34	I05	I.42
c	94	I26	I43	I05	I.60
d	I06	I25	I69	I05	2.00
e	89	I35	I5I	I05	I.50
f	II4	I47	202	I05	2.30
g	I06	I87	I6I	I05	2.10
h	95	I53	I97	I05	I.55
j	98	I35	I89	I05	I.50
k	80	I48	I80	I05	I.54
l	80	I28	I68	I05	I.52
m	73	II6	I55	I05	I.6I
w	6I	I30	I40	I05	I.60
o	74	I38	I52	I05	I.49
z	69	I25	I45	I05	I.6I
t	88	I25	I86	I05	I.30
r	I00	I04	I62	I05	I.56
p	84	I07	I45	I05	I.76
y	73	I03	I40	I05	I.40



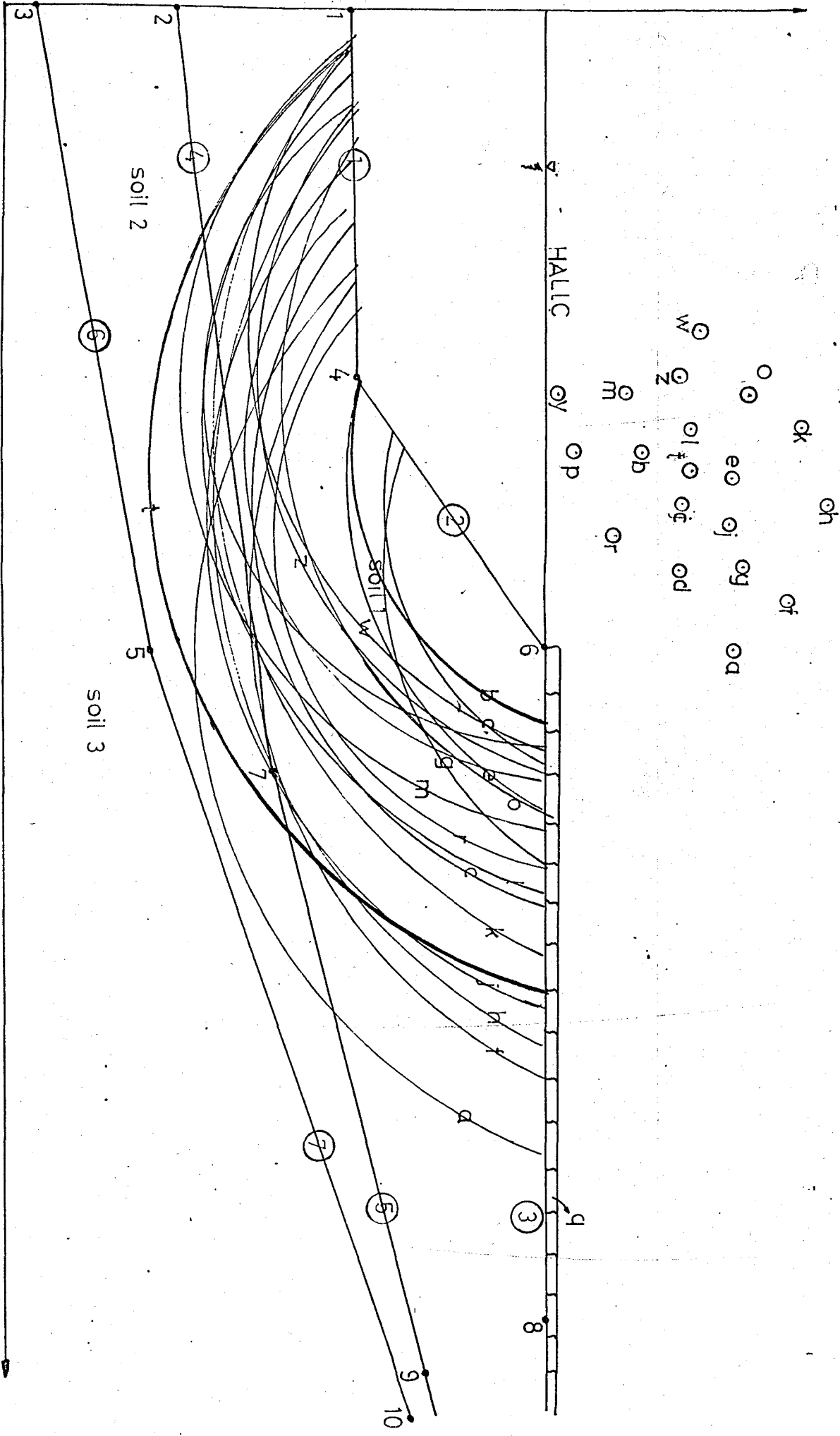


Fig : (3-3)A

5	67	78	99	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	13	077	58	976	K=	4	KK=	1
2	40	849	36	962	K=	5	KK=	2
3	70	111	67	111	K=	6	KK=	3
4	20	111	05	111	K=	8	KK=	4
5	43	111	54	111	K=	9	KK=	5
6	64	063	60	032	K=	0	KK=	6
7	86	111	05	111	K=	1	KK=	7

IND SLICE WIDTH AND NO OF SLICES

****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50

FI=	30000	FO=	25393
FI=	25393	FO=	29647
FI=	29647	FO=	30238
FI=	30238	FO=	30318

THE SAFETY FACTOR FOR POINT 3 IS 1.3038

TRIAL CIRCLE NO 2

CIRCLE CTR COORDS: X= 97.082 Y= 253.1

ENTRANCE PT COORDS: X= 86.41 Y= 205.1

TRIAL ARC RADIUS= 97.082

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

ARC NO	X	Y
1	97.232	59.85
4	47.947	38.52
5	162.836	59.69
3	185.111	05.11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	59	854	K=	1	KK=	1	
2	000	30	111	K=	1	KK=	2	
3	000	67	111	K=	2	KK=	3	
4	19	232	59	854	K=	3	KK=	3
5	47	947	38	52	K=	3	KK=	4
6	70	111	67	111	K=	3	KK=	5
7	15	077	38	52	K=	3	KK=	6
8	20	111	05	111	K=	3	KK=	7
9	43	111	54	111	K=	3	KK=	7
10	62	836	59	854	K=	4	KK=	7
11	86	111	05	111	K=	4	KK=	7
12	233	55	05	111	K=	4	KK=	9
13	235	111	05	111	K=	4	KK=	9
14	240	111	66	111	K=	4	KK=	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	19	232	59	854	K=	4	KK=	1
2	47	947	38	52	K=	5	KK=	2

567
 432836
 547116
 595686
 75511
 K= 9
 K= 7
 K= 1
 KK= 5
 KK= 6
 KK= 7

ND SLICE WIDTH AND NO OF SLICES

***MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI= 00000 FO= 25872
 FI= 25872 FO= 30167
 FI= 30167 FO= 30777
 FI= 30777 FO= 30860

THE SAFETY FACTOR FOR POINT 2 IS 1.30860

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= X= 887.1 Y= 128.11
 TRIANGLE PT COORDS: X= 86.7 Y= 105.11
 TRIAL ARC RADIUS= 100.663

X LINE 2 NOT INTERSECTED BY TRIAL CIRCLE

X LINE 6 NOT INTERSECTED BY TRIAL CIRCLE

X LINE 7 NOT INTERSECTED BY TRIAL CIRCLE

*LINE 2 IS NOT INTERSECTED BUT IS IN ARC

C INTERSECT WITH LINE ARRAY

NO	X	Y
14	723	59721
44	211	37753
161	622	59734
186	111	05711

E ARRAY WITH ALL INTERSECTIONS FOLLOWS:

NO	X	Y	K	KK
1	000	57711	1	1
2	000	30711	1	2
3	000	111	1	3
4	14723	59721	2	3
5	44211	37753	3	3
6	70000	67711	3	4
7	11511	28711	3	5
8	12000	05711	3	6
9	14300	54711	3	7
10	161622	59734	4	7
11	186111	05711	4	8
12	000	05711	4	9
13	23300	80711	4	9
14	24000	66711	4	0

E APPLICABLE ARRAY ARC INT FOLLOWS:

NO	X	Y	K	KK
1	14723	59721	4	1
2	44211	37753	5	2
3	70000	67711	6	3
4	12000	05711	8	4
5	14300	54711	9	5
6	161622	59734	0	6
7	186111	05711	1	7

ND SLICE WIDTH AND NO OF SLICES

***MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI= 00000 FO= 24727
 FI= 24727 FO= 28123
 FI= 28123 FO= 28575
 FI= 28575 FO= 28750

THE SAFETY FACTOR FOR POINT 3 IS 1.28750

In cross-section(3-3) B soil types are given as:

Soil I : Artificial Fill

Soil II : Sedimentary Layer

Soil III : Decomposed Graywacke

The results taken from the computer for cross-section(3-3) B are:

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	I05	I48	I83	I07	I.29
b	96	I39	I60	I07	I.65
c	I06	I39	I67	I07	I.80
d	II7	I46	I73	I07	2.20
e	99	I46	I8I	I07	I.I3
f	III	I55	I88	I07	I.36
h	I27	I49	200	I07	I.50
j	II9	I63	I88	I07	2.I2
k	86	I4I	I80	I07	I.I2
l	83	I50	I74	I07	I.I9
m	82	I6I	I92	I07	I.35
n	95	I60	I89	I07	I.II6

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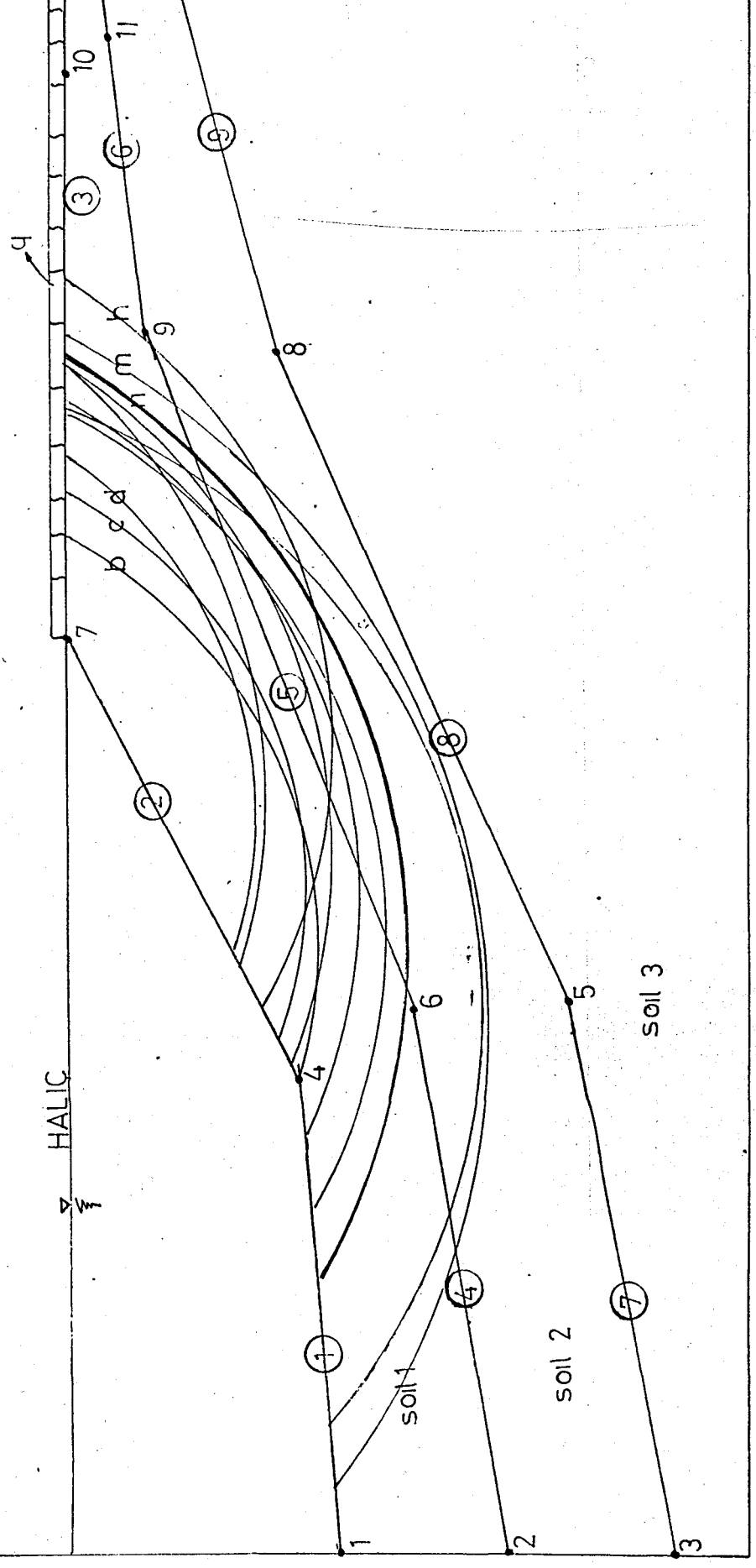


Fig: (3-3)B

OF LINES 9 NO OF LINE INTERSECT= 12
 OF SOILS= 3 NO OF EXTERNAL SOIL LINES= 3
 OF X INCREMENTS= 2 NO OF Y INCREMENTS= 2
 INITIAL SLICE WIDTH= 200

LINE NO	END NO	COORD INT	X1	Y1	X2	Y2	SLOPE	LINE INTER
1	2	00	74	64	74	69	674664	1
2	3	00	44	69	44	07	542857	4
3	4	00	44	77	233	07	000000	7
4	5	00	86	36	86	50	162558	2
5	6	00	94	50	94	07	407407	6
6	7	00	84	10	237	27	162791	9
7	8	00	84	27	84	73	202114	3
8	9	00	88	73	88	90	442308	5
9					244		30357	8

LINE NO	X	Y
1	00	64
2	00	36
3	00	69
4	74	69
5	84	50
6	86	50
7	144	107
8	188	73
9	194	94
10	233	107
11	237	101
12	244	90

LINE NO	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESION
1	4	4	0	7.8	20.0	19.6
2	7	7	0	7.8	20.0	19.6
3	2	6	0	7.8	20.0	19.6
4	6	9	0	7.8	20.0	19.6
5	9	4	0	7.8	20.0	19.6
6	6	5	0	7.8	12.0	0.0
7	9	3	0	7.8	12.0	0.0
8	3	5	0	7.8	12.0	0.0
9	8	2	0	7.8	12.0	0.0
10	3	5	0	3.3	45.0	18.6
11	3	5	0	3.3	45.0	18.6
12	8	2	0	3.3	45.0	18.6

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X= 95.1 Y= 60.1
 TANGENT PT COORDS: X= 89.1 Y= 60.7
 TRIAL ARC RADIUS= 107.9

- X LINE 2 NOT INTERSECTED BY TRIAL CIRCLE
- X LINE 4 NOT INTERSECTED BY TRIAL CIRCLE
- X LINE 6 NOT INTERSECTED BY TRIAL CIRCLE
- X LINE 7 NOT INTERSECTED BY TRIAL CIRCLE
- X LINE 8 NOT INTERSECTED BY TRIAL CIRCLE

*LINE 9 NOT INTERSECTED BY TRIAL CTRCL

*LINE 2 IS NOT INTERSECTED BUT IS IN ARC

C INTERSECT WITH LINE ARRAY

CE NO	X	Y
40	798	66
91	393	52
73	137	85
89	137	07

E ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK	LINE NO
1	0000	64	1	KK	1
2	0000	36	1	KK	2
3	0000	10	1	KK	3
4	798	66	2	KK	4
5	74	69	2	KK	5
6	84	27	2	KK	6
7	86	50	2	KK	7
8	91	52	3	KK	8
9	44	07	3	KK	9
10	73	85	4	KK	10
11	88	73	4	KK	11
12	89	07	4	KK	12
13	94	07	4	KK	13
14	33	00	4	KK	14
15	23	00	4	KK	15
16	24	00	4	KK	16

E APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK	LINE NO
1	40	798	4	KK	1
2	74	69	5	KK	2
3	91	393	8	KK	3
4	44	07	9	KK	4
5	73	85	0	KK	5
6	89	07	2	KK	6

ND SLICE WIDTH AND NO OF SLICES

***MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50

FI	FO
00000	0345
0345	1504
1504	1623
1623	1635

THE SAFETY FACTOR FOR POINT T IS 1.1635

TRIAL CIRCLE NO 2

CIRCLE CTR COORDS: X= 98 Y= 60

ORIG PT COORDS: X= 89 Y= 07

TRIAL ARC RADIUS= 105.309

*LINE 2 NOT INTERSECTED BY TRIAL CTRCL

*LINE 4 NOT INTERSECTED BY TRIAL CTRCL

*LINE 6 NOT INTERSECTED BY TRIAL CTRCL

*LINE 7 NOT INTERSECTED BY TRIAL CTRCL

*LINE 8 NOT INTERSECTED BY TRIAL CTRCL

*LINE 9 NOT INTERSECTED BY TRIAL CTRCL

*LINE 2 IS NOT INTERSECTED BUT IS IN ARC

C INTERSECT WITH LINE ARRAY

NO X Y
 48 230 67 36
 97 228 54 38
 172 404 85 42
 189 1 07 1

ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 1 0000 64 1 1 KK= 1
 2 0000 36 1 1 KK= 2
 3 0000 10 1 1 KK= 3
 4 230 67 2 2 KK= 4
 5 74 11 2 2 KK= 5
 6 84 11 2 2 KK= 6
 7 86 11 2 2 KK= 7
 8 97 22 3 3 KK= 8
 9 44 11 3 3 KK= 9
 10 72 04 4 4 KK= 10
 11 88 11 4 4 KK= 11
 12 89 11 4 4 KK= 12
 13 94 11 4 4 KK= 13
 14 233 07 4 4 KK= 14
 15 337 07 4 4 KK= 15
 16 244 90 4 4 KK= 16

APPLICABLE ARRAY ARC INT FOLLOWS:
 1 48 230 67 36 4 KK= 1
 2 74 11 69 11 5 KK= 2
 3 97 22 54 38 8 KK= 3
 4 44 11 07 11 9 KK= 4
 5 72 04 85 42 7 KK= 5
 6 89 11 07 1 2 KK= 6

SLICE WIDTH AND NO OF SLICES
 FI= 00000 FO= 1025
 FI= 1025 FO= 224
 FI= 224 FO= 2363
 FI= 2363 FO= 2375

THE SAFETY FACTOR FOR POINT 2IS 1.12375

AL CIRCLE NO 3
 CLE CTR COORDS: X= X= 95.7 Y= 63.1
 RANCE PT. COORDS: X= 89.7 Y= 07.1
 TRIAL ARC RADIUS= 109.47

LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 LINE 2IS NOT INTERSECTED BUT IS IN ARC

INTERSECT WITH LINE ARRAY
 NO X Y
 42 817 67 00
 94 907 53 69
 171 720 84 99
 189 1 07 1

ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 1 0000 64 1 1 KK= 1

4	000	107	67	000	K=	1	KK=	3
5	42	817	67	000	K=	2	KK=	4
6	74	111	69	000	K=	2	KK=	5
7	84	111	27	000	K=	2	KK=	6
8	86	111	50	000	K=	2	KK=	6
9	94	907	53	695	K=	3	KK=	6
10	44	111	07	111	K=	3	KK=	7
11	77	720	84	989	K=	4	KK=	8
12	88	111	73	111	K=	4	KK=	8
13	189	111	07	111	K=	4	KK=	8
14	194	111	94	111	K=	4	KK=	9
15	233	111	07	111	K=	4	KK=	0
16	237	111	00	111	K=	4	KK=	1
	244	111	90	111	K=	4	KK=	2

THE APPLICABLE ARRAY ARC INT FOLLOWS:

1	42	817	67	000	K=	4	KK=	1
2	74	111	69	000	K=	5	KK=	2
3	94	907	53	695	K=	8	KK=	3
4	44	111	07	111	K=	9	KK=	4
5	77	720	84	989	K=	0	KK=	5
6	88	111	07	111	K=	2	KK=	6

IND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI=	00000	FO=	1353
FI=	1353	FO=	2597
FI=	2597	FO=	2720
FI=	2720	FO=	2733

THE SAFETY FACTOR FOR POINT 3IS 1.12733

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= X= 987.7 Y= 63.1
 ENTRANCE PT. COORDS: X= 89.7 Y= 07.1
 TRIAL ARC RADIUS= 106.850

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCLE
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCLE
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCLE
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCLE
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCLE
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCLE
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

ARC NO	X	Y
1	50.387	67.51
5	101.324	56.31
5	170.448	84.47
3	189.11	07.1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	64	111	K=	1	KK=	1	
2	000	36	111	K=	1	KK=	2	
3	000	10	111	K=	1	KK=	3	
4	50	387	67	510	K=	3	KK=	3
5	74	111	69	000	K=	2	KK=	4
6	84	111	27	000	K=	2	KK=	5
7	86	111	50	000	K=	2	KK=	6
8	0	324	56	309	K=	3	KK=	6

I=	10	70	84	K=	4	KK=	7
I=	11	88	73	K=	4	KK=	8
I=	12	99	07	K=	4	KK=	9
I=	13	44	94	K=	4	KK=	0
I=	14	33	07	K=	4	KK=	1
I=	15	37	00	K=	4	KK=	2
I=	16	24	90	K=	4	KK=	

THE APPLICABLE ARRAY ARC INT FOLLOWS:

I=	1	50	67	K=	4	KK=	1
I=	2	33	55	K=	5	KK=	2
I=	3	11	11	K=	8	KK=	3
I=	4	32	30	K=	9	KK=	4
I=	5	44	11	K=	0	KK=	5
I=	6	70	44	K=	2	KK=	6
I=		89	07	K=		KK=	

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	2758
FI=	2758	FO=	434
FI=	434	FO=	4267
FI=	4267	FO=	4280

THE SAFETY FACTOR FOR POINT 4 IS 1.14280

RPRT PRINT#

The results taken from the computer program for cross-section
(4-4) A are:

Circle NO	Circle Center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	85	115	137	85	1.83
b	92	111	150	85	1.40
c	86	110	139	85	1.83
d	92	117	163	85	1.21
e	107	119	174	85	1.71
f	77	119	134	85	1.74
g	81	112	130	85	1.83
h	83	127	144	85	1.80
i	101	115	180	85	1.35
j	74	104	140	85	1.20
k	68	118	154	85	1.16

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ek f^o g^o h^o i^o j^o
ek f^o g^o h^o i^o j^o
ek f^o g^o h^o i^o j^o

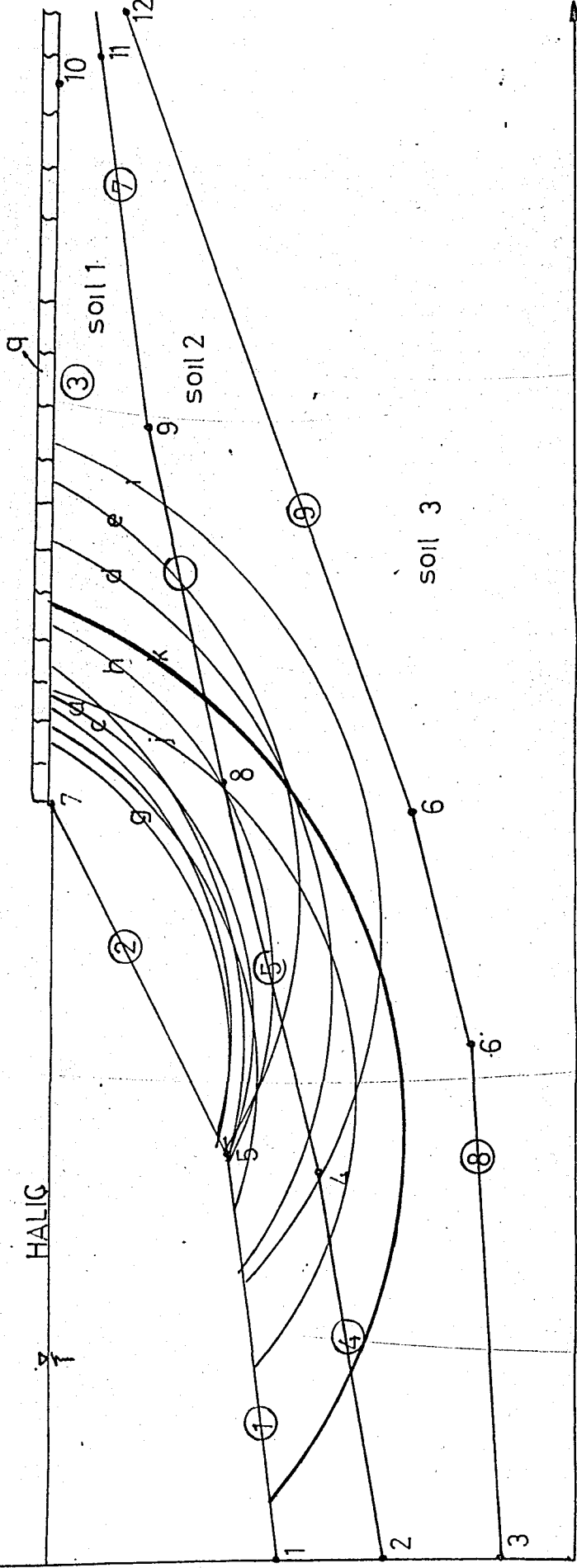


Fig : (4-4) A

OF LINES 9 NO OF LINE INTERSECT= 12
 OF SOILS= 3 NO OF EXTERNAL SOIL LINES= 3
 OF X INCREMENTS= 3 NO OF Y INCREMENTS= 3
 INITIAL SLICE WIDTH= 2.0

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INTER
1	2	00	53	49	63	55	950706	1
2	3	00	22	55	23	85	7241	5
3	4	00	11	85	39	85	000000	7
4	5	00	00	32	26	41	47273	2
5	6	00	65	45	25	57	50000	4
6	7	00	25	57	28	69	4286	8
7	8	00	89	69	40	77	55593	9
8	9	00	50	13	24	25	999076	3
9	20	00	20	25	24	73	393443	6

LINE INTERSECT ARRAY

LINE NO	X	Y
1	00	49
2	00	33
3	00	23
4	61	41
5	30	55
6	22	55
7	11	85
8	22	57
9	88	69
10	00	57
11	23	85
12	42	77
13	00	73

SOIL DATA ARRAY

LINE NO	LEFT INT	PT INT	SAT	UNIT WT	PHI	COHESION
1	5	5	00	78	20	19
2	7	0	00	78	20	19
3	2	4	00	78	20	19
4	8	8	00	78	20	19
5	9	1	00	78	20	19
6	4	4	00	78	22	19
7	8	8	00	78	12	00
8	9	1	00	78	12	00
9	4	4	00	78	12	00
10	6	6	00	78	12	00
11	2	2	00	78	12	00
12	3	3	00	78	45	68
13	6	2	00	77	45	68

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X= 68.117 Y= 18.111
 ORIGIN PT COORDS: X= 54.111 Y= 85.111
 TRIAL ARC RADIUS= 92.114

- X LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- X LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- X LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- X LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- X LINE 9 NOT INTERSECTED BY TRIAL CIRCL

LINE 5 IS NOT INTERSECTED BUT IS IN ARC

INTERSECT WITH LINE ARRAY

NO	X	Y
6	405	49772
26	374	36700
139	790	60226
154	111	85111

ARRAY WITH ALL INTERSECTIONS FOLLOWS:

NO	X	Y	K	KK
1	000	49772	1	1
2	000	32771	1	1
3	000	13771	1	1
4	6405	49772	2	3
5	63374	35599	3	3
6	63374	44995	3	3
7	63374	55111	3	3
8	22011	25111	3	3
9	22011	85111	3	3
10	22599	57111	3	3
11	22599	60226	4	4
12	23979	85111	4	4
13	23979	69111	4	4
14	23979	85111	4	4
15	24011	77111	4	4
16	24211	73111	4	4

APPLICABLE ARRAY ARCINT FOLLOWS:

NO	X	Y	K	KK
1	6405	49772	4	1
2	63374	35599	5	2
3	63374	44995	6	3
4	63374	55111	7	4
5	22011	25111	9	5
6	22011	85111	10	6
7	22599	57111	11	7
8	23979	60226	12	8

AND SLICE WIDTH AND NO OF SLICES

***MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI	FO
18874	18874
21567	21567
21898	21898
21938	21938

THE SAFETY FACTOR FOR POINT IS 1.21938

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 72711 Y= 18311
 ORIGIN PT COORDS: X= 54711 Y= 85311
 TRIAL ARC RADIUS= 88391

X LINE 2 NOT INTERSECTED BY TRIAL CIRCL

X LINE 5 NOT INTERSECTED BY TRIAL CIRCL

X LINE 7 NOT INTERSECTED BY TRIAL CIRCL

X LINE 8 NOT INTERSECTED BY TRIAL CIRCL

X LINE 9 NOT INTERSECTED BY TRIAL CIRCL

*LINE 2 IS NOT INTERSECTED BUT IS IN ARC

*LINE 5 IS NOT INTERSECTED BUT IS IN ARC

INTERSECT WITH LINE ARRAY

LINE NO	X	Y	LINE NO	X	Y
1	50	75	5	75	50
2	37	42	6	42	37
3	60	03	7	03	60
4	85	11	8	11	85

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	LINE NO	X	Y	K	K
1	50	75	4	75	50	1	1
2	32	11	5	11	32	1	1
3	13	44	6	44	13	1	1
4	50	48	7	48	50	2	2
5	37	18	8	18	37	3	3
6	4	11	9	11	4	3	3
7	55	55	10	55	55	3	3
8	25	57	11	57	25	3	3
9	57	60	12	60	57	3	3
10	60	32	13	32	60	4	4
11	85	5	14	5	85	4	4
12	5	69	15	69	5	4	4
13	38	7	16	7	38	4	4
14	4	11	17	11	4	4	4
15	22	39	18	39	22	4	4
16	24	42	19	42	24	4	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	LINE NO	X	Y	K	K
1	50	75	4	75	50	4	4
2	37	42	5	42	37	5	5
3	60	03	6	03	60	6	6
4	85	11	7	11	85	7	7
5	57	60	8	60	57	9	9
6	60	32	9	32	60	0	0
7	85	5	10	5	85	1	1
8	5	69	11	69	5	2	2

IND SLICE WIDTH AND NO OF SLICES

FILE	NO	FO
FILE	16084	FO= 6084
FILE	18404	FO= 8404
FILE	18694	FO= 8694
FILE	1873	FO= 873

THE SAFETY FACTOR FOR POINT 2IS 1.18731

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 76.511 Y= 18.11
 ENTRANCE PT. COORDS: X= 84.694 Y= 85.11
 TRIAL ARC RADIUS= 84.694

XX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 **LINE 2 IS NOT INTERSECTED BUT IS IN ARC
 **LINE 5 IS NOT INTERSECTED BUT IS IN ARC

RC INTERSECT WITH LINE ARRAY

LINE NO	X	Y	LINE NO	X	Y
1	23	948	5	38	39
4	46	124	6	59	77
6	137	522	8	85	1
3	154	111			

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	49	1	KK	1
2	000	32	1	KK	2
3	000	33	1	KK	3
4	000	13	2	KK	4
5	948	55	3	KK	5
6	224	38	3	KK	6
7	111	90	3	KK	7
8	111	55	3	KK	8
9	111	57	3	KK	9
0	111	59	4	KK	0
1	111	57	4	KK	1
2	111	85	4	KK	2
3	111	77	4	KK	3
4	111	73	4	KK	4

THE APPLICABLE ARRAY ARC INT FOLLOWS:

1	23	5	3	388	4	KK	1
2	46	3	8	904	5	KK	2
3	6	4	1	111	6	KK	3
4	6	5	5	111	7	KK	4
5	3	5	5	111	9	KK	5
6	3	5	7	111	0	KK	6
7	3	5	7	66	1	KK	7
8	5	5	7	66	1	KK	8

FIND SLICE WIDTH AND NO OF SLICES

FILE	00000	FO	4429
FILE	4429	FO	6527
FILE	6527	FO	6798
FILE	6798	FO	6833

THE SAFETY FACTOR FOR POINT 31S T₁ 6833

TRIAL CIRCLE NO 4
 TRIAL CTR COORDS: X= 68.7 Y= 22.17
 ENTRANCE PT COORDS: X= 54.4 Y= 85.11
 TRIAL ARC RADIUS= 93.622

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

***LINE 5 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
8	50.1	49.92
30	11.5	36.55
138	06.1	59.89
154	11.1	85.41

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	49	1	KK	1
2	000	32	1	KK	2
3	000	13	2	KK	3
4	8.501	49.919	2	KK	3

In cross-section (4-4) B soil types are given as :

Soil I : Artificial fill

Soil II : Sedimentary Layer

Soil III: Decomposed Graywacke

The results taken from the computer for cross-section

(4-4) B are :

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	x	Y	x	Y	
a	85	I23	I42	90	I.90
b	82	II6	I35	90	I.94
c	99	II8	I59	90	I.60
d	89	II7	I50	90	I.I6
e	85	II2	I28	90	2.00
f	79	I23	I32	90	I.85
g	I05	I28	I59	90	I.95
h	92	I4I	I69	90	I.I8
j	72	II0	I37	90	I.I6
k	66	I27	I45	90	I.I4

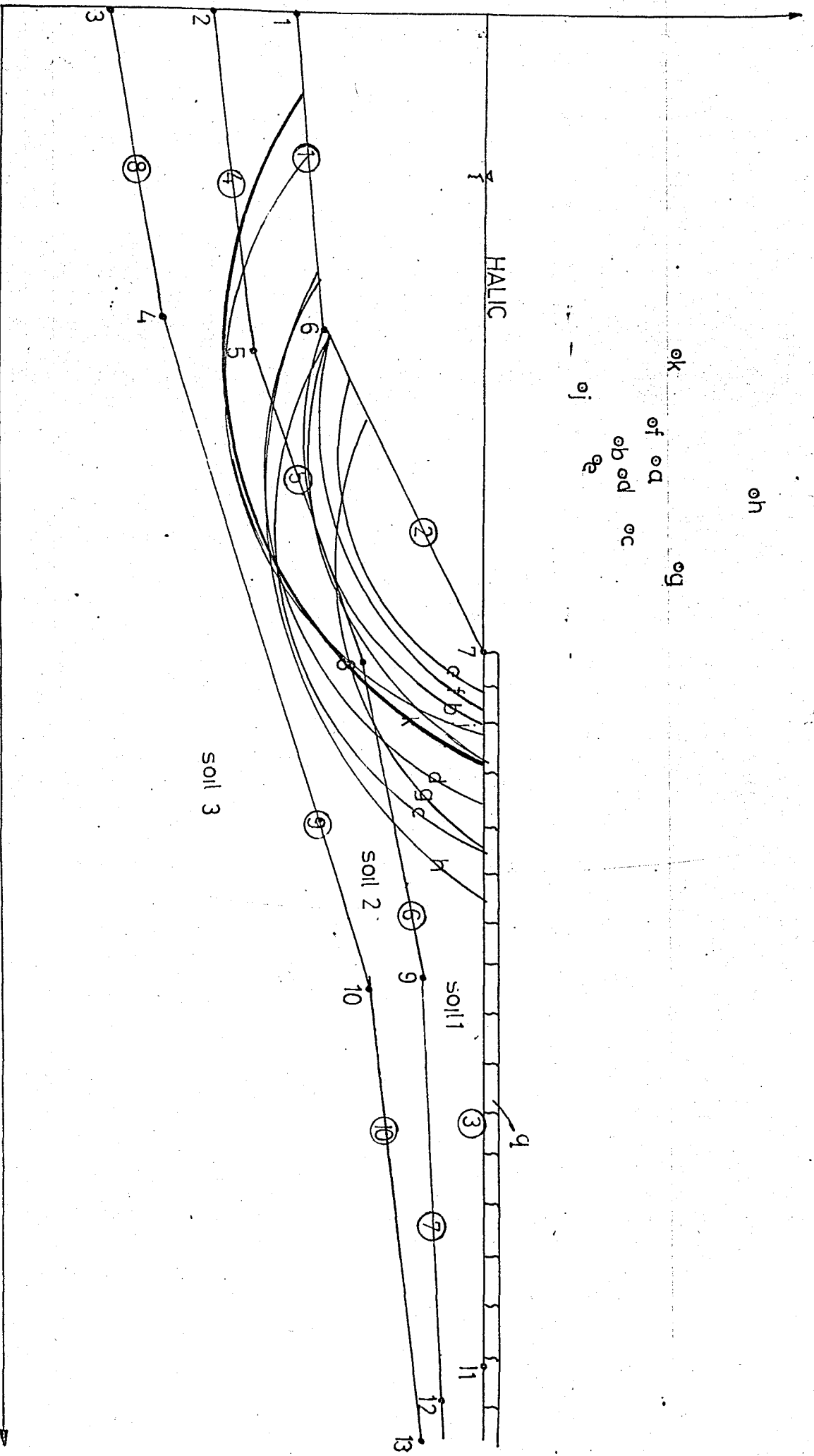


Fig : (4-4) B

NO OF LINES = 10 NO OF LINE INTERSECT = 13
 NO OF SOILS = 3 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 3 NO OF Y INCREMENTS = 3
 INITIAL SLICE WIDTH = 200

LINE NO	END NO	COORD. INT	MATRIX	Y1	X2	Y2	SLOPE	LINE INTE
1	2	00	00	55	60	60	83	1
2	3	00	00	60	60	90	49	7
3	4	00	00	90	60	90	18	2
4	5	00	00	40	60	46	00	5
5	6	00	00	46	67	67	15	8
6	7	00	00	67	67	79	28	9
7	8	00	00	79	67	82	06	3
8	9	00	00	20	67	30	11	4
9	10	00	00	30	69	82	17	6
10	11	00	00	69	23	80	57	10

LINE NO	INTERSECT X	Y
1	00	55
2	00	60
3	00	90
4	57	40
5	59	46
6	60	67
7	67	67
8	12	90
9	18	67
10	22	79
11	25	69
12	27	82
13	30	80

SOIL NO	LINE #	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESION
1	2	6	7	00	78	20	19
1	3	7	7	00	88	20	19
1	4	2	7	00	88	20	19
1	5	5	7	00	88	20	19
1	6	8	7	00	88	20	19
1	7	9	7	00	88	20	19
1	8	9	7	00	88	20	19
1	9	2	7	00	88	12	00
1	10	3	7	00	88	12	00
1	11	4	7	00	88	12	00
1	12	4	7	00	88	12	00
1	13	3	7	00	77	45	68
1	14	3	7	00	77	45	68
1	15	4	7	00	77	45	68

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X = 66 Y = 27
 ENTRANCE PT COORDS: X = 45 Y = 90
 TRIAL ARC RADIUS = 87.235

- XX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

**LINE 2 IS NOT INTERSECTED BUT IS IN ARC

**LINE 5 IS NOT INTERSECTED BUT IS IN ARC

RC INTERSECT WITH LINE ARRAY

RC NO	X	Y
24	316	57
52	237	45
29	751	68
45	111	90

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	55	1	1
2	000	40	1	2
3	000	20	1	3
4	316	57	2	3
5	237	45	3	3
6	111	30	3	4
7	111	46	3	5
8	111	60	3	6
9	111	90	3	7
10	229	67	3	8
11	229	68	4	8
12	451	90	4	8
13	111	79	4	9
14	111	69	4	9
15	229	90	4	9
16	229	82	4	9
17	230	80	4	9

THE APPLICABLE ARRAY ARC INT FOLLOWS:

LINE NO	X	Y	K	KK
1	24	316	4	1
2	52	237	5	2
3	59	111	7	3
4	60	111	8	4
5	229	111	9	5
6	229	751	10	6
7	45	111	11	7
8	45	111	12	8

FIND SLICE WIDTH AND NO OF SLICES

FI	FO
0000	1946
1946	3620
3620	3832
3832	3858

THE SAFETY FACTOR FOR POINT 2 IS 1.13858

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 74.7 Y= 27.1
 ENTRANCE PT. COORDS: X= 45.1 Y= 90.1
 TRIAL ARC RADIUS= 87.062

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC LINE NO	INTERSECT WITH	X	Y
5	33	822	57.92
6	63	944	47.70
3	123	315	68.99
	145	111	90.91

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE	X	Y	K	KK
2	000	000	1	1
3	000	000	1	1
4	000	000	1	1
5	33	822	2	3
6	63	944	2	4
7	123	315	2	5
8	145	111	2	6
9	000	000	3	7
10	000	000	3	8
11	000	000	3	8
12	000	000	4	9
13	000	000	4	9
14	000	000	4	9
15	000	000	4	9
16	000	000	4	9
17	000	000	4	9

THE APPLICABLE ARRAY ARC INT FOLLOWS:

LINE	X	Y	K	KK
2	33	822	4	1
3	63	944	7	2
4	123	315	8	3
5	145	111	9	4
6	000	000	11	5
7	000	000	12	6

FIND SLICE WIDTH AND NO OF SLICES

FO	FI
2695	2695
4467	4467
4689	4689
4716	4716

THE SAFETY FACTOR FOR POINT 3 IS 1.14716

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= 66.111 Y= 131.111
 ENTRANCE PT COORDS: X= 45.777 Y= 90.911
 TRIAL ARC RADIUS= 89.006

- XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC
 ***LINE 5 IS NOT INTERSECTED BUT IS IN ARC

INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	7481	5657
2	44904	4467
3	129254	6838
4	14511	901

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K
1	7481	5657	3
2	44904	4467	3
3	129254	6838	3
4	14511	901	3
5	17481	5657	3
6	44904	4467	3
7	59254	4667	3
8	60111	6038	3
9	223254	901	3
10	229254	6738	3
11	229254	6838	3
12	229254	901	3
13	229254	6738	3
14	229254	6838	3
15	229254	901	3
16	229254	6738	3
17	229254	6838	3
18	229254	901	3

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K
1	7481	5657	4
2	44904	4467	5
3	59254	4667	7
4	60111	6038	8
5	223254	901	9
6	229254	6738	0
7	229254	6838	0
8	229254	901	2

FIND SLICE WIDTH AND NO OF SLICES

FI	FO
00000	2465
2465	4477
4477	4389
4389	4415

THE SAFETY FACTOR FOR POINT 4IS 1.1445

TRIAL CIRCLE NO 5
 CIRCLE CTR COORDS: X= 705.4 Y= 317.1
 ENTRANCE PT. COORDS: X= 145.4 Y= 90.1
 TRIAL ARC RADIUS= 85.475

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	25921	5735
5	59254	4628
6	27358	6809
3	14511	901

In cross-section (8-8) A soil types are given as :

Soil I is Bottom Sludge? It has been determined that it is formed by sedimentation of eroded materials and pollutant in water. The engineering characteristics has been taken as :

n : 1.15 t/m³

c : 12

e : 0

Soil II : Artificial Fill

Soil III : Sedimentary Layer

Soil 4 : Decomposed Graywacke

The results taken from the computer for cross-section (8-8)A are

Circle NO	Circle Center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	86	III	I35	8I	1.18
b	83	I05	II8	8I	1.14
c	9I	I08	I24	8I	1.50
d	98	I23	I65	8I	1.60
e	I0I	II3	I53	8I	1.60
f	84	I20	I27	8I	1.14
g	82	93	I33	8I	1.30
m	72	I08	I36	8I	1.24
n	74	II7	I36	8I	1.13
p	8I	I28	I57	8I	1.35

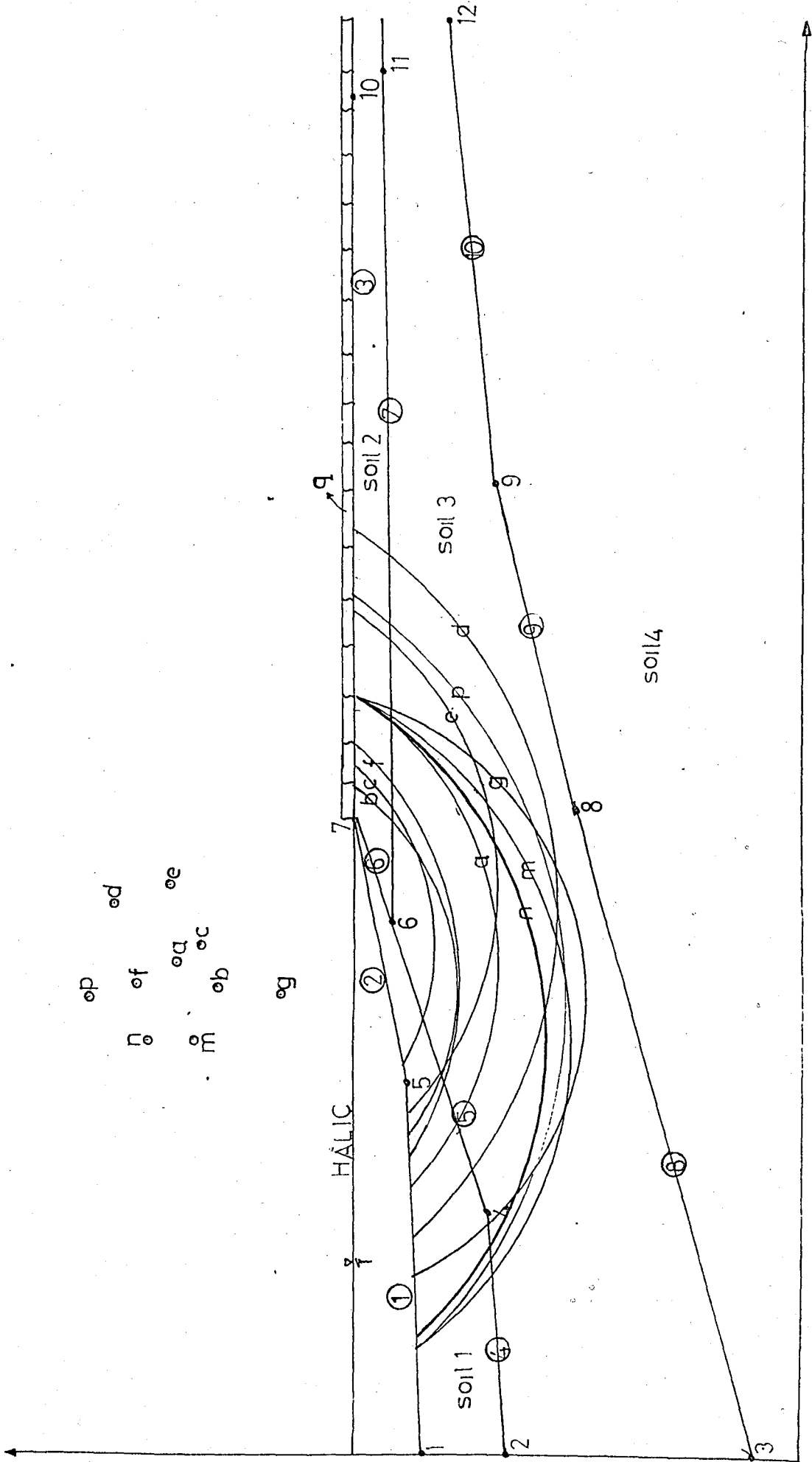


Fig : (8-8) A

SLOPE STABILITY FOR TASKIZAK(I) MAHIR KOSELER THESIS

NO OF LINES = 10 NO OF LINE INTERSECT = 12
 NO OF SOILS = 4 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 3 NO OF Y INCREMENTS = 3
 INITIAL SLICE WIDTH = 2.0

LINE COORD MATRIX

LINE NO	END NO	COORD X	COORD Y	X2	Y2	SLOPE	LINE INT
1	2	55	68	65	78	460	1
2	3	13	78	33	88	752	1
3	4	40	55	40	88	333	1
4	5	95	74	53	99	333	1
5	6	95	74	95	88	665	1
6	7	15	8	22	40	204	1
7	8	75	54	44	82	204	1
8	9			55	66	665	1
9	10			24	66	333	1

LINE INTERSECT ARRAY

LINE NO	X	Y
1	00	68
2	00	53
3	00	88
4	40	55
5	66	71
6	99	74
7	33	81
8	33	41
9	77	54
10	22	88
11	44	77
12	22	66

SOIL DATA ARRAY

SOIL NO	LINE #	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESION
1	2	5	5	0	1.5	22	0
1	3	7	7	0	1.5	22	0
1	4	2	4	0	1.5	22	0
1	5	6	6	0	1.5	22	0
1	6	6	6	0	1.5	22	0
1	7	7	7	0	1.5	22	0
1	8	6	6	0	1.5	22	0
1	9	6	6	0	1.5	22	0
1	10	9	9	0	1.5	22	0
2	8	3	3	0	1.3	45	68
2	9	3	3	0	1.3	45	68
2	10	3	3	0	1.3	45	68

TRIAL CIRCLE NO 1
 CENTER COORDS: X = 84.27 Y = 11.1
 TRIAL ARC RADIUS = 58.052

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC
 ***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 INFO NO X Y
 1 53 8 16 70 59
 5 67 36 7 64 53
 7 120 17 1 74 62
 3 127 1 1 8 1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 I= 2 0000 88 1 1 1 1 K= 1 KK= 1
 I= 3 0000 53 1 1 1 1 K= 1 KK= 2
 I= 4 0000 8 1 1 1 1 K= 1 KK= 3
 I= 5 40 1 1 1 1 55 1 1 1 1 K= 1 KK= 4
 I= 6 53 8 16 70 59 7 1 1 1 1 K= 2 KK= 4
 I= 7 67 36 7 64 53 7 1 1 1 1 K= 2 KK= 5
 I= 8 95 5 1 1 1 74 62 8 1 1 1 1 K= 3 KK= 6
 I= 9 113 1 1 1 1 8 1 1 1 1 K= 3 KK= 7
 I= 10 120 17 1 74 62 4 1 1 1 1 K= 3 KK= 8
 I= 11 127 1 1 74 62 8 1 1 1 1 K= 4 KK= 8
 I= 12 27 5 1 1 1 8 1 1 1 1 K= 4 KK= 9
 I= 13 24 0 1 1 1 8 1 1 1 1 K= 4 KK= 10
 I= 14 27 5 1 1 1 54 1 1 1 1 K= 4 KK= 11
 I= 15 24 0 1 1 1 8 1 1 1 1 K= 4 KK= 12
 I= 16 24 4 1 1 1 66 1 1 1 1 K= 4 KK= 12

THE APPLICABLE ARRAY ARC INT FOLLOWS:
 I= 1 53 8 16 70 59 K= 5 KK= 1
 I= 2 67 36 7 64 53 K= 6 KK= 2
 I= 3 67 36 7 64 53 K= 7 KK= 3
 I= 4 95 5 1 1 1 74 62 K= 8 KK= 5
 I= 5 113 1 1 1 1 8 1 1 1 1 K= 9 KK= 5
 I= 6 120 17 1 74 62 K= 11 KK= 6
 I= 7 127 1 1 74 62 K= 12 KK= 7

FIND SLICE WIDTH AND NO OF SLICES
 FI= 1.00000 F0= 1.3258
 FI= 1.3258 F0= 1.4675
 FI= 1.4675 F0= 1.4811
 FI= 1.4811 F0= 1.4823

THE SAFETY FACTOR FOR POINT IS 1.14823

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 88.27 Y= 120.51
 ENTRANCE PT COORDS: X= 88.27 Y= 120.51
 TRIAL ARC RADIUS= 55.754

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	52.983	74.601
2	73.958	66.800
3	119.266	74.460
4	127.111	8.241

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	0.000	68.111	1	1
2	0.000	53.811	1	1
3	0.000	8.241	1	1
4	40.111	55.711	1	1
5	52.983	74.601	2	2
6	55.511	77.111	2	2
7	73.958	66.800	3	3
8	95.111	74.601	3	3
9	113.111	8.241	3	3
10	115.111	4.601	3	3
11	119.266	74.601	4	4
12	127.111	8.241	4	4
13	27.111	8.241	4	4
14	27.111	5.401	4	4
15	24.211	77.111	4	4
16	24.411	66.800	4	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK
1	52.983	74.601	5	1
2	65.111	77.111	6	2
3	73.958	66.800	7	3
4	95.111	74.601	8	4
5	113.111	8.241	9	5
6	119.266	74.601	11	6
7	127.111	8.241	12	7

FIND SLICE WIDTH AND NO OF SLICES

FI	FO
1.00000	22606
2.2606	25148
2.25148	25385
2.25385	25407

THE SAFETY FACTOR FOR POINT 2 IS 1.25407

TRIAL CIRCLE NO 3

CIRCLE CTR COORDS: X= 92.111 Y= 120.111
 ENTRANCE PT. COORDS: X= 127.111 Y= 81.111
 TRIAL ARC RADIUS= 52.402

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC LINE NO	INTERSECT WITH LINE ARRAY	X	Y
2		70.711	72.28
5		80.409	69.03
7		113.111	74.58
3		127.111	8.11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	000	1	1
2	000	000	1	1
3	000	000	1	1
4	40	111	1	1
5	65	111	1	1
6	70	711	2	2
7	80	409	3	3
8	95	111	3	3
9	113	111	3	3
10	118	038	4	4
11	127	111	4	4
12	175	111	4	4
13	240	111	4	4
14	242	111	4	4
15	244	111	4	4
16	244	111	4	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK
1	70.711	72.28	6	6
2	80.409	69.03	7	7
3	95	111	8	8
4	113	111	9	9
5	118	038	11	11
6	127	111	12	12

FIND SLICE WIDTH AND NO OF SLICES

FI	FO
000000	40689
40689	45530
45530	45948
45948	45984

THE SAFETY FACTOR FOR POINT 3 IS 1.45984

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= 84.111 Y= 124.111
 ENTRANCE PT COORDS: X= 127.111 Y= 81.111
 TRIAL ARC RADIUS= 60.811

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC LINE NO	INTERSECT WITH LINE ARRAY	X	Y
-------------	---------------------------	---	---

5
7
3

55
69
119
127

27
194
422
111

70
65
74
8

65
66
61
41

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	0000	68	1	K=	1	KK=	1
I=	2	0000	53	1	K=	1	KK=	2
I=	3	0000	8	1	K=	1	KK=	3
I=	4	550	55	1	K=	1	KK=	4
I=	5	555	70	65	K=	2	KK=	4
I=	6	655	7	1	K=	2	KK=	5
I=	7	659	65	58	K=	3	KK=	5
I=	8	955	74	58	K=	3	KK=	6
I=	9	333	8	1	K=	3	KK=	7
I=	10	119	4	1	K=	3	KK=	8
I=	11	127	74	607	K=	4	KK=	8
I=	12	27	8	1	K=	4	KK=	9
I=	13	75	54	1	K=	4	KK=	9
I=	14	000	8	1	K=	4	KK=	0
I=	15	44	77	1	K=	4	KK=	0
I=	16	22	66	1	K=	4	KK=	2

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	27	70	65	K=	5	KK=	1
I=	2	111	7	1	K=	6	KK=	2
I=	3	699	65	58	K=	7	KK=	3
I=	4	955	74	58	K=	8	KK=	4
I=	5	333	8	1	K=	9	KK=	5
I=	6	119	4	1	K=	1	KK=	6
I=	7	127	74	607	K=	2	KK=	7

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	6048
FI=	1116048	FO=	7765
FI=	1117765	FO=	7925
FI=	1117925	FO=	7940

THE SAFETY FACTOR FOR POINT 4 IS 1.17940

TRIAL CIRCLE NO 5
 CIRCLE CTR COORDS: X= 88.41 Y= 24.1
 ENTRANCE PT COORDS: X= 127.41 Y= 8.1
 TRIAL ARC RADIUS= 58.052

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	64.490	7.208
5	75.593	67.440
7	118.391	74.559
3	127.111	81.111

In cross-section (8-8) B soil types are given as :

Soil I : Bottom Sludge (Slurry)

Soil II : Artificial Fill

Soil III : Sedimentary Layer

Soil 4 : Decomposed Graywacke

The results taken from the computer for cross-section (8-8)B a

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	101	110	143	64	1.67
b	97	103	133	64	3.11
c	107	101	139	64	3.62
d	93	108	136	64	1.54
e	109	108	152	64	1.67
f	86	111	133	64	1.44
g	88	103	139	64	1.16

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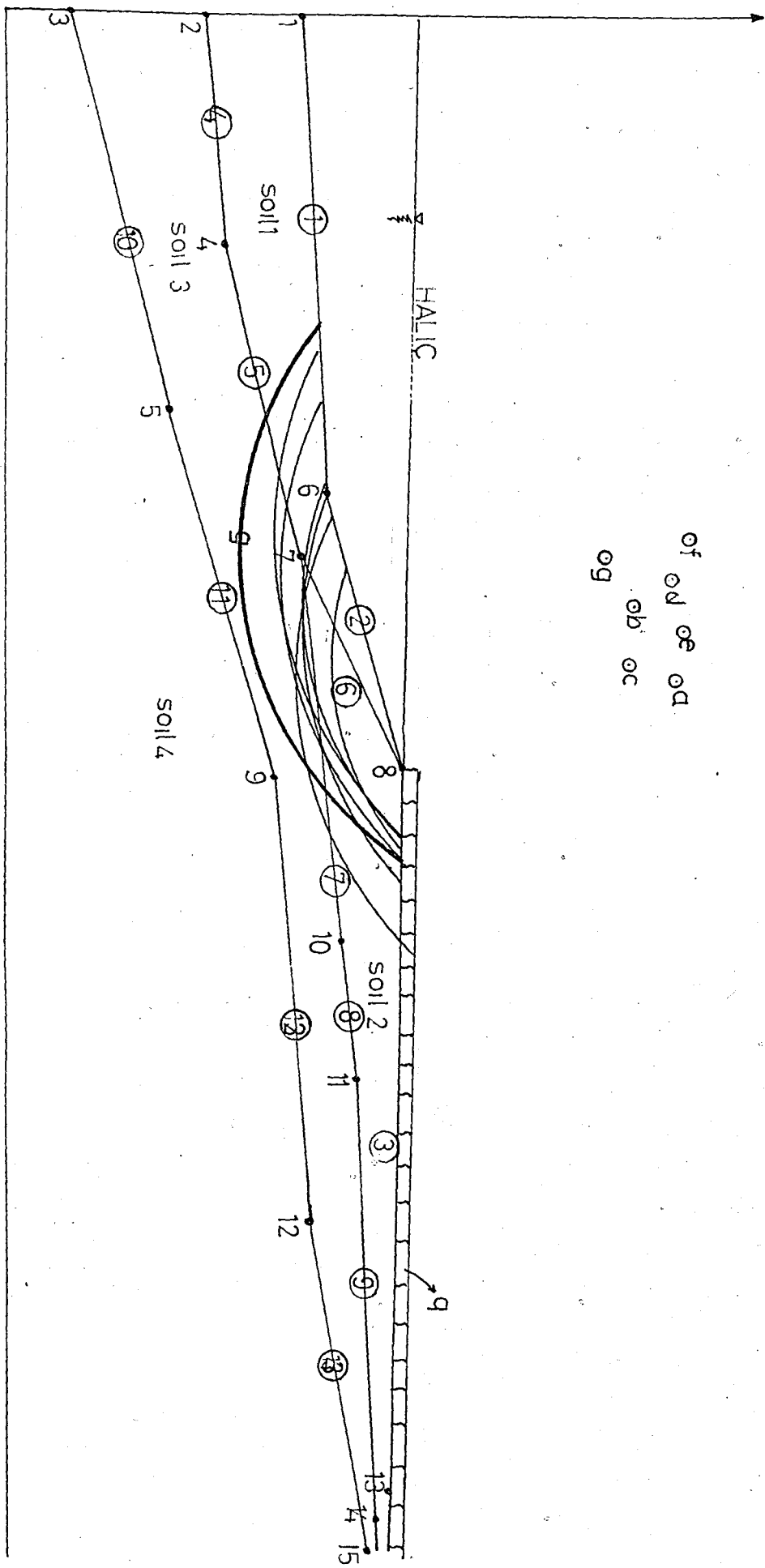


Fig : (8-8) B

PE STABILITY FOR TASKIZAK(TI)MAHR KOSELER THESIS:

OF LINES 13 NO OF LINE INTERSECT= 15
 OF SOILS= 4 NO OF EXTERNAL SOIL LINES= 3
 OF X INCREMENTS= 3 NO OF Y INCREMENTS= 3
 IN INITIAL SLICE WIDTH= 2.0

LINE END COORD MATRIX		X			Y			SLOPE			LINE INTER		
NO	NO	INT	X1	X2	Y1	Y2	SLOPE	SLOPE	SLOPE	LINE INTER	LINE INTER	LINE INTER	
1	1	0	77	77	0	0	0	0	0	1	6	8	
2	1	0	24	24	0	0	0	0	0	3	3	4	
3	1	0	36	36	0	0	0	0	0	2	4	7	
4	1	0	89	89	0	0	0	0	0	7	7	8	
5	1	0	89	89	0	0	0	0	0	7	7	0	
6	1	0	48	48	0	0	0	0	0	1	0	1	
7	1	0	74	74	0	0	0	0	0	1	4	5	
8	1	0	64	64	0	0	0	0	0	3	5	9	
9	1	0	25	25	0	0	0	0	0	1	2	5	
10	1	0	99	99	0	0	0	0	0	1	2	5	

LINE INTERSECT ARRAY		X			Y		
NO	NO	INT	X1	X2	Y1	Y2	
1	1	0	77	77	0	0	
2	1	0	24	24	0	0	
3	1	0	36	36	0	0	
4	1	0	89	89	0	0	
5	1	0	89	89	0	0	
6	1	0	48	48	0	0	
7	1	0	74	74	0	0	
8	1	0	64	64	0	0	
9	1	0	25	25	0	0	
10	1	0	99	99	0	0	

LINE NO	LINE #	LEFT INT	PT. INT	SAT	UNIT	WT	PHI	COHESI	ON
1	1	5	6	0	5	5	12	0	0
2	1	8	8	0	5	5	12	0	0
3	1	2	4	0	5	5	12	0	0
4	1	7	7	0	5	5	12	0	0
5	1	4	7	0	5	5	12	0	0
6	1	7	8	0	5	5	12	0	0
7	1	7	8	0	5	5	12	0	0
8	1	7	8	0	5	5	12	0	0
9	1	7	8	0	5	5	12	0	0
10	1	7	8	0	5	5	12	0	0
11	1	7	8	0	5	5	12	0	0
12	1	7	8	0	5	5	12	0	0
13	1	7	8	0	5	5	12	0	0

AL CIRCLE NO 1
 CLE CTR COORDS: X = X = 88 Y = 39
 RANCE PT. COORDS: X = X = 64 Y = 64

TRIAL ARC RADIUS= 64.203

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 12 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 13 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC
 ***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 1 50 048 51 41
 2 65 024 43 20
 3 127 433 52 36
 4 139 111 64 11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	50	41	K	1	KK	1
2	000	33	20	K	1	KK	2
3	000	11	36	K	1	KK	3
4	000	33	11	K	1	KK	4
5	36	51	41	K	2	KK	4
6	50	43	20	K	2	KK	5
7	64	52	36	K	3	KK	5
8	65	49	11	K	3	KK	6
9	77	49	11	K	3	KK	7
10	89	64	11	K	3	KK	8
11	24	64	11	K	3	KK	9
12	27	44	33	K	4	KK	9
13	39	55	44	K	4	KK	9
14	48	55	44	K	4	KK	0
15	79	56	49	K	4	KK	1
16	99	49	11	K	4	KK	2
17	29	64	11	K	4	KK	3
18	30	58	24	K	4	KK	4
19	232	56	11	K	4	KK	5

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	50	48	51	41	K	5	KK	1
2	65	24	43	20	K	7	KK	2
3	77	11	52	36	K	8	KK	3
4	89	11	49	11	K	9	KK	4
5	24	11	64	11	K	0	KK	5
6	27	33	52	36	K	2	KK	5
7	39	11	64	11	K	3	KK	7

FIND SLICE WIDTH AND NO OF SLICES.

1	000	00	FO	4	67
2	4	67	FO	5	63
3	5	63	FO	6	65
4	6	65	FO	6	88

TRIAL CIRCLE NO 2
 TRIANGLE CTR COORDS: X= X= 92.717 Y= 103.711
 ENTRANCE PT. COORDS: X= X= 39.39 Y= 64.11
 TRIAL ARC RADIUS= 61.074

- XX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 12 NOT INTERSECTED BY TRIAL CIRCL
- XX LINE 13 NOT INTERSECTED BY TRIAL CIRCL
- ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC
- ***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	59.228	51.65
2	72.905	45.14
3	125.888	52.23
4	139.111	64.11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	59.228	51.65	1	1
2	72.905	45.14	1	2
3	125.888	52.23	1	3
4	139.111	64.11	1	4
5	36.000	36.000	1	4
6	59.228	51.65	2	5
7	72.905	45.14	2	5
8	125.888	52.23	3	6
9	139.111	64.11	3	7
10	24.000	24.000	3	8
11	25.555	25.555	3	9
12	33.333	33.333	4	9
13	39.390	39.390	4	0
14	48.000	48.000	4	1
15	56.000	56.000	4	2
16	77.000	77.000	4	3
17	77.000	77.000	4	3
18	23.000	23.000	4	4
19	23.000	23.000	4	5

THE APPLICABLE ARRAY ARC INT FOLLOWS:

LINE NO	X	Y	K	KK
1	59.228	51.65	5	1
2	72.905	45.14	7	2
3	77.000	77.000	8	3
4	89.000	89.000	9	4
5	24.000	24.000	0	5
6	25.555	25.555	2	6
7	39.390	39.390	3	7

FIND SLICE WIDTH AND NO OF SLICES
 FI= 000000 FO= 8968
 FI= 18968 FO= 21496
 FI= 21496 FO= 21784
 FI= 21784 FO= 21816

THE SAFETY FACTOR FOR POINT 2IS T₂₁₈₁₆

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= X= 96.719 Y= 103.711
 ENTRANCE PT COORDS: X= X= 39.711 Y= 64.711
 TRIAL ARC RADIUS= 58.052

- XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 12 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 13 NOT INTERSECTED BY TRIAL CIRCL
- ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC
- ***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	68.783	51.89
2	80.882	47.09
3	123.78	52.04
4	139.11	64.5

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000000	50.0000	1	1
2	000000	33.0000	1	2
3	000000	11.0000	1	3
4	36.0000	36.0000	1	4
5	64.0000	26.0000	1	5
6	68.0000	55.0000	2	5
7	77.0000	52.0000	2	6
8	80.0000	47.0000	3	6
9	89.0000	49.0000	3	7
10	123.0000	52.0000	4	7
11	124.0000	64.0000	4	8
12	125.0000	44.0000	4	9
13	139.0000	64.0000	4	9
14	148.0000	54.0000	4	0
15	174.0000	56.0000	4	4
16	199.0000	49.0000	4	4
17	229.0000	64.0000	4	3
18	230.0000	58.0000	4	4
19	232.0000	56.0000	4	4

THE APPLICABLE ARRAY ARC INT FOLLOWS:
 I= 1 68.783 51.895 K= 6 KK= 1

3	77	52	K=	7	KK=	3
4	80	47	K=	8	KK=	4
5	89	49	K=	9	KK=	5
6	23	52	K=	0	KK=	6
7	39	64	K=	1	KK=	7

FIND SLICE WIDTH AND NO OF SLICES

FILE	0000	FO	30652
FTE	30652	FO	34954
FLE	34954	FO	35422
FIL	35422	FO	35472

THE SAFETY FACTOR FOR POINT 3IS 1.35472

TRIAL CIRCLE NO 4
 ENTRANCE PT COORDS: X= 88.11 Y= 07.11
 TRIAL ARC RADIUS= 66.708

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 12 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 13 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC
 ***LINE 6 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

IN	NO	X	Y
1	5	356	44
2	7	249	75
3	13	049	24
4	19	1	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	50	K=	1	KK=	1
2	000	33	K=	2	KK=	2
3	000	11	K=	1	KK=	3
4	36	38	K=	1	KK=	4
5	51	51	K=	2	KK=	4
6	64	26	K=	2	KK=	5
7	67	43	K=	3	KK=	5
8	77	22	K=	3	KK=	6
9	89	49	K=	3	KK=	7
10	124	64	K=	3	KK=	8
11	25	44	K=	3	KK=	9
12	26	52	K=	4	KK=	9
13	39	64	K=	4	KK=	9
14	48	54	K=	4	KK=	0
15	74	56	K=	4	KK=	1
16	99	49	K=	4	KK=	2

In cross-section (IO-IO)A soil types are given as :

Soil I : Bottom Sludge

Soil II : Artificial Fill

Soil III : Sedimentary Layer

Soil 4 : Decomposed Graywacke

The results taken from the computer for cross-section (IO-IO)A are

Circle NO	Circle Center Coordinates		Entrance Points		Factor Of Safety
	X	Y	X	Y	
a	II7	III	I4I	90	I.24
b	I25	II6	I59	90	I.58
c	III	II7	I49	90	I.3I
d	II9	I0I	I68	90	3.05
e	II9	I30	I82	90	2.77
f	II6	I43	I87	90	2.54
g	I08	I29	I6I	90	2.3I
h	I04	I52	I84	90	3.34
k	II9	I23	I45	90	I.54

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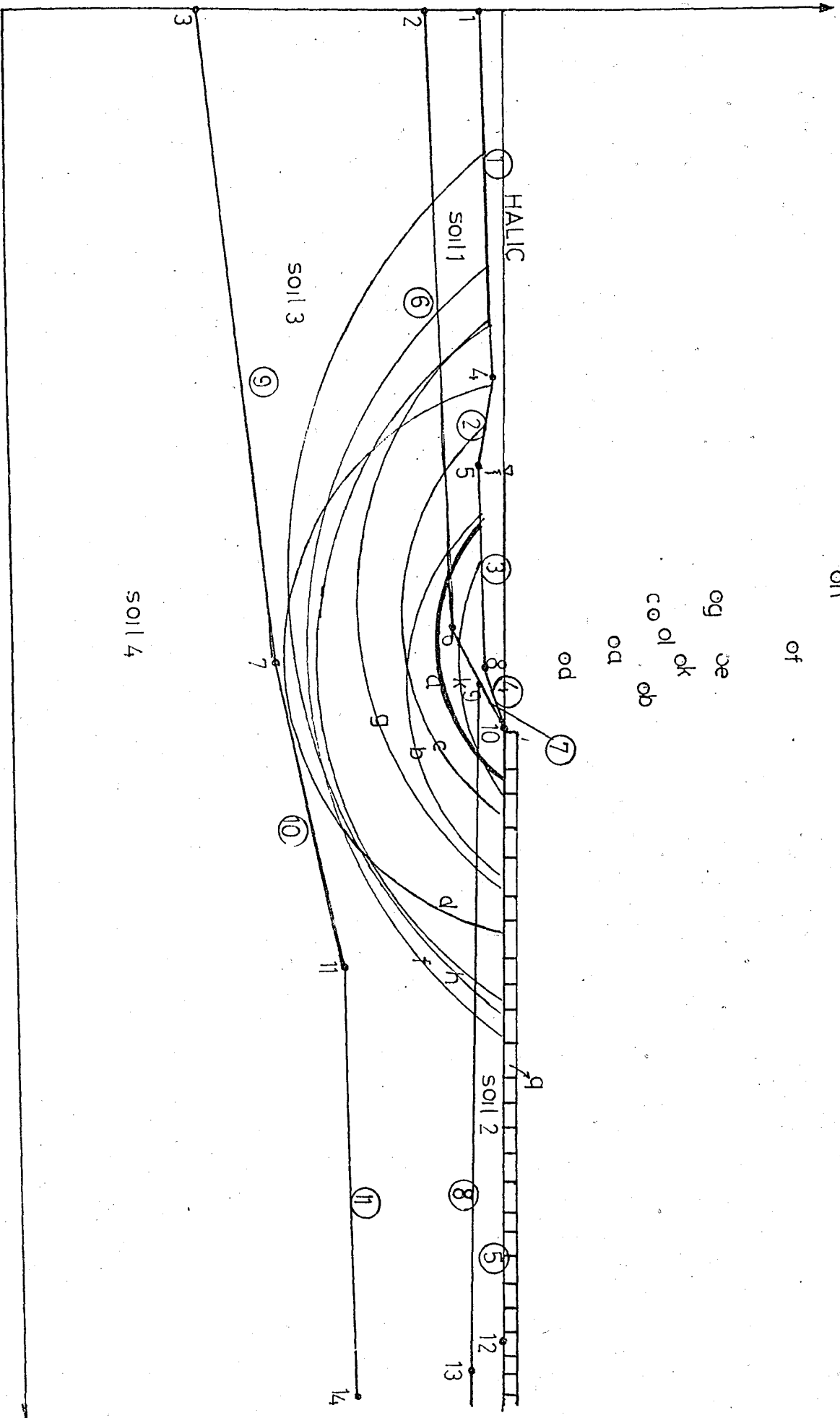


Fig : (10-10)A

OF LINES 11 NO OF LINE INTERSECT= 14
 OF SOILS= 4 NO OF EXTERNAL SOIL LINES= 5
 OF X INCREMENTS= 3 NO OF Y INCREMENTS= 3
 IN ITIAL SLICE WIDTH= 270

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INTE
1	2	67	00	87	67	88	749007	00
2	3	84	00	88	84	86	77647	00
3	4	22	00	86	22	90	000000	00
4	5	32	00	86	32	90	000000	00
5	6	00	00	90	00	80	000000	00
6	7	00	00	78	00	90	000000	00
7	8	00	00	80	00	83	000000	00
8	9	25	00	87	25	90	447619	00
9	10	00	00	35	00	47	999076	00
10	11	20	00	47	20	59	999076	00
11	12	75	00	59	75	60	754339	00

LINE NO	INTERSECT X	Y
1	00	87
2	00	78
3	00	35
4	00	88
5	67	86
6	84	86
7	00	47
8	00	86
9	00	87
10	25	90
11	00	59
12	20	90
13	00	83
14	00	60

OIL NO	LINE #	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESI ON
1	2	4	4	000	11.5	12.0	000000
2	3	5	8	000	11.5	12.0	000000
3	4	5	00	000	11.5	12.0	000000
4	5	00	00	000	11.5	12.0	000000
5	6	00	00	000	11.5	12.0	000000
6	7	00	00	000	11.5	12.0	000000
7	8	00	00	000	11.5	12.0	000000
8	9	00	00	000	11.5	12.0	000000
9	10	00	00	000	11.5	12.0	000000
10	11	00	00	000	11.5	12.0	000000
11	12	00	00	000	11.5	12.0	000000
12	13	00	00	000	11.5	12.0	000000
13	14	00	00	000	11.5	12.0	000000
14	15	00	00	000	11.5	12.0	000000
15	16	00	00	000	11.5	12.0	000000
16	17	00	00	000	11.5	12.0	000000
17	18	00	00	000	11.5	12.0	000000
18	19	00	00	000	11.5	12.0	000000
19	20	00	00	000	11.5	12.0	000000
20	21	00	00	000	11.5	12.0	000000
21	22	00	00	000	11.5	12.0	000000
22	23	00	00	000	11.5	12.0	000000
23	24	00	00	000	11.5	12.0	000000
24	25	00	00	000	11.5	12.0	000000
25	26	00	00	000	11.5	12.0	000000
26	27	00	00	000	11.5	12.0	000000
27	28	00	00	000	11.5	12.0	000000
28	29	00	00	000	11.5	12.0	000000
29	30	00	00	000	11.5	12.0	000000
30	31	00	00	000	11.5	12.0	000000
31	32	00	00	000	11.5	12.0	000000
32	33	00	00	000	11.5	12.0	000000
33	34	00	00	000	11.5	12.0	000000
34	35	00	00	000	11.5	12.0	000000
35	36	00	00	000	11.5	12.0	000000
36	37	00	00	000	11.5	12.0	000000
37	38	00	00	000	11.5	12.0	000000
38	39	00	00	000	11.5	12.0	000000
39	40	00	00	000	11.5	12.0	000000
40	41	00	00	000	11.5	12.0	000000
41	42	00	00	000	11.5	12.0	000000
42	43	00	00	000	11.5	12.0	000000
43	44	00	00	000	11.5	12.0	000000
44	45	00	00	000	11.5	12.0	000000
45	46	00	00	000	11.5	12.0	000000
46	47	00	00	000	11.5	12.0	000000
47	48	00	00	000	11.5	12.0	000000
48	49	00	00	000	11.5	12.0	000000
49	50	00	00	000	11.5	12.0	000000
50	51	00	00	000	11.5	12.0	000000
51	52	00	00	000	11.5	12.0	000000
52	53	00	00	000	11.5	12.0	000000
53	54	00	00	000	11.5	12.0	000000
54	55	00	00	000	11.5	12.0	000000
55	56	00	00	000	11.5	12.0	000000
56	57	00	00	000	11.5	12.0	000000
57	58	00	00	000	11.5	12.0	000000
58	59	00	00	000	11.5	12.0	000000
59	60	00	00	000	11.5	12.0	000000
60	61	00	00	000	11.5	12.0	000000
61	62	00	00	000	11.5	12.0	000000
62	63	00	00	000	11.5	12.0	000000
63	64	00	00	000	11.5	12.0	000000
64	65	00	00	000	11.5	12.0	000000
65	66	00	00	000	11.5	12.0	000000
66	67	00	00	000	11.5	12.0	000000
67	68	00	00	000	11.5	12.0	000000
68	69	00	00	000	11.5	12.0	000000
69	70	00	00	000	11.5	12.0	000000
70	71	00	00	000	11.5	12.0	000000
71	72	00	00	000	11.5	12.0	000000
72	73	00	00	000	11.5	12.0	000000
73	74	00	00	000	11.5	12.0	000000
74	75	00	00	000	11.5	12.0	000000
75	76	00	00	000	11.5	12.0	000000
76	77	00	00	000	11.5	12.0	000000
77	78	00	00	000	11.5	12.0	000000
78	79	00	00	000	11.5	12.0	000000
79	80	00	00	000	11.5	12.0	000000
80	81	00	00	000	11.5	12.0	000000
81	82	00	00	000	11.5	12.0	000000
82	83	00	00	000	11.5	12.0	000000
83	84	00	00	000	11.5	12.0	000000
84	85	00	00	000	11.5	12.0	000000
85	86	00	00	000	11.5	12.0	000000
86	87	00	00	000	11.5	12.0	000000
87	88	00	00	000	11.5	12.0	000000
88	89	00	00	000	11.5	12.0	000000
89	90	00	00	000	11.5	12.0	000000
90	91	00	00	000	11.5	12.0	000000
91	92	00	00	000	11.5	12.0	000000
92	93	00	00	000	11.5	12.0	000000
93	94	00	00	000	11.5	12.0	000000
94	95	00	00	000	11.5	12.0	000000
95	96	00	00	000	11.5	12.0	000000
96	97	00	00	000	11.5	12.0	000000
97	98	00	00	000	11.5	12.0	000000
98	99	00	00	000	11.5	12.0	000000
99	100	00	00	000	11.5	12.0	000000

TRIAL CIRCLE NO 1
 CTR COORDS: X= 17.1 Y= 11.1
 ENTRANCE PT COORDS: X= 4.4 Y= 9.0
 TRIAL ARC RADIUS= 3.890

XX LINE NOT INTERSECTED BY TRIAL CIRCL
 XX LINE NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 4 IS NOT INTERSECTED BUT IS IN ARC
 ***LINE 7 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 3 97.3 2 86.7
 6 109.7 40 80.09
 8 137.5 57 86.64
 9 141.1 1 90.1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 I= 1 000 87 1 1 KK= 1
 I= 2 000 78 1 1 KK= 1 2
 I= 3 000 35 1 1 KK= 1 2 3
 I= 4 67 88 1 1 KK= 1 4
 I= 5 84 86 1 1 KK= 1 5
 I= 6 97 86 2 2 KK= 1 5 5
 I= 7 09 80 3 3 KK= 1 5 5 6
 I= 8 11 80 3 3 KK= 1 5 5 6 7
 I= 9 20 47 3 3 KK= 1 5 5 6 7 8
 I= 10 22 86 3 3 KK= 1 5 5 6 7 8 9
 I= 11 25 87 3 3 KK= 1 5 5 6 7 8 9
 I= 12 32 90 3 3 KK= 1 5 5 6 7 8 9
 I= 13 37 86 4 4 KK= 1 5 5 6 7 8 9
 I= 14 41 90 4 4 KK= 1 5 5 6 7 8 9
 I= 15 75 59 4 4 KK= 1 5 5 6 7 8 9
 I= 16 229 90 4 4 KK= 1 5 5 6 7 8 9
 I= 17 230 83 4 4 KK= 1 5 5 6 7 8 9
 I= 18 232 60 4 4 KK= 1 5 5 6 7 8 9

THE APPLICABLE ARRAY ARCINT FOLLOWS:
 I= 1 97.3 2 86.7 KK= 6
 I= 2 109.7 40 80.09 KK= 7
 I= 3 111.1 1 86.64 KK= 8
 I= 4 122.2 1 86.64 KK= 10
 I= 5 125.5 1 87.337 KK= 11
 I= 6 132.1 1 90.1 KK= 12
 I= 7 137.5 57 86.64 KK= 13
 I= 8 141.1 1 90.1 KK= 14

FIND SLICE WIDTH AND NO OF SLICES
 FI= 1 000 87 FO= 21473
 FI= 2 1473 FO= 24381
 FI= 3 24381 FO= 24711
 FI= 4 24711 FO= 24747

THE SAFETY FACTOR FOR POINT IIS 1.24747

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 120.7 Y= 11.741
 ENTRANCE PT COORDS: X= 14.4 Y= 90.11
 TRIAL ARC RADIUS= 29.698

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL

***LINE 4 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 3 104 080 86
 7 114 836 88
 8 135 967 86
 5 141 111 90

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 I= 1 0000 87 K= 1 KK= 1
 I= 2 0000 78 K= 1 KK= 2
 I= 3 0000 35 K= 1 KK= 3
 I= 4 67 88 K= 1 KK= 4
 I= 5 84 86 K= 1 KK= 5
 I= 6 04 86 K= 2 KK= 6
 I= 7 11 80 K= 2 KK= 7
 I= 8 14 88 K= 3 KK= 8
 I= 9 14 88 K= 3 KK= 9
 I= 10 22 47 K= 3 KK= 10
 I= 11 22 86 K= 3 KK= 11
 I= 12 25 87 K= 3 KK= 12
 I= 13 32 90 K= 3 KK= 13
 I= 14 36 86 K= 4 KK= 14
 I= 15 44 90 K= 4 KK= 15
 I= 16 75 59 K= 4 KK= 16
 I= 17 22 90 K= 4 KK= 17
 I= 18 23 83 K= 4 KK= 18
 I= 19 32 60 K= 4 KK= 19

THE APPLICABLE ARRAY ARCINT FOLLOWS:
 I= 2 0000 86 K= 6 KK= 2
 I= 3 22 88 K= 8 KK= 3
 I= 4 22 86 K= 8 KK= 4
 I= 5 25 87 K= 8 KK= 5
 I= 6 36 90 K= 2 KK= 6
 I= 7 44 86 K= 4 KK= 7

FIND SLICE WIDTH AND NO OF SLICES
 FI= 0000 FO= 37942
 FI= 37942 FO= 43391
 FI= 43391 FO= 43972
 FI= 43972 FO= 44032

THE SAFETY FACTOR FOR POINT 2 IS 1.44032

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 23.71 Y= 90.11
 ENTRANCE PT. COORDS: X= 41.71 Y= 90.11
 TRIAL ARC RADIUS= 27.659

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 4 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 LINE NO

3	111	279	86
7	118	228	83
8	136	102	86
5	141	111	90

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	87	K	K	1
2	000	78	K	K	2
3	000	35	K	K	3
4	57	88	K	K	4
5	84	86	K	K	5
6	111	80	K	K	6
7	111	86	K	K	7
8	111	83	K	K	8
9	111	47	K	K	9
0	222	86	K	K	0
1	225	87	K	K	1
2	325	90	K	K	2
3	336	86	K	K	3
4	447	59	K	K	4
5	475	90	K	K	5
6	229	90	K	K	6
7	230	83	K	K	7
8	232	60	K	K	8

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	111	279	86	7	K	7
2	118	228	83	8	K	8
3	222	102	86	10	K	10
4	225	111	87	11	K	11
5	325	102	90	12	K	12
6	336	111	86	13	K	13
7	447	111	90	14	K	14

FIND SLICE WIDTH AND NO OF SLICES

FI	00000	FO	75605
FI	75605	FO	86865
FI	86865	FO	87845
FI	87845	FO	87926

THE SAFETY FACTOR FOR POINT 3 IS 1.87926

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= 117.5 Y= 142.1
 ENTRANCE PT COORDS: X= 14.5 Y= 90.1
 TRIAL ARC RADIUS= 33.941

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

9 NOT INTERSECTED BY TRIAL CIRCL
 10 NOT INTERSECTED BY TRIAL CIRCL
 11 NOT INTERSECTED BY TRIAL CIRCL
 4 IS NOT INTERSECTED BUT IS IN ARC

INTERSECT WITH LINE ARRAY

X	Y
97.928	86.55
12.036	80.55
137.067	86.66
141.111	90.11

ARRAY WITH ALL INTERSECTIONS FOLLOWS:

Array	Intersections	Follows
87	87	KK= 1
78	78	KK= 1
35	35	KK= 1
88	88	KK= 1
86	86	KK= 1
86	86	KK= 2
80	80	KK= 2
80	80	KK= 3
47	47	KK= 3
86	86	KK= 3
87	87	KK= 3
90	90	KK= 4
86	86	KK= 4
90	90	KK= 4
59	59	KK= 4
90	90	KK= 4
83	83	KK= 4
60	60	KK= 4

ELICABLE ARRAY ARC INT. FOLLOWS:

Array	Arc Int.	Follows
97.928	86.55	KK= 6
12.036	80.55	KK= 8
137.067	86.66	KK= 1
141.111	90.11	KK= 2
137.067	86.66	KK= 3
141.111	90.11	KK= 4

SLICE WIDTH AND NO. OF SLICES

FI= 28964	FO= 1128964
FI= 32874	FO= 1132874
FI= 33292	FO= 1133292
FI= 33335	FO= 1133335

THE SAFETY FACTOR FOR POINT 4 IS 1.33335

CIRCLE NO 5
 CTR COORDS: X= 120.111 Y= 14.111
 POINT COORDS: X= 14.111 Y= 90.111
 TRIAL ARC RADIUS= 31.890

1 NOT INTERSECTED BY TRIAL CIRCL
 2 NOT INTERSECTED BY TRIAL CIRCL
 4 NOT INTERSECTED BY TRIAL CIRCL
 5 NOT INTERSECTED BY TRIAL CIRCL
 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

***LINE 4 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y	ARC NO
3	104	86	86
7	116	82	82
8	136	86	86
5	141	90	90
	347	86	86
	379	82	82
	376	86	86
	376	90	90

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	ARC NO	K	KK
1	000	87	87	1	1
2	000	78	78	1	1
3	000	35	35	1	1
4	67	88	88	1	1
5	84	86	86	1	1
6	104	86	86	2	2
7	116	80	80	2	2
8	122	82	82	3	3
9	122	47	47	3	3
10	125	86	86	3	3
11	132	87	87	3	3
12	132	90	90	3	3
13	136	86	86	4	4
14	144	90	90	4	4
15	175	59	59	4	4
16	229	90	90	4	4
17	230	83	83	4	4
18	232	60	60	4	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	ARC NO	K	KK
1	104	86	86	6	6
2	116	82	82	8	8
3	122	86	86	1	1
4	125	87	87	1	1
5	132	90	90	2	2
6	136	86	86	3	3
7	144	90	90	4	4

FIND SLICE WIDTH AND NO OF SLICES

FI	FO
00000	52322
52322	59756
59756	60466
60466	6053

THE SAFETY FACTOR FOR POINT SIS 1.60531

TRIAL CIRCLE NO 5
 CIRCLE CTR COORDS: X= 123.2 Y= 14.1
 ENTRANCE PT COORDS: X= 141.0 Y= 90.0
 TRIAL ARC RADIUS= 30.000

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

In cross-section (IO-IO)B soil types are given as :

Soil I : Bottom Sludge

Soil II : Artificial Fill

Soil III : Sedimentary Layer

Soil 4 : Decomposed Graywacke

The results taken from the computer for cross-section (IO-IO)B a

Circle NO	Circle Center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	I23	II3	I47	9I	1.80
b	I29	II2	I49	9I	2.56
c	I25	I23	I58	9I	2.30
d	II6	I28	I57	9I	2.95
e	I2I	I37	I65	9I	2.78
f	I07	I52	I69	9I	3.07
g	I09	I37	I8I	9I	4.0I
h	II4	II5	I60	9I	4.47

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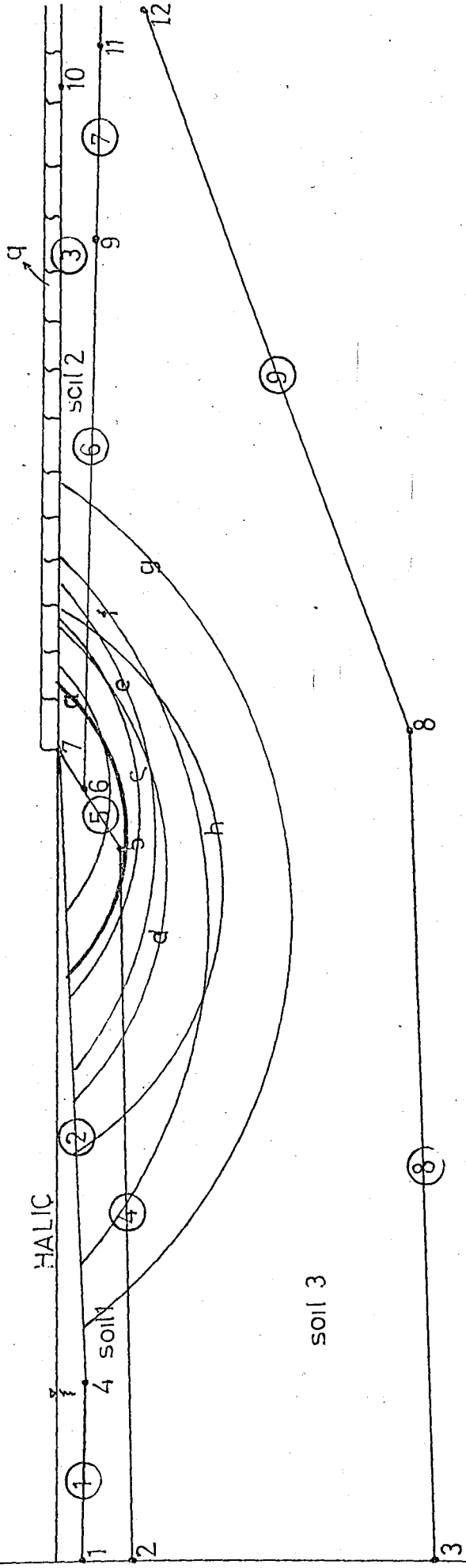


Fig : (10-10) B

LOPE STABILITY FOR HALIC KOPRU(II) NAHIR KOSELER THESIS

NO OF LINES = 9 NO OF LINE INTERSECT = 72
 NO OF SOILS = 4 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 3 NO OF Y INCREMENTS = 3
 INITIAL SLICE WIDTH = 200

LINE NO	LINE NO	END INT	COORD MATRIX	X1	Y1	X2	Y2	SLOPE	LINE INTERSECT
1	1	1	27	88	88	27	88	0.0000	1
1	1	2	36	88	88	36	88	0.0000	1
1	1	3	12	88	88	12	88	0.0000	1
1	1	4	28	88	88	28	88	0.0000	1
1	1	5	14	88	88	14	88	0.0000	1
1	1	6	22	88	88	22	88	0.0000	1
1	1	7	38	88	88	38	88	0.0000	1

LINE NO	INTERSECT	X	Y
1	1	27	88
1	2	36	88
1	3	12	88
1	4	28	88
1	5	14	88
1	6	22	88
1	7	38	88

SOIL NO	LINE #	LEFT INT	RT INT	SAT	UNIT	WT	PHI	COHESI ON
1	1	4	4	0	1	5	12	0
1	2	7	7	0	1	5	12	0
1	3	5	5	0	1	5	12	0
1	4	7	7	0	1	5	12	0
1	5	6	6	0	1	5	12	0
1	6	6	6	0	7	8	20	19
1	7	9	9	0	7	8	20	19
1	8	7	7	0	7	8	20	19
1	9	5	5	0	7	8	20	19
1	10	6	6	0	7	8	12	0
1	11	9	9	0	7	8	12	0
1	12	3	3	0	7	8	12	0
1	13	3	3	0	3	7	45	68
1	14	3	3	0	3	7	45	68

TRIAL CIRCLE NO 1
 TRIAL CTR COORDS: X = 23.711 Y = 13.111
 ENTRANCE PT COORDS: X = 14.711 Y = 9.111
 TRIAL ARC RADIUS = 32.558

- XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 5 IS NOT INTERSECTED BUT IS IN ARC

ARC LINE NO	INTERSECT WITH X	LINE ARRAY Y
2	00.058	90.028
4	17.138	81.044
6	40.638	85.671
3	47.111	91.028

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:						
I=	1	000	K=	1	KK=	1
I=	2	000	K=	1	KK=	2
I=	3	000	K=	1	KK=	3
I=	4	000	K=	1	KK=	4
I=	5	000	K=	1	KK=	4
I=	6	27.058	K=	2	KK=	4
I=	7	17.138	K=	3	KK=	5
I=	8	18.066	K=	3	KK=	6
I=	9	128.066	K=	3	KK=	7
I=	10	133.066	K=	3	KK=	8
I=	11	4.058	K=	4	KK=	8
I=	12	47.111	K=	4	KK=	9
I=	13	214.058	K=	4	KK=	9
I=	14	233.058	K=	4	KK=	0
I=	15	236.058	K=	4	KK=	0
I=	16	240.058	K=	4	KK=	1

THE APPLICABLE ARRAY ARCINT FOLLOWS:						
I=	2	000	K=	5	KK=	1
I=	3	000	K=	6	KK=	2
I=	4	000	K=	7	KK=	3
I=	5	000	K=	8	KK=	4
I=	6	27.058	K=	9	KK=	5
I=	7	17.138	K=	11	KK=	6

FIND SLICE WIDTH AND NO OF SLICES			
F=	000000	F0=	68864
F=	68864	F0=	79457
F=	79457	F0=	80455
F=	80455	F0=	80544

THE SAFETY FACTOR FOR POINT IS 1.80544

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 126.711 Y= 133.111
 ENTRANCE PT COORDS: X= 47.441 Y= 9.111
 TRIAL ARC RADIUS= 30.444

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC LINE NO	INTERSECT WITH X	LINE ARRAY Y
2	00.028	90.028
5	21.058	83.044
6	39.330	85.671
3	47.111	91.028

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	89	1	KK	1
2	000	89	1	KK	2
3	000	83	1	KK	3
4	000	88	1	KK	4
5	000	88	2	KK	5
6	000	90	2	KK	6
7	000	88	3	KK	7
8	000	86	3	KK	8
9	000	93	3	KK	9
10	000	95	4	KK	10
11	000	88	4	KK	11
12	000	88	4	KK	12
13	000	99	4	KK	13
14	000	83	4	KK	14
15	000	73	4	KK	15

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	06	90	5	KK	1
2	11	83	7	KK	2
3	28	86	8	KK	3
4	36	99	9	KK	4
5	39	85	1	KK	5
6	47	9	2	KK	6

FIND SLICE WIDTH AND NO OF SLICES

F1	00000	F0	2	59	6
F2	15906	F0	2	338	55
F3	33855	F0	2	35	86
F4	23586	F0	2	35	278

THE SAFETY FACTOR FOR POINT 21S 2.35278

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 29.47 Y= 13.11
 ENTRANCE PT COORDS: X= 28.425 Y= 9.47
 TRIAL ARC RADIUS= 28.425

- XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

ARC NO	X	Y
2	11	953
5	125	866
6	135	997
3	147	111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	89	1	KK	1
2	000	89	1	KK	2
3	000	83	1	KK	3
4	000	88	1	KK	4
5	000	88	2	KK	5
6	000	90	2	KK	6
7	000	88	3	KK	7
8	000	86	3	KK	8
9	000	93	3	KK	9
10	000	95	4	KK	10
11	000	88	4	KK	11
12	000	88	4	KK	12
13	000	99	4	KK	13
14	000	83	4	KK	14
15	000	73	4	KK	15

1	233	90	K	4	KK	1
2	36	84	K	7	KK	2
3	240	86	K	8	KK	3
4		90	K	9	KK	4
5		85	K	0	KK	5
6		73	K	2	KK	6

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	00	90	K	5	KK	1
2	25	84	K	7	KK	2
3	36	86	K	8	KK	3
4	36	90	K	9	KK	4
5	47	85	K	0	KK	5
6		73	K	2	KK	6

FIND SLICE WIDTH AND NO OF SLICES

FI	100000	FO	3	29465
FI	229465	FO	3	22594
FI	3362594	FO	3	664087
FI	3664087	FO	3	6448

THE SAFETY FACTOR FOR POINT 3IS 3.64148

TRIAL CIRCLE NO 4
 CIRCLE COORDS: X= X= 23.47 Y= 16.11
 ENTRANCE PT COORDS: X= X= 47.9 Y= 9.11
 TRIAL ARC RADIUS= 34.655

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
2	100	183
3	119	142
4	139	740
5	147	131
6		90
7		81
8		85
9		95

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	00	90	K	1	KK	1
2	25	84	K	1	KK	2
3	36	86	K	1	KK	3
4	36	90	K	2	KK	4
5	47	85	K	2	KK	5
6		73	K	3	KK	6
7			K	3	KK	7
8			K	3	KK	8
9			K	4	KK	8
0			K	4	KK	9
1			K	4	KK	0
2			K	4	KK	1
3			K	4	KK	2
4			K	4	KK	3
5			K	4	KK	4
6			K	4	KK	5

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	00	90	K	5	KK	1
2	25	84	K	7	KK	2
3	36	86	K	8	KK	3
4	36	90	K	9	KK	4
5	47	85	K	0	KK	5
6		73	K	2	KK	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	1.700000	FO=	1.788869
FI=	2.02386	FO=	2.02386
FI=	2.03277	FO=	2.03277

THE SAFETY FACTOR FOR POINT 4IS 2.03361

TRIAL CIRCLE NO 5
 CIRCLE CTR COORDS: X= X= 26.711 Y= 16.711
 ENTRANCE PT COORDS: X= X= 47.111 Y= 9.111
 TRIAL ARC RADIUS= 32.650

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 2 106.134 90.29
 5 122.569 83.64
 6 138.151 85.76
 3 147.111 9.111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	89	K=	1	KK=	1
I=	2	000	88	K=	1	KK=	2
I=	3	000	3	K=	1	KK=	3
I=	4	27	88	K=	1	KK=	4
I=	5	06	90	K=	2	KK=	4
I=	6	18	88	K=	2	KK=	5
I=	7	22	85	K=	3	KK=	5
I=	8	28	86	K=	3	KK=	6
I=	9	33	99	K=	3	KK=	7
I=	10	33	85	K=	3	KK=	8
I=	11	38	99	K=	4	KK=	8
I=	12	47	99	K=	4	KK=	8
I=	13	22	88	K=	4	KK=	9
I=	14	23	88	K=	4	KK=	9
I=	15	23	85	K=	4	KK=	0
I=	16	24	73	K=	4	KK=	2

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	06	90	K=	5	KK=	1
I=	2	22	83	K=	7	KK=	2
I=	3	28	86	K=	8	KK=	3
I=	4	33	99	K=	9	KK=	4
I=	5	38	85	K=	1	KK=	5
I=	6	47	99	K=	2	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	1.700000	FO=	2.52911
FI=	2.02386	FO=	2.75517
FI=	2.03277	FO=	2.76877
FI=	2.76877	FO=	2.76952

THE SAFETY FACTOR FOR POINT 5IS 2.76952

TRIAL CIRCLE NO 6
 CIRCLE CTR COORDS: X= X= 29.711 Y= 16.711
 ENTRANCE PT COORDS: X= X= 47.111 Y= 9.111
 TRIAL ARC RADIUS= 30.806

5.1.2 Stability Analysis After Dredging

As mentioned in chapter III, the insufficient depth for navigation and contribution to the water pollution of bottom sludge make necessary dredging in Haliç.

Since the bottom and underlying clay formations are very soft and weak, stability of these formations should be evaluated.

Considering the sufficient depth for navigation, the height of dredging will be minimum 6.5 meters between Taşkızak and Haliç Bridge and 4.0 meters from the Haliç Bridge upstream, (Arıcan, 1976). At Taşkızak, The height of bottom sludge is nearly 15 meters. Around Haliç Bridge, it is 6-10 meters.

At Taşkızak, we first analyzed the condition when all of the bottom sludge is dredged and then the case when 6 meters of bottom sludge is dredged. Around Haliç Bridge, dredging of all bottom sludge is necessary for navigation.

So for these cases, stability analysis has been conducted. The conclusions of these results will be discussed in next section.

After dredging of bottom sludge of 10 meters :

The results taken from the computer for cross-section(3-3)B:

Circle NO	Circle Center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
h (a)	99	146	181	107	1.09
k (b)	86	141	180	107	0.99
l (c)	83	150	174	107	1.06
m (d)	82	161	192	107	0.95
n (e)	95	160	189	107	1.07

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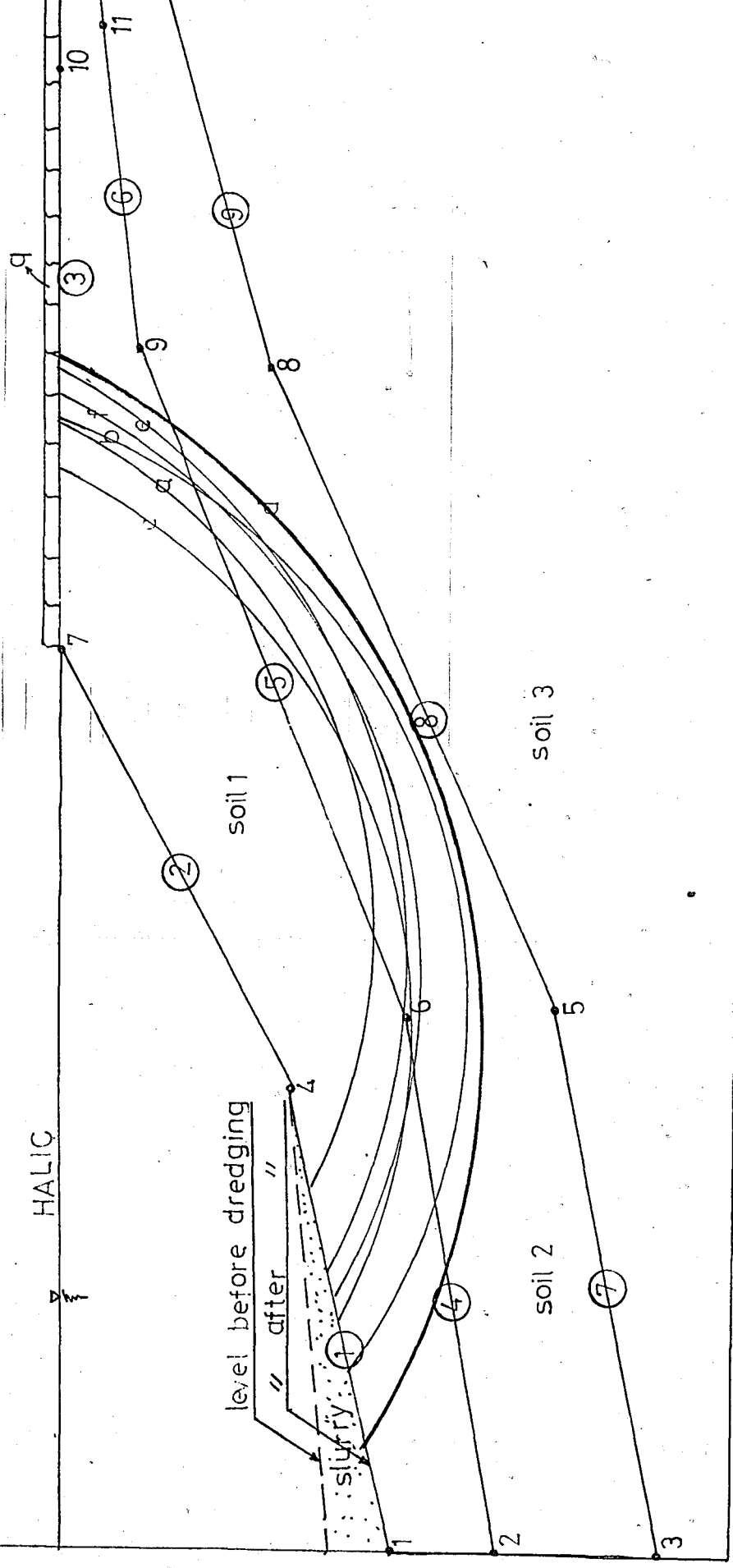


Fig: (3-3)B After dredging

SLOPE STABILITY FOR UNKAP (IT) EXCAVATION, K. THESIS

NO OF LINES 9 NO OF LINE INTERSECT= 12
 NO OF SOILS= 3 NO OF EXTERNAL SOIL LINES= 3
 NO OF X INCREMENTS= 2 NO OF Y INCREMENTS= 2
 INITIAL SLICE WIDTH= 2.0

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INT
1	2	0	74	54	74	69	202399	1
2	3	0	44	69	44	07	542857	4
3	4	0	86	36	233	07	000000	7
4	5	0	94	50	86	50	162588	2
5	6	0	34	94	94	01	407407	6
6	7	0	88	10	237	01	162791	1
7	8	0	38	27	84	27	202308	9
8	9	0	88	73	244	90	303571	3
9	10	0						5
10	11	0						8

LINE NO	INTERSECT X	Y
1	74	54
2	44	69
3	86	36
4	94	50
5	34	94
6	88	10
7	38	27
8	88	73
9		
10		
11		
12		

SOIL NO	DATA ARRAY	LEFT INT	PT INT	SAT	UNIT WT	PHI	COHESION
1	1	4	7	0	7.8	20.0	19.6
2	2	7	7	0	7.8	20.0	19.6
3	3	2	6	0	7.8	20.0	19.6
4	4	6	6	0	7.8	20.0	19.6
5	5	6	6	0	7.8	20.0	19.6
6	6	9	6	0	7.8	20.0	19.6
7	7	5	9	0	7.8	12.0	0.0
8	8	5	8	0	7.8	12.0	0.0
9	9	8	8	0	7.8	12.0	0.0
10	10	3	5	0	7.8	12.0	0.0
11	11	5	8	0	7.8	12.0	0.0
12	12	5	8	0	7.8	12.0	0.0
13	13	3	3	0	3.3	45.0	18.6
14	14	3	3	0	3.3	45.0	18.6
15	15	3	3	0	3.3	45.0	18.6

TRIAL CIRCLE NO 1
 CIRCLE CENTER COORDS: X= 99.802 Y= 46.711
 ENTRANCE PT. COORDS: X= 18.802 Y= 207.111
 TRIAL ARC RADIUS= 90.802

- XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

3	74	1	69	1	K	6	KK	3
4	86	1	50	1	K=	8	KK=	4
5	44	1	07	1	K=	9	KK=	5
6	67	69	83	347	K=	0	KK=	6
7	80	1	07	1	K=	1	KK=	7

AND SLICE WIDTH AND NO OF SLICES

***MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50

FI=	00000	FO=	98488
FI=	98488	FO=	98289
FI=	98289	FO=	98262

THE SAFETY FACTOR FOR POINT 1 IS 0.98262

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 89.711 Y= 44.311
 ENTRANCE PT. COORDS: X= 180.111 Y= 07.111
 TRIAL ARC RADIUS= 97.144

LINE 2 NOT INTERSECTED BY TRIAL CIRCLE

LINE 6 NOT INTERSECTED BY TRIAL CIRCLE

LINE 7 NOT INTERSECTED BY TRIAL CIRCLE

LINE 8 NOT INTERSECTED BY TRIAL CIRCLE

LINE 9 NOT INTERSECTED BY TRIAL CIRCLE

LINE 2 IS NOT INTERSECTED BUT IS IN ARC

DO NOT INTERSECT WITH LINE ARRAY

NO	X	Y
34	735	6102
65	791	4681
167	010	8307
180	111	0731

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	300	54	K	1	KK	1
2	300	36	K	1	KK	2
3	300	36	K	1	KK	3
4	300	36	K	1	KK	3
5	65	46	K	3	KK	3
6	74	69	K	3	KK	4
7	86	27	K	3	KK	5
8	86	50	K	3	KK	6
9	44	07	K	3	KK	7
10	67	83	K	4	KK	7
11	80	07	K	4	KK	7
12	88	73	K	4	KK	8
13	94	94	K	4	KK	9
14	23	07	K	4	KK	10
15	33	07	K	4	KK	11
16	23	07	K	4	KK	11
17	24	90	K	4	KK	12

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	300	61	K	4	KK	1
2	65	46	K	5	KK	2
3	74	69	K	6	KK	3
4	86	50	K	8	KK	4
5	44	07	K	9	KK	5
6	67	83	K	10	KK	6
7	80	07	K	11	KK	7

FIND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI	30000	FO	99209
FI	99209	FO	99004
FI	99004	FO	99090

THE SAFETY FACTOR FOR POINT 2IS 99090

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 86.2 Y= 144.1
 ENTRANCE PT. COORDS: X= 80.0 Y= 107.3
 TRIAL ARC RADIUS= 107.2

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
29	94	60
61	56	46
166	42	82
180	1	07

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	300	54	K	1	KK	1
2	300	36	K	1	KK	2
3	300	36	K	1	KK	3
4	29	60	K	2	KK	3
5	51	55	K	3	KK	3
6	74	69	K	3	KK	4
7	84	27	K	3	KK	5
8	85	50	K	3	KK	6

10	466	077	K=	3	KK=	7
11	680	778	K=	4	KK=	7
12	888	777	K=	4	KK=	8
13	994	942	K=	4	KK=	9
14	337	077	K=	4	KK=	0
15	223	942	K=	4	KK=	1
16	244	900	K=	4	KK=	2

THE APPLICABLE ARRAY ARC INT. FOLLOWS:

1	29	60	K=	4	KK=	1
2	61	46	K=	5	KK=	2
3	74	69	K=	6	KK=	3
4	86	50	K=	8	KK=	4
5	44	07	K=	9	KK=	5
6	65	82	K=	0	KK=	6
7	80	07	K=	1	KK=	7

IND SLICE WIDTH AND NO OF SLICES

***MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI=	00000	FO=	98383
FI=	98383	FO=	98172
FI=	98172	FO=	98444

THE SAFETY FACTOR FOR POINT 3 IS 98.44

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= X= 89.711 Y= 44.717
 ENTRANCE PT. COORDS: X= X= 80.711 Y= 07.717
 TRIAL ARC RADIUS= 98.234

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	36.088	61.742
4	70.733	47.667
5	165.629	82.511
3	180.111	07.711

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	54	K=	1	KK=	1
2	000	36	K=	1	KK=	2
3	000	70	K=	1	KK=	3
4	36	61	K=	2	KK=	3
5	70	47	K=	3	KK=	3
6	74	69	K=	3	KK=	4
7	84	27	K=	3	KK=	5
8	86	50	K=	3	KK=	6
9	44	07	K=	3	KK=	7
10	65	82	K=	4	KK=	7
11	80	07	K=	4	KK=	7
12	000	73	K=	4	KK=	8
13	88	94	K=	4	KK=	8
14	33	07	K=	4	KK=	9
15	237	00	K=	4	KK=	0
16	244	90	K=	4	KK=	1

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	36	088	6	415	K=	4	KK=	1
I=	70	733	47	661	K=	5	KK=	2
I=	74	711	69	711	K=	6	KK=	3
I=	86	711	50	711	K=	8	KK=	4
I=	44	629	07	711	K=	9	KK=	5
I=	65	629	82	711	K=	0	KK=	6
I=	80	629	07	711	K=	1	KK=	7

FIND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50

FI=	1.00000	FO=	99654
FI=	99654	FO=	99609

THE SAFETY FACTOR FOR POINT 4 IS 99609

ID PROGRAM EXECUTION

After Dredging of All Bottom Sludge:

The results taken from the computer for cross-section(8-8)A:

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	86	111	135	81	1.09
b	83	105	118	81	1.03
c	91	108	124	81	1.19
d	98	123	165	81	1.48
e	101	113	153	81	1.52
f	84	120	127	81	1.05
g	82	93	133	81	1.17
m	72	108	136	81	1.02
n	74	117	136	81	0.97
p	81	128	157	81	1.16

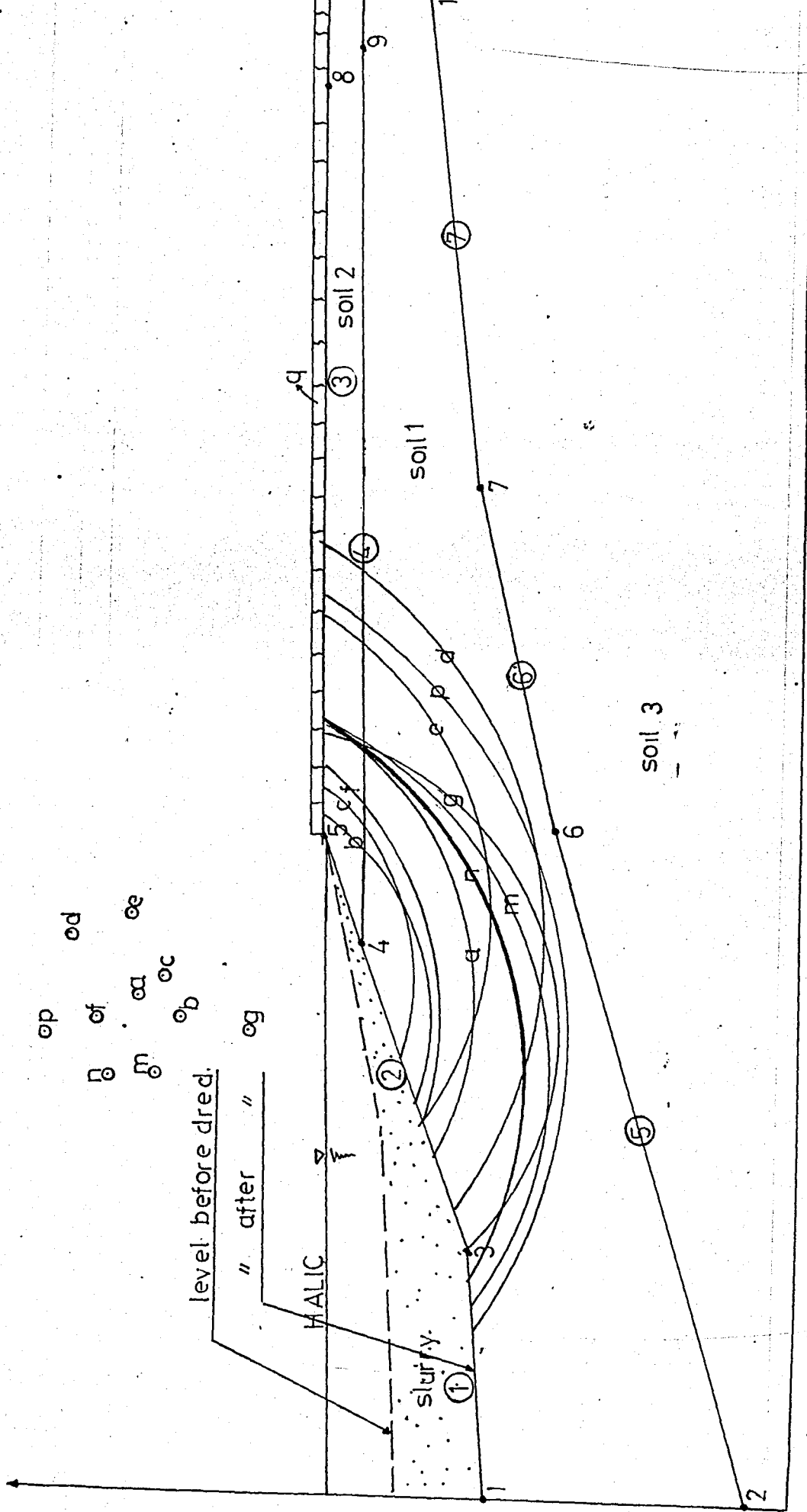


Fig : (8-8) A After dredging of all bottom sludge

SOIL STABILITY FOR TASKIZAK(T)EXCAVE MAHIR KOSELER THESIS

NO OF LINES = 7 NO OF LINE INTERSECT = 10
 NO OF SOILS = 3 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 2 NO OF Y INCREMENTS = 2
 INITIAL SLICE WIDTH = 2.0

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INTER
1	2	00	40	53	40	55	498	3
2	3	00	33	55	30	81	335	4
3	4	00	11	87	24	88	000	8
4	5	00	95	74	24	77	204	9
5	6	00	15	8	11	54	285	6
6	7	00	75	44	17	54	156	2
7	8	00	11	54	24	66	173	7

LINE NO	INTERSECT X	ARRAY Y
1	00	53
2	00	87
3	40	55
4	33	74
5	11	8
6	95	44
7	75	54
8	11	87
9	33	74
10	11	54

LINE NO	DATA ARRAY #	LEFT INT	RIGHT INT	SAT	UNIT WT	PHI	COHESION
1	1	3	4	0	7.8	12	0
2	2	4	9	0	7.8	12	0
3	3	6	7	0	7.8	12	0
4	4	7	0	0	7.8	12	0
5	5	5	9	0	7.8	12	0
6	6	5	8	0	7.8	12	0
7	7	2	6	0	7.8	12	0
8	8	5	7	0	7.8	12	0
9	9	5	8	0	7.8	12	0
10	10	6	7	0	7.8	12	0

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X = 74 Y = 17
 TRIAL PT COORDS: X = 136 Y = 81
 TRIAL ARC RADIUS = 71.694

X LINE 2 NOT INTERSECTED BY TRIAL CIRCLE

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC LINE NO	X	Y
1	38	270
2	132	033
3	136	111
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	53	1	1
2	000	8	1	1
3	38	270	2	2
4	40	111	2	2
5	95	111	2	2
6	133	033	2	2
7	136	111	2	2
8	47	47	3	3
9	74	86	3	3
10	8	111	3	3
11	8	111	3	3
12	8	111	3	3
13	2	4	3	3

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK
1	000	53	3	1
2	000	8	4	2
3	38	270	5	3
4	40	111	6	4
5	95	111	8	5
6	133	033	8	6
7	136	111	9	6

FIND SLICE WIDTH AND NO OF SLICES

FI	FO
00000	98907
98907	98806
98806	98796

THE SAFETY FACTOR FOR POINT TIS 98796

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 77.11 Y= 87.11
 ENTRANCE PT. COORDS: X= 36.11 Y= 86.11
 TRIAL ARC RADIUS= 69.116

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

ARC LINE NO	X	Y
2	43	941
4	131	907
3	136	111
5		
6		
7		
8		
9		
10		
11		
12		
13		

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	53	1	1
2	000	8	1	1
3	43	941	1	1
4	131	907	1	1
5	136	111	1	1

K=	6	7	8	9	10	11	12	13	8	4	7	4	1	1	K=	2	KK=	5
K=	7	8	9	10	11	12	13	14	9	5	8	6	0	1	K=	3	KK=	6
K=	8	9	10	11	12	13	14	15	10	6	9	8	1	1	K=	3	KK=	6
K=	9	10	11	12	13	14	15	16	11	7	10	9	1	1	K=	3	KK=	7
K=	10	11	12	13	14	15	16	17	12	8	11	10	1	1	K=	3	KK=	8
K=	11	12	13	14	15	16	17	18	13	9	12	11	1	1	K=	3	KK=	9
K=	12	13	14	15	16	17	18	19	14	10	13	12	1	1	K=	3	KK=	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	43	94	1	56	475	K=	4	KK=	1
I=	2	95	11	1	74	11	K=	5	KK=	2
I=	3	13	11	1	81	11	K=	6	KK=	3
I=	4	13	11	1	74	860	K=	8	KK=	4
I=	5	36	11	1	81	860	K=	9	KK=	5

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	00237
FI=	00237	FO=	00259

THE SAFETY FACTOR FOR POINT 2 IS 1.00259

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 74.717 Y= 20.311
 ENTRANCE PT. COORDS: X= 36.511 Y= 8.311
 TRIAL ARC RADIUS= 73.246

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
2	40.251	55.716
4	131.702	74.86
5	136.111	81.11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	53	7	K=	1	KK=	1
I=	2	000	58	8	K=	1	KK=	2
I=	3	40	55	6	K=	2	KK=	3
I=	4	40.251	55	6	K=	2	KK=	4
I=	5	95	74	1	K=	2	KK=	5
I=	6	113	81	1	K=	2	KK=	6
I=	7	115	4	1	K=	2	KK=	6
I=	8	131.702	74	8	K=	3	KK=	6
I=	9	136.111	81	8	K=	3	KK=	6
I=	10	175	55	4	K=	3	KK=	7
I=	11	240	81	4	K=	3	KK=	8
I=	12	242	77	4	K=	3	KK=	9
I=	13	244	66	4	K=	3	KK=	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	40	251	55	7	K=	4	KK=	1
I=	2	95	11	74	1	K=	5	KK=	2
I=	3	13	11	81	1	K=	6	KK=	3
I=	4	13	11	74	860	K=	8	KK=	4
I=	5	36	11	81	860	K=	9	KK=	5

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	97779
FI=	97779	FO=	97578
FI=	97578	FO=	97559

TRIAL CIRCLE NO 4
 CIRCLE CENTER COORDS: X= X= 77.711 Y= 20.711
 ENTRANCE PT. COORDS: X= X= 73.36 Y= 81.11
 TRIAL ARC RADIUS= 70.725

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
2	45.282	56.955
3	131.456	74.855
4	136.111	81.111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	53.8	1	1
2	000	82.2	1	2
3	40.000	55.5	1	3
4	45.282	56.955	2	4
5	95.555	74.855	2	5
6	131.456	81.111	2	6
7	136.111	81.111	3	7
8	136.111	81.111	3	8
9	136.111	81.111	3	9
10	244.0	81.111	3	0
11	244.0	81.111	3	0
12	244.0	81.111	3	0
13	244.0	81.111	3	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK
1	45.282	56.955	4	1
2	95.555	74.855	5	2
3	131.456	81.111	6	3
4	136.111	81.111	6	4
5	136.111	81.111	9	5

FIND SLICE WIDTH AND NO OF SLICES

FI= 1.00000 FO= 19932
 FI= .99321 FO= 99259

ABRKPT PRINT: THE SAFETY FACTOR FOR POINT 4 IS .99259

After Dredging of 6m. of Bottom Sludge:

The results taken from the computer for cross-section
(8-8)A are:

Circle NO	Circle Center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	86	III	I35	8I	0.99
b	83	I05	II8	8I	0.95
c	9I	I08	I24	8I	I.II
d	98	I23	I65	8I	I.45
e	I0I	II3	I53	8I	I.40
f	84	I20	I27	8I	I.I2
g	82	93	I33	8I	I.I9
m	72	I08	I36	8I	I.09
n	74	II7	I36	8I	I.00
p	8I	I28	I57	8I	I.I9

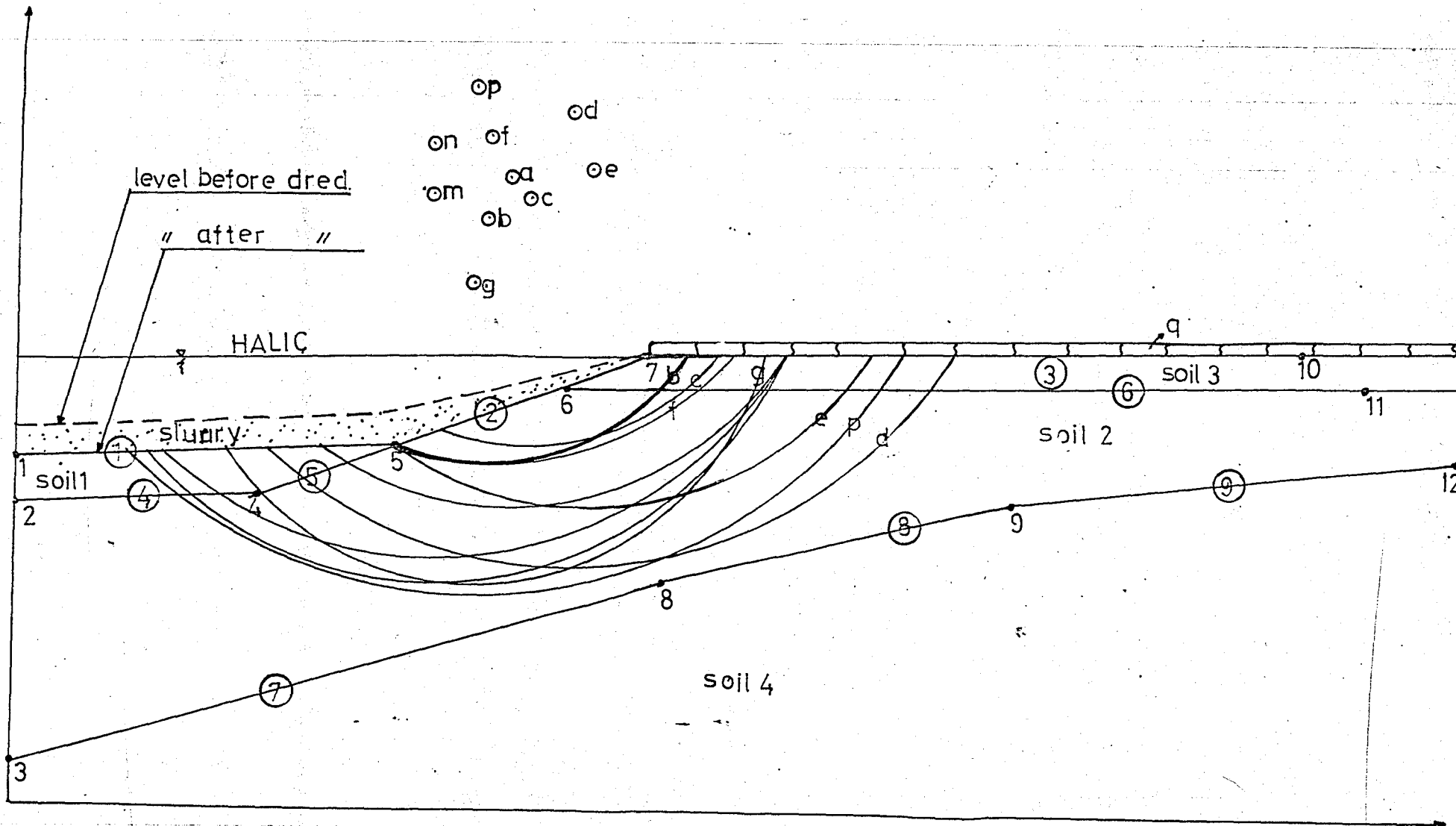


Fig : (8-8)A After Dredging of 6m. of Bottom Sludge

LOPE STABILITY FOR TASKIZAK(I)EXCAVA(2) MAHIR KOSELER THESIS

NO OF LINES = 9 NO OF LINE INTERSECT = 12
 NO OF SOILS = 4 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 2 NO OF Y INCREMENTS = 2
 INITIAL SLICE WIDTH = 2.0

LINE NO	END INT	COORD MATRIX	X1	Y1	X2	Y2	SLOPE	LINE INT
1	00	65	00	62	65	00	000000	1
2	00	13	00	22	13	00	395833	2
3	00	40	00	88	40	00	000000	3
4	00	95	00	55	95	00	498616	4
5	00	15	00	74	15	00	280000	5
6	00	75	00	48	75	00	204082	6
7	00	15	00	55	15	00	280000	7
8	00	75	00	48	75	00	204082	8
9	00	15	00	55	15	00	280000	9
10	00	75	00	48	75	00	204082	10

LINE INTERSECT ARRAY

LINE NO	X	Y
1	00	62
2	00	55
3	00	88
4	00	55
5	40	62
6	95	74
7	15	88
8	75	48
9	15	55
10	75	48
11	24	81
12	24	77
13	24	66

OIL DATA ARRAY

LINE NO	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESION
1	00	55	00	55	12	00
2	00	45	00	55	12	00
3	00	55	00	55	12	00
4	00	55	00	55	12	00
5	40	55	00	55	12	00
6	95	55	00	55	12	00
7	15	55	00	55	12	00
8	75	55	00	55	12	00
9	15	55	00	55	12	00
10	75	55	00	55	12	00
11	24	55	00	55	20	19
12	24	55	00	55	20	19
13	24	55	00	55	45	68
14	24	55	00	55	45	68

TRIAL CIRCLE NO: 1
 TRIAL CTR COORDS: X = 42.438 Y = 83.181
 ENTRANCE PT. COORDS: X = 42.438 Y = 83.181
 TRIAL ARC RADIUS = 42.438

- XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 8 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 9 NOT INTERSECTED BY TRIAL CIRCL

RC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
70	994	6444
124	460	7447
118	111	8151

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	622	1	1
2	000	537	1	1
3	000	811	1	1
4	40	55	1	3
5	65	62	1	5
6	70	64	2	5
7	95	74	2	6
8	112	74	3	7
9	124	81	3	8
10	133	85	3	8
11	140	88	3	9
12	144	88	3	9
13	144	88	3	9
14	24	77	3	11
15	24	66	3	12

THE APPLICABLE ARRAY ARC INT FOLLOWS:

LINE NO	X	Y	K	KK
6	64	44	6	1
7	74	41	7	2
8	74	46	8	3
9	81	51	9	4
11	81	51	11	5

IND SLICE WIDTH AND NO OF SLICES

FI	FO
0000	9639
9639	95874
95874	95797

THE SAFETY FACTOR FOR POINT TIS 95797

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 86.1 Y= 105.1
 ENTRANCE PT COORDS: X= 18.1 Y= 81.1
 TRIAL ARC RADIUS= 40.000

(X) LINE 1 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 4 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 5 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 7 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 8 NOT INTERSECTED BY TRIAL CIRCL

(X) LINE 9 NOT INTERSECTED BY TRIAL CIRCL

RC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
75	983	6641
111	797	7445
118	111	8151

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	622	1	1
2	000	537	1	2

3	40	55	8	K	1	KK	3
4	65	62	5	K	1	KK	5
5	75	66	6	K	2	KK	6
6	95	74	7	K	2	KK	6
7	113	74	8	K	3	KK	7
8	115	84	8	K	3	KK	8
9	118	55	5	K	3	KK	9
10	175	87	8	K	3	KK	0
11	240	77	7	K	3	KK	0
12	242	66	6	K	3	KK	1
13	244			K	3	KK	2
14							
15							

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	75	983	66	4	4	K	6	KK	1
2	95	117	74	4	1	K	7	KK	2
3	113	797	74	4	5	K	8	KK	3
4	118	111	8	1	1	K	9	KK	4
5			8	1	1	K	1	KK	5

FIND SLICE WIDTH AND NO OF SLICES

FI	00000	FO	04952
FI	04952	FO	05709
FI	05709	FO	05820
FI	05820	FO	05837

THE SAFETY FACTOR FOR POINT 2IS 1.05837

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= X= 83.711 Y= 08.211
 ENTRANCE PT. COORDS: X= X= 18.011 Y= 8.211
 TRIAL ARC RADIUS= 44.204

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

2	72	756	65	4
6	71	756	74	5
3	118	111	8	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	0000	62	1	KK	1
2	0000	53	1	KK	2
3	0000	8	1	KK	3
4	40	55	1	KK	4
5	65	62	1	KK	5
6	72	756	3	KK	5
7	95	74	5	KK	6
8	113	74	5	KK	6
9	115	8	3	KK	7
10	118	55	3	KK	8
11	175	87	3	KK	8
12	240	77	3	KK	9
13	242	66	3	KK	0
14			3	KK	0
15			3	KK	1
			3	KK	2

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	72	756	65	37	K=	6	KK=	1
2	95	111	74	45	K=	7	KK=	2
3	113	155	74	45	K=	8	KK=	3
4	113	155	81	45	K=	9	KK=	4
5	118	111	81	45	K=	1	KK=	5

FIND SLICE WIDTH AND NO OF SLICES

FI=	100000	FO=	99844
FI=	99844	FO=	99821

THE SAFETY FACTOR FOR POINT 3IS 99821

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= X= 86711 Y= 108711
 ENTRANCE PT COORDS: X= 18711 Y= 81711
 TRIAL ARC RADIUS= 47869

- XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

LINE NO	77	703	67	10
2	110	981	74	43
3	118	111	81	45

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	0000	62	1	KK=	1
2	0000	53	1	KK=	2
3	0000	88	1	KK=	3
4	40	55	1	KK=	4
5	67	62	1	KK=	5
6	77	62	2	KK=	5
7	95	74	2	KK=	6
8	110	74	3	KK=	6
9	113	81	3	KK=	7
10	118	81	3	KK=	8
11	113	81	3	KK=	8
12	118	81	3	KK=	9
13	75	55	3	KK=	9
14	242	87	3	KK=	10
15	244	77	3	KK=	10
	244	66	3	KK=	12

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	77	703	67	5	KK=	6	KK=	1
2	95	111	74	4	KK=	7	KK=	2
3	110	981	74	4	KK=	8	KK=	3
4	113	155	81	4	KK=	9	KK=	4
5	118	111	81	4	KK=	1	KK=	5

FIND SLICE WIDTH AND NO OF SLICES

FI=	100000	FO=	1305
FI=	1305	FO=	33058
FI=	33058	FO=	3305
FI=	3305	FO=	3339

THE SAFETY FACTOR FOR POINT 4IS 13339

After Dredging of all Bottom Sludge:

The results taken from the computer for cross-section

(8-8)B are:

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	101	110	143	64	1.55
b	97	103	133	64	1.99
c	107	101	139	64	2.59
d	93	108	136	64	1.42
e	109	108	152	64	1.58
f	86	111	133	64	1.35
g	88	103	139	64	1.15

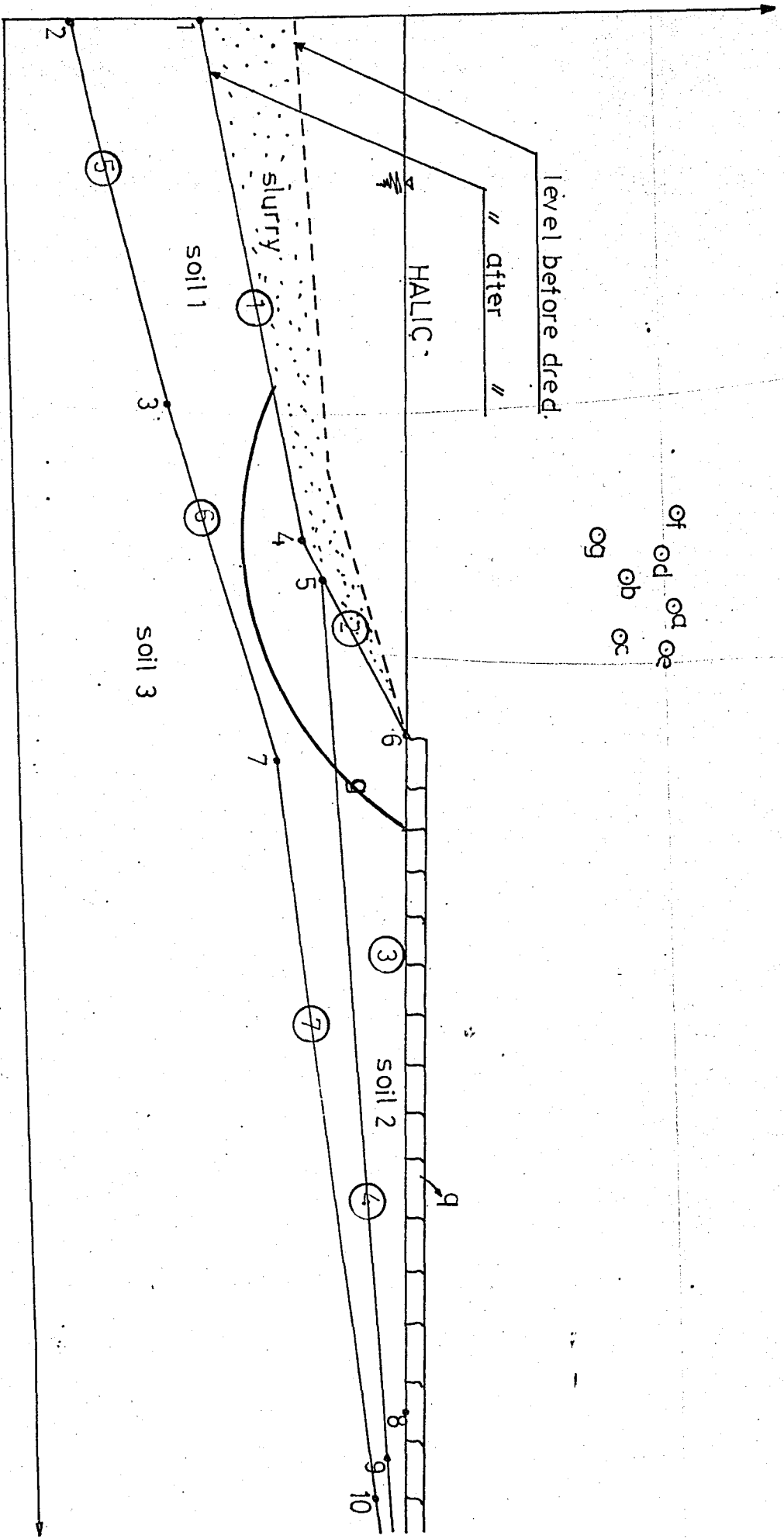


Fig : (8-8) B After Dredging of all bottom Sludge.

OPEN STABILITY FOR TASKIZAK(II) EXCAVA(1) MAHIR KOSELER THESIS

NO OF LINES = 7 NO OF LINE INTERSECT = 10
 NO OF SOILS = 3 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 2 NO OF Y INCREMENTS = 2
 INITIAL SLICE WIDTH = 2.0

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INT
1	2	89	00	33	89	49	179557	4
2	3	124	00	49	24	64	29557	6
3	4	94	00	64	22	64	00000	5
4	5	64	00	52	30	58	44176	5
5	6	64	00	28	64	26	29508	2
6	7	125	00	44	23	44	29508	3
7	8	125	00	56	32	56	11215	7

LINE NO	INTERSECT X	Y
1	00	33
2	00	49
3	64	26
4	94	29
5	94	52
6	124	64
7	125	44
8	229	44
9	230	58
10	232	56

SOIL NO	LINE #	LEFT INT	RT. INT	SAT	UNIT WT	PHI	COHESION
1	1	4	4	00	7.8	12	00
2	2	5	5	00	7.8	12	00
3	3	3	7	00	7.8	12	00
4	4	7	0	00	7.8	12	00
5	5	6	6	00	7.8	12	00
6	6	3	7	00	7.8	12	00
7	7	5	6	00	7.8	20	66
8	8	5	6	00	7.8	20	66
9	9	5	6	00	7.8	20	66
10	10	3	7	00	7.8	45	68
11	11	3	7	00	7.8	45	68
12	12	3	7	00	7.8	45	68

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X = 88.71 Y = 33.11
 ENTRANCE PT. COORDS: X = 39.11 Y = 64.11
 TRIAL ARC RADIUS = 64.203

XX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 **LINE 2 IS NOT INTERSECTED BUT IS IN ARC

LINE NO	INTERSECT WITH X	Y
1	62	34
2	129	04
3	139	11
4	44	31
5	53	65
6	64	11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	33	1	KK=	1
I=	2	000	33	1	KK=	2
I=	3	000	33	1	KK=	2
I=	4	62	44	2	KK=	3
I=	5	64	26	2	KK=	4
I=	6	89	49	2	KK=	5
I=	7	94	52	2	KK=	6
I=	8	24	64	2	KK=	7
I=	9	25	44	2	KK=	7
I=	0	229	53	3	KK=	7
I=	1	39	64	3	KK=	8
I=	2	30	58	3	KK=	9
I=	3	232	56	3	KK=	9

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	62	44	3	KK=	1
I=	2	89	49	5	KK=	2
I=	3	94	52	6	KK=	3
I=	4	24	64	7	KK=	4
I=	5	25	44	9	KK=	5
I=	6	39	64	10	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	3250
FI=	3250	FO=	4830
FI=	4830	FO=	4999
FI=	4999	FO=	5016

THE SAFETY FACTOR FOR POINT TIS 1.15016

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= X= 9 Y= 103
 ENTRANCE PT. COORDS: X= 39 Y= 64
 TRIAL ARC RADIUS= 61.847

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	68	738
4	128	194
3	139	111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	33	1	KK=	1
I=	2	000	33	1	KK=	2
I=	3	000	33	1	KK=	3
I=	4	64	26	2	KK=	3
I=	5	68	45	2	KK=	4
I=	6	89	49	2	KK=	5
I=	7	94	52	2	KK=	6
I=	8	24	64	2	KK=	7
I=	9	25	44	2	KK=	7
I=	0	229	53	3	KK=	7
I=	1	39	64	3	KK=	8
I=	2	30	58	3	KK=	9
I=	3	232	56	3	KK=	9

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	68	45	4	KK=	1
I=	2	89	49	5	KK=	2

3
4
5
6

94
228
339

52
64
53
64

K
K
K
K

6
7
9
0

KK
KK
KK
KK

3
4
5
6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	5468
FI=	15468	FO=	7353
FI=	7353	FO=	7554
FI=	7554	FO=	7575

THE SAFETY FACTOR FOR POINT 2IS 1.17575

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= X= 88.711 Y= 406.711
 ENTRANCE PT. COORDS: X= 39.711 Y= 64.711
 TRIAL ARC RADIUS= 66.068

- XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	63.995	44.60
2	128.227	53.62
3	139.111	64.71

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	63.995	44.60	1	1
2	128.227	53.62	1	2
3	139.111	64.71	2	3
4	89.111	49.111	2	4
5	94.111	52.111	2	5
6	224.111	64.111	2	6
7	225.111	44.111	2	7
8	128.227	53.62	2	8
9	139.111	64.71	3	9
10	229.111	64.71	3	7
11	230.111	58.111	3	8
12	230.111	58.111	3	9
13	232.111	56.111	3	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK
1	63.995	44.60	3	1
2	89.111	49.111	5	2
3	94.111	52.111	6	3
4	124.111	64.111	7	4
5	128.227	53.62	9	5
6	139.111	64.71	0	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	4.43
FI=	4.43	FO=	5831
FI=	5831	FO=	6010
FI=	6010	FO=	6029

THE SAFETY FACTOR FOR POINT 3IS 1.16029

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= X= 91.711 Y= 406.711
 ENTRANCE PT. COORDS: X= 39.711 Y= 64.711
 TRIAL ARC RADIUS= 63.781

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
LINE NO X Y

1	70	467	45	76
4	227	276	53	57
3	139	111	64	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	33	1	KK=	1
I=	2	000	11	1	KK=	2
I=	3	64	26	1	KK=	3
I=	4	70	45	2	KK=	4
I=	5	89	49	2	KK=	5
I=	6	94	52	2	KK=	6
I=	7	124	64	2	KK=	7
I=	8	125	44	2	KK=	8
I=	9	127	53	3	KK=	9
I=	10	139	64	3	KK=	10
I=	11	229	64	3	KK=	11
I=	12	230	58	3	KK=	12
I=	13	232	56	3	KK=	13

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	2	70	45	4	KK=	1
I=	3	89	49	5	KK=	2
I=	4	94	52	6	KK=	3
I=	5	124	64	7	KK=	4
I=	6	127	53	9	KK=	5
I=	6	139	64	10	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	7563
FI=	17563	FO=	9711
FI=	9711	FO=	9937
FI=	9937	FO=	9961

BRKPT PRINTS

THE SAFETY FACTOR FOR POINT 4 IS 1.1996T

After dredging of 8m. of Bottom Sludge

The results taken from the computer for cross-section

(8-8)B are:

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	101	110	143	64	1.46
b	97	103	133	64	2.01
c	107	101	139	64	3.35
d	93	108	136	64	1.33
e	109	108	152	64	1.46
f	86	111	133	64	1.24
g	88	103	139	64	1.01

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og

level before dred.

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HALIC

slurry

soil 1

soil 2

soil 3

soil 4

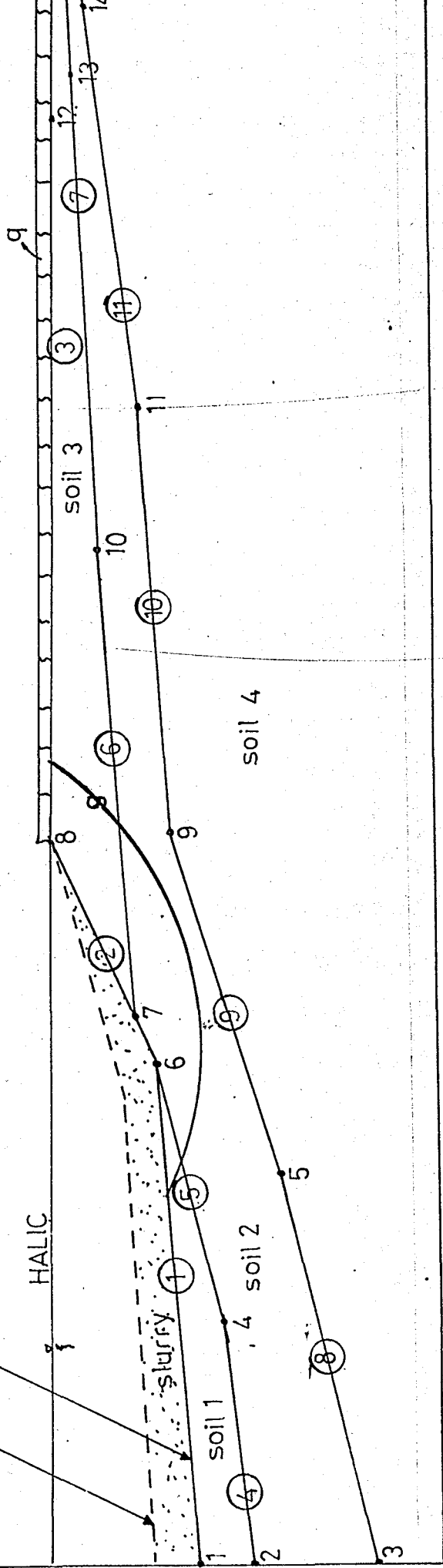


Fig : (8-8) B Dredging of 8m. of Bottom Sludge

STABILITY FOR TASKIZAK(II)EXCAVA(2) MAHIR KOSELER THESIS

F LINES 11 NO OF LINE INTERSECT= 14
 F SOILS= 4 NO OF EXTERNAL SOIL LINES= 3
 F X INCREMENTS= 2 NO OF Y INCREMENTS= 2
 IN ITIAL SLICE WIDTH= 200

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INTER
1	2	0	89	44	28	48	67	6
2	3	0	24	64	33	64	57	7
3	4	0	36	33	33	36	00	8
4	5	0	96	33	66	48	00	4
5	6	0	48	55	44	55	75	7
6	7	0	64	22	30	58	48	10
7	8	0	25	44	25	44	33	3
8	9	0	99	44	99	49	22	3
9	10	0	99	44	32	56	75	5

INTERSECT ARRAY

X	Y
36	42
64	33
89	66
96	26
124	48
125	55
148	44
199	44
229	55
230	64
232	58
232	56

DATA ARRAY

LINE #	LEFT INT	RT INT	SAT	UNIT	WT	PHI	COHESI ON
2	6	6	0	1	5	12	0
3	4	4	0	1	5	12	0
4	6	6	0	1	5	12	0
5	6	6	0	1	5	12	0
6	7	7	0	1	8	12	0
7	4	4	0	1	8	12	0
8	6	6	0	1	8	12	0
9	3	3	0	1	8	12	0
10	5	5	0	1	8	12	0
11	9	9	0	1	8	12	0
12	4	4	0	1	8	12	0
13	8	8	0	2	0	20	6
14	7	7	0	2	0	20	6
15	10	10	0	2	0	20	6
16	3	3	0	2	0	45	6
17	5	5	0	2	0	45	6
18	9	9	0	2	0	45	6
19	4	4	0	2	0	45	6

AL CIRCLE NO 1
 CTR COORDS: X= 88.33 Y= 03.11
 RANCE PT COORDS: X= 39.11 Y= 64.11
 TRIAL ARC RADIUS= 64.203

LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

ARC NO	X	Y
1	58.661	46.06
5	65.928	42.86
6	128.200	52.96
3	139.111	64.11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE	X	Y	K	KK
1	58.661	46.06	1	1
2	58.661	46.06	1	2
3	58.661	46.06	1	3
4	36.111	36.111	1	4
5	58.661	46.06	2	5
6	65.928	42.86	2	5
7	65.928	42.86	3	5
8	89.111	48.111	3	6
9	96.111	49.111	3	7
10	124.225	52.225	3	8
11	128.200	52.96	3	9
12	128.200	52.96	4	9
13	139.111	64.11	4	9
14	139.111	64.11	4	0
15	139.111	64.11	4	1
16	229.111	64.11	4	2
17	230.111	58.11	4	3
18	232.111	56.11	4	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE	X	Y	K	KK
1	58.661	46.06	5	1
2	65.928	42.86	7	2
3	89.111	48.111	8	3
4	96.111	49.111	9	4
5	124.225	52.225	9	5
6	128.200	52.96	2	6
7	139.111	64.11	3	7

FIND SLICE WIDTH AND NO OF SLICES

FI=	1.00000	FO=	0.01086
FI=	0.01086	FO=	0.01225
FI=	0.01225	FO=	0.01243

THE SAFETY FACTOR FOR POINT 1 IS 1.01243

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 9.111 Y= 103.111
 ENTRANCE PT. COORDS: X= 139.111 Y= 64.111
 TRIAL ARC RADIUS= 61.847

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 NO X Y
 66 072 46 56
 72 099 44 26
 127 229 52 91
 139 111 64 11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	42	1	K=	1	KK=	1
2	000	33	1	K=	1	KK=	2
3	000	1	1	K=	1	KK=	3
4	36	36	1	K=	1	KK=	4
5	64	26	1	K=	1	KK=	5
6	66	46	2	K=	2	KK=	5
7	72	44	3	K=	3	KK=	5
8	89	48	3	K=	3	KK=	6
9	96	5	3	K=	3	KK=	7
10	24	64	3	K=	3	KK=	8
11	22	44	3	K=	3	KK=	9
12	27	52	4	K=	4	KK=	9
13	39	64	4	K=	4	KK=	9
14	48	54	4	K=	4	KK=	10
15	99	49	4	K=	4	KK=	11
16	22	64	4	K=	4	KK=	12
17	30	58	4	K=	4	KK=	13
18	23	56	4	K=	4	KK=	14

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	66	072	46	56	K=	6	KK=	1
2	72	099	44	26	K=	7	KK=	2
3	89	111	48	11	K=	8	KK=	3
4	96	111	5	11	K=	9	KK=	4
5	24	111	64	11	K=	10	KK=	5
6	27	229	52	91	K=	12	KK=	6
7	39	111	64	11	K=	13	KK=	7

FIND SLICE WIDTH AND NO OF SLICES
 FI= 00000 FO= 003397
 FI= 03397 FO= 00385
 FI= 0385 FO= 003910

THE SAFETY FACTOR FOR POINT 215 1.03910

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= 88.711 Y= 106.711
 ENTRANCE PT. COORDS: X= 39.711 Y= 64.711
 TRIAL ARC RADIUS= 66.068

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 11 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	60	46
2	31	72
3	19	43
4	72	26
5	11	48
6	28	52
7	5	64
8	11	58
9	11	56
10	11	56
11	11	56

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	KK
1	000	42	1	1
2	000	33	1	1
3	000	11	1	1
4	36	38	1	1
5	60	46	2	2
6	64	26	2	2
7	67	43	3	3
8	89	48	3	3
9	96	5	3	3
10	22	64	3	3
11	22	44	3	3
12	22	52	4	4
13	23	64	4	4
14	48	54	4	4
15	99	49	4	4
16	22	64	4	4
17	23	58	4	4
18	23	56	4	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K	KK
1	60	46	5	5
2	31	72	7	7
3	19	43	8	8
4	72	26	9	9
5	11	48	10	10
6	28	52	10	10
7	5	64	10	10
8	11	58	10	10
9	11	56	10	10

FIND SLICE WIDTH AND NO OF SLICES

FO =	02236
FI =	02525
FO =	02561

THE SAFETY FACTOR FOR POINT 3 IS 0.2561

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= 92 Y= 06
 ENTRANCE PT. COORDS: X= 139 Y= 64
 TRIAL ARC RADIUS= 63.781

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

ARC NO	67	94	5	46	69
LINE NO	73	95	8	44	68
3	126	95	52	85	
5	139	11	64	11	

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	42	1	K=	1	KK=	1
2	000	33	1	K=	1	KK=	2
3	000	11	1	K=	1	KK=	3
4	000	35	1	K=	1	KK=	4
5	36	26	1	K=	1	KK=	5
6	64	46	6	K=	2	KK=	5
7	67	44	6	K=	3	KK=	5
8	73	48	1	K=	3	KK=	6
9	89	5	1	K=	3	KK=	7
10	96	64	4	K=	3	KK=	8
11	24	44	4	K=	3	KK=	9
12	22	52	2	K=	4	KK=	9
13	26	64	4	K=	4	KK=	9
14	39	54	4	K=	4	KK=	0
15	48	49	4	K=	4	KK=	1
16	99	66	4	K=	4	KK=	2
17	23	58	4	K=	4	KK=	3
18	23	56	5	K=	4	KK=	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	67	46	6	K=	6	KK=	1
2	73	44	7	K=	7	KK=	2
3	89	48	8	K=	8	KK=	3
4	96	5	9	K=	9	KK=	4
5	24	64	0	K=	0	KK=	5
6	22	52	2	K=	2	KK=	6
7	26	64	3	K=	3	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	05852
FI=	05852	FO=	06642
FI=	06642	FO=	06744
FI=	06744	FO=	06757

THE SAFETY FACTOR FOR POINT 4 IS 1.06757

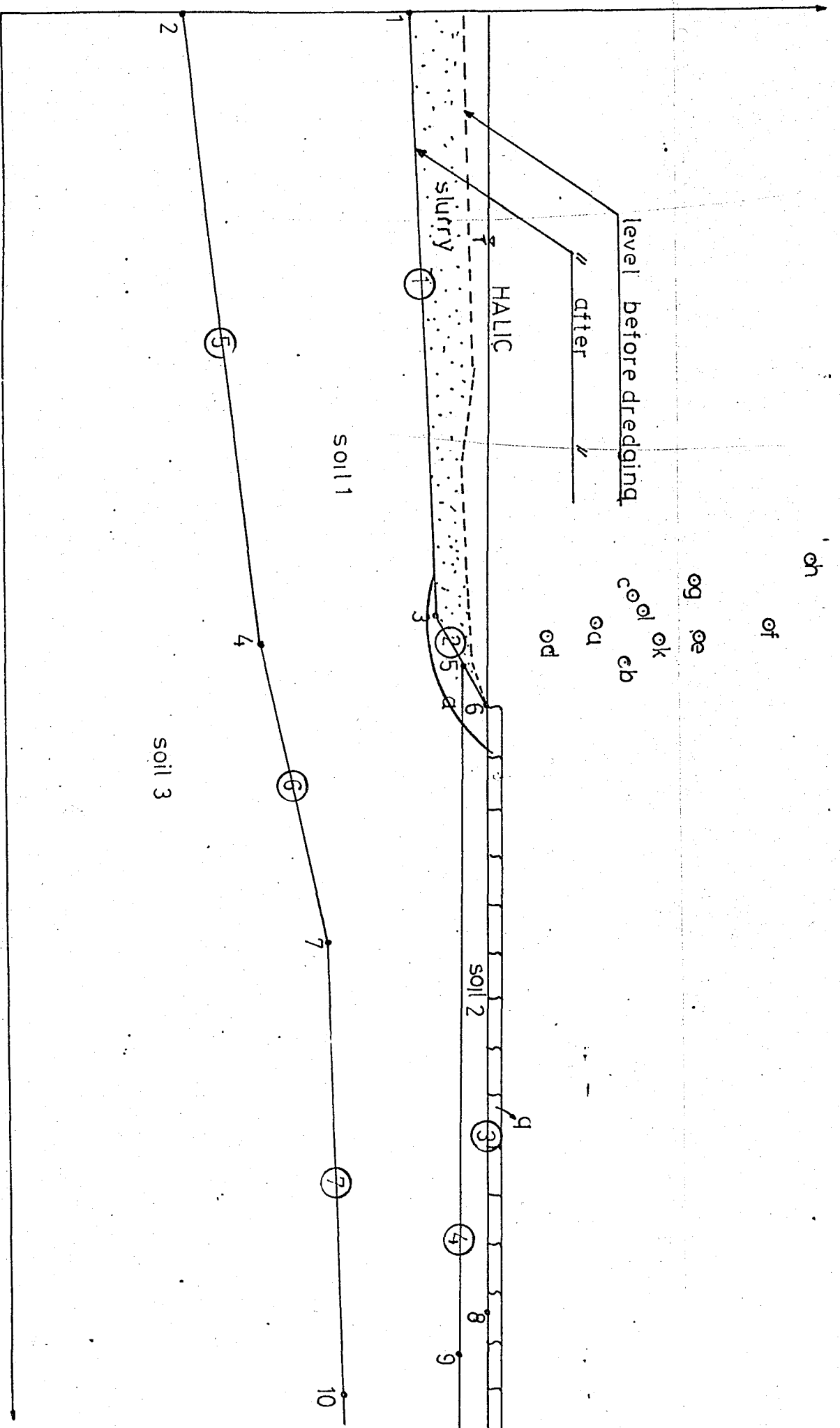
CRKPT PRINTS

After Dredging of 9m. of Bottom Sludge:

The results taken from the computer for cross-section
(IO-IO) A are:

Circle NO	Circle Center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	II7	III	I4I	90	I.0I
b	I25	II6	I56	90	I.4I
c	III	II7	I49	90	I.33
d	II9	IOI	I68	90	2.58
e	II9	I30	I82	90	2.33
f	II6	I43	I87	90	2.44
g	IO8	I29	I6I	90	I.82
h	IO4	I52	I84	90	2.68
k	II9	I23	I45	90	I.35
l	II4	I20	I47	90	I.I7

Fig (10-10) B After Dredging



OF LINES 7 NO OF LINE INTERSECT= 10
 OF SOILS= 3 NO OF EXTERNAL SOIL LINES= 3
 OF X INCREMENTS= 2 NO OF Y INCREMENTS= 2
 IN ITIAL SLICE WIDTH= 2.0

LINE NO	END INT	COORD. MATRIX	Y1	X2	Y2	SLOPE	LINE INTER
1	2	100	78	1	80	1800000	3
2	3	100	80	1	90	475190	5
2	2	132	90	1	90	000000	8
2	2	125	87	1	83	380952	9
2	2	100	35	1	47	000000	4
2	2	120	47	1	59	999076	7
2	2	175	59	1	60	218182	7
						175439	7

INTERSECT ARRAY

NO	X	Y
1	00	78
2	00	35
3	11	80
4	120	47
5	125	87
6	132	90
7	175	59
8	22	90
9	230	83
0	232	60

DATA ARRAY

NO	LINE #	LEFT INT	RT INT	SAT	UNIT	WT	PHI	COHESI ON
1	2	1	3	0		78	12	0
2	3	1	5	0		77	12	0
4	5	2	9	0		77	12	0
5	5	2	4	0		77	12	0
6	6	4	7	0		77	12	0
7	7	5	0	0		77	12	0
2	3	5	8	0		77	20	6
3	3	5	6	0		77	20	6
4	5	5	9	0		77	20	6
5	5	2	4	0		77	20	6
6	6	4	7	0		77	20	6
7	7	5	0	0		77	20	6

AL CIRCLE NO 1
 CLE CTR COORDS: X= 117.511 Y= 17.511
 RANCE PT COORDS: X= 49.511 Y= 90.511
 TRIAL ARC RADIUS= 46.615

LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 LINE 2 IS NOT INTERSECTED BUT IS IN ARC

INTERSECT WITH LINE ARRAY

NO	X	Y
1	83	48
2	146	103
3	149	111
4	79	61
5	86	31
6	90	11

1	83	418	79	613	K=	1	KK=	1
2	11	11	80	11	K=	2	KK=	2
3	20	11	47	11	K=	2	KK=	4
4	22	11	87	11	K=	2	KK=	5
5	32	11	90	11	K=	2	KK=	6
6	46	103	86	51	K=	3	KK=	6
7	49	11	90	11	K=	3	KK=	6
8	49	11	90	11	K=	3	KK=	7
9	75	11	59	11	K=	3	KK=	7
10	22	11	90	11	K=	3	KK=	8
11	23	11	83	11	K=	3	KK=	9
12	30	11	60	11	K=	3	KK=	9
13	23	11	60	11	K=	3	KK=	9

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	83	418	79	613	K=	3	KK=	1
2	11	11	80	11	K=	4	KK=	3
3	25	11	87	11	K=	6	KK=	3
4	32	11	90	11	K=	7	KK=	4
5	46	103	86	51	K=	8	KK=	5
6	49	11	90	11	K=	9	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	30020
FI=	30020	FO=	33068
FI=	33068	FO=	33311
FI=	33311	FO=	33330

THE SAFETY FACTOR FOR POINT 1 IS 1.33330

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= X= 147.77 Y= 177.11
 ENTRANCE PT. COORDS: X= 149.77 Y= 90.77
 TRIAL ARC RADIUS= 44.204

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

ARC NO	X	Y
1	97	79
2	5	74
3	3	86
4	28	32
5	1	90
6	1	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	000	78	11	K=	1	KK=	1	
2	000	35	11	K=	1	KK=	2	
3	90	513	79	740	K=	2	KK=	2
4	11	11	80	11	K=	2	KK=	3
5	11	11	47	11	K=	2	KK=	4
6	11	11	87	11	K=	2	KK=	5
7	11	11	90	11	K=	2	KK=	6
8	45	828	86	322	K=	3	KK=	6
9	49	11	90	11	K=	3	KK=	6
10	75	11	59	11	K=	3	KK=	7
11	22	11	90	11	K=	3	KK=	7
12	23	11	83	11	K=	3	KK=	8
13	23	11	60	11	K=	3	KK=	9

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	90	513	79	740	K=	3	KK=	1
2	11	11	80	11	K=	4	KK=	2

I= 5 6
 I= 6 49 11 82 86 32 2 K= 7 8 KK= 5 6
 90 49 11 82 86 32 2 K= 9 KK= 6

FIND SLICE WIDTH AND NO OF SLICES
 FI= 00000 FO= 18386
 FI= 8386 FO= 20262
 FI= 20262 FO= 20427
 FI= 20427 FO= 20441

THE SAFETY FACTOR FOR POINT 2 IS 1.20441

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= X= 112.1 Y= 20.1
 ENTRANCE PT. COORDS: X= X= 49.1 Y= 90.1
 TRIAL ARC RADIUS= 48.45

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 1 84 551 79763
 4 145 787 86732
 3 149 787 90711

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 I= 2 0000 K= 1 KK= 1
 I= 3 0000 K= 1 KK= 2
 I= 4 84 551 79763 K= 2 KK= 2
 I= 5 112 111 80711 K= 2 KK= 3
 I= 6 125 111 87711 K= 2 KK= 5
 I= 7 32 111 90711 K= 2 KK= 6
 I= 8 45 787 86732 K= 3 KK= 6
 I= 9 149 787 90711 K= 3 KK= 7
 I= 10 75 111 59711 K= 3 KK= 8
 I= 11 229 111 90711 K= 3 KK= 8
 I= 12 230 111 83711 K= 3 KK= 9
 I= 13 232 111 60711 K= 3 KK= 9

THE APPLICABLE ARRAY ARCINT FOLLOWS:
 I= 2 84 551 79763 K= 3 KK= 1
 I= 3 112 111 80711 K= 6 KK= 3
 I= 4 125 111 87711 K= 7 KK= 4
 I= 5 145 787 86732 K= 8 KK= 5
 I= 6 149 787 90711 K= 9 KK= 6

FIND SLICE WIDTH AND NO OF SLICES
 FI= 00000 FO= 25794
 FI= 25794 FO= 28340
 FI= 28340 FO= 28544
 FI= 28544 FO= 28560

THE SAFETY FACTOR FOR POINT 3 IS 1.28560

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= X= 149.1 Y= 20.1
 ENTRANCE PT. COORDS: X= X= 49.1 Y= 90.1
 TRIAL ARC RADIUS= 46.98

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 1 91.830 79.76
 2 145.481 86.33
 3 149.1 90.1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	78	1	K=	1	KK=	1
I=	2	000	35	1	K=	1	KK=	2
I=	3	830	79	4	K=	2	KK=	3
I=	4	11	80	1	K=	2	KK=	4
I=	5	20	47	1	K=	2	KK=	5
I=	6	25	87	1	K=	2	KK=	6
I=	7	45	90	1	K=	2	KK=	6
I=	8	55	86	3	K=	3	KK=	6
I=	9	48	90	1	K=	3	KK=	6
I=	10	75	59	1	K=	3	KK=	7
I=	11	9	90	1	K=	3	KK=	8
I=	12	23	83	1	K=	3	KK=	9
I=	13	32	60	1	K=	3	KK=	9

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	91.830	79.764	K=	3	KK=	1
I=	2	145.481	80.1	K=	4	KK=	2
I=	3	149.1	87.1	K=	6	KK=	3
I=	4	32	90.1	K=	7	KK=	4
I=	5	45	86.335	K=	8	KK=	5
I=	6	49	90.1	K=	9	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	5570
FI=	5570	FO=	7126
FI=	7126	FO=	7263
FI=	7263	FO=	7274

PROGRAM EXECUTION THE SAFETY FACTOR FOR POINT 4 IS 1.17274

After Dredging of Bottom Sludge:

The results taken from the computer for cross-section
(10-10)B are:

Circle NO	Circle center Coordinates		Entrance Points		FACTOR OF SAFETY
	X	Y	X	Y	
a	I23	II3	I47	9I	I.28
b	I29	II2	I49	9I	2.0I
c	I25	I23	I58	9I	I.32
d	II6	I28	I57	9I	I.46
e	I2I	I37	I65	9I	I.52
f	I07	I52	I69	9I	2.19
g	I09	I39	I8I	9I	2.93
h	II4	II5	I60	9I	I.19

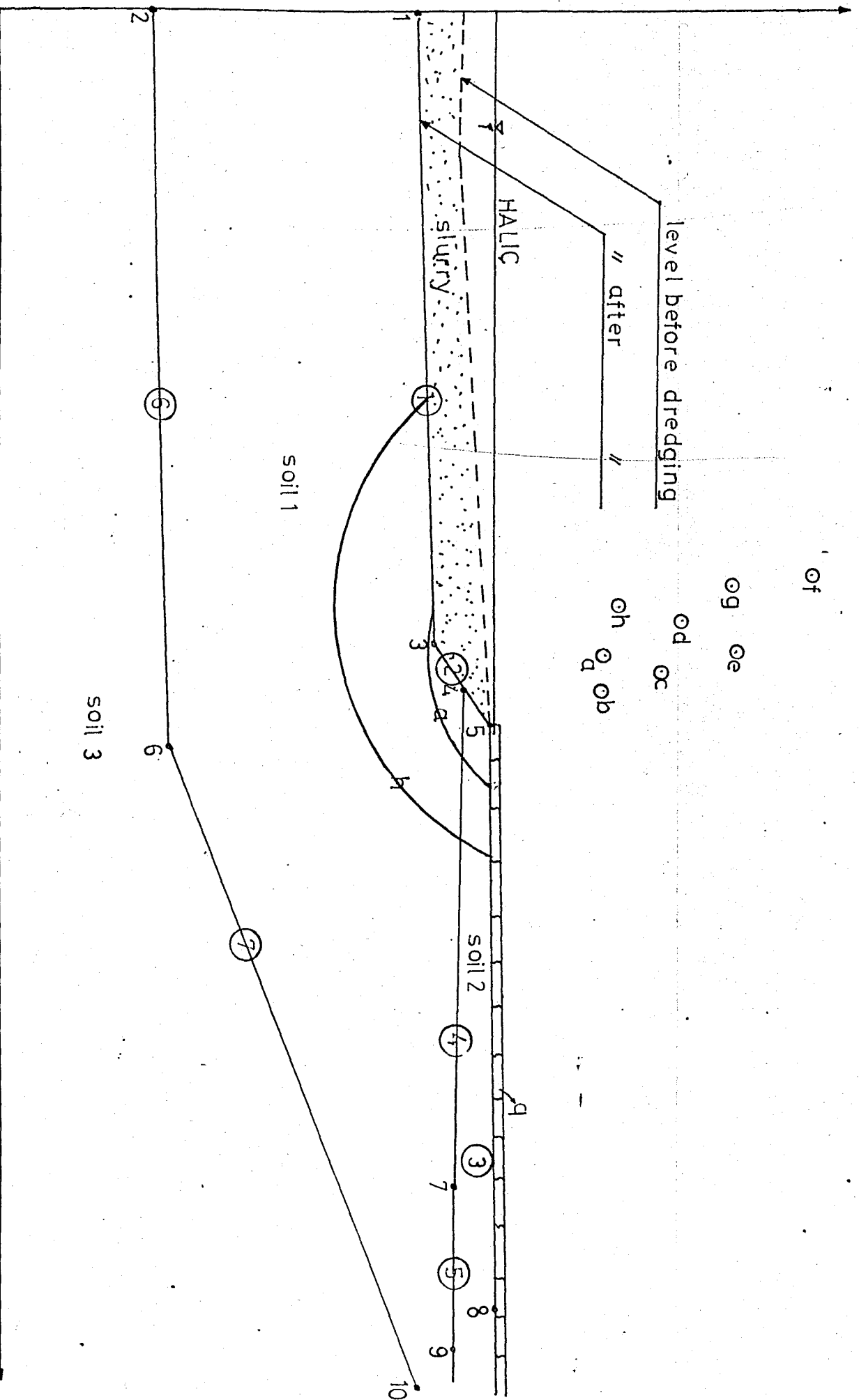


Fig (10-10) B After Dredging

OF LINES = 7 NO OF LINE INTERSECT = 10
 OF SOILS = 3 NO OF EXTERNAL SOIL LINES = 3
 OF X INCREMENTS = 3 NO OF Y INCREMENTS = 3
 INITIAL SLICE WIDTH = 2.0

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INTE
1	2	18	100	808	133	808	000000	5
2	3	26	100	908	333	908	555556	5
3	2	28	100	808	333	808	000000	4
4	2	14	100	808	222	808	334883	7
5	2	14	100	808	333	808	000000	2
6	2	38	100	808	222	808	000000	7
7	2	38	100	808	333	808	000000	2

LINE INTERSECT ARRAY

LINE NO	X	Y
1	00	83
2	00	33
3	00	86
4	29	86
5	36	99
6	38	33
7	44	83
8	22	99
9	33	83
0	35	87

SOIL DATA ARRAY

LINE NO	LINE #	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESI ON
1	2	3	4	00	78	12	00
2	4	7	7	00	78	22	00
3	5	7	9	00	78	12	00
4	6	2	6	00	78	22	00
5	7	6	5	00	78	22	00
6	2	4	8	00	78	20	66
7	3	5	7	00	78	20	66
8	4	7	9	00	78	20	66
9	5	4	7	00	78	20	66
0	6	2	6	00	77	45	66

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X = 147.1 Y = 151.1
 ENTRANCE PT COORDS: X = 160.4 Y = 91.1
 TRIAL ARC RADIUS = 51.884

XX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 *LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

ARC NO	X	Y
1	74	99
2	156	452
3	160	111

I=	2	74	000	8	K=	1	KK=	1
I=	3	18	000	8	K=	1	KK=	2
I=	4	28	000	8	K=	2	KK=	3
I=	5	36	000	8	K=	2	KK=	5
I=	6	38	000	8	K=	2	KK=	6
I=	7	56	000	8	K=	2	KK=	6
I=	8	60	000	8	K=	3	KK=	6
I=	9	14	000	8	K=	3	KK=	7
I=	10	21	000	8	K=	3	KK=	8
I=	11	33	000	8	K=	3	KK=	9
I=	12	33	000	8	K=	3	KK=	9
I=	13	24	000	8	K=	3	KK=	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	74	000	8	K=	3	KK=	1
I=	2	18	000	8	K=	4	KK=	2
I=	3	28	000	8	K=	5	KK=	3
I=	4	36	000	8	K=	6	KK=	4
I=	5	38	000	8	K=	8	KK=	5
I=	6	56	000	8	K=	9	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

FI=	00000	FO=	88463
FI=	88463	FO=	98694
FI=	98694	FO=	99360
FI=	99360	FO=	99401

THE SAFETY FACTOR FOR POINT 1 IS 1.99401

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= X= 18.711 Y= 15.111
 ENTRANCE PT. COORDS: X= X= 16.011 Y= 9.111
 TRIAL ARC RADIUS= 48.374

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	83.702	8.111
2	156.077	8.511
3	160.111	9.111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	8	K=	1	KK=	1
I=	2	000	8	K=	1	KK=	2
I=	3	83	8	K=	2	KK=	3
I=	4	18	8	K=	2	KK=	5
I=	5	28	8	K=	2	KK=	6
I=	6	36	8	K=	2	KK=	6
I=	7	38	8	K=	3	KK=	6
I=	8	56	8	K=	3	KK=	7
I=	9	60	8	K=	3	KK=	8
I=	10	14	8	K=	3	KK=	9
I=	11	21	8	K=	3	KK=	9
I=	12	33	8	K=	3	KK=	9
I=	13	24	8	K=	3	KK=	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	83	8	K=	3	KK=	1
I=	2	18	8	K=	4	KK=	2

I= 5
I= 6
156.077
160.111
85.435
93.211
K= 8
K= 9
KK= 5
KK= 6

FIND SLICE WIDTH AND NO OF SLICES
FI= 00000 FO= 63872
FI= 63872 FO= 71216
FI= 71216 FO= 71757
FI= 71757 FO= 71795

THE SAFETY FACTOR FOR POINT 2IS 1.71795

TRIAL CIRCLE NO 3
CIRCLE CTR COORDS: X= X= 122.111 Y= 15.111
ENTRANCE PT COORDS: X= X= 160.111 Y= 9.111
TRIAL ARC RADIUS= 44.944

XXX LINE 2NOT INTERSECTED BY TRIAL CIRCL
XXX LINE 5NOT INTERSECTED BY TRIAL CIRCL
XXX LINE 6NOT INTERSECTED BY TRIAL CIRCL
XXX LINE 7NOT INTERSECTED BY TRIAL CIRCL

***LINE 2IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY
LINE NO X Y
1 92.717 81.111
2 155.615 85.111
3 160.111 91.111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
I= 1 00000 81.111 K= 1 KK= 1
I= 2 00000 83.111 K= 1 KK= 2
I= 3 71717 88.111 K= 2 KK= 3
I= 4 18.111 88.111 K= 2 KK= 4
I= 5 28.111 86.111 K= 2 KK= 5
I= 6 336.111 99.111 K= 2 KK= 6
I= 7 338.111 83.111 K= 2 KK= 6
I= 8 55.615 85.111 K= 2 KK= 6
I= 9 60.111 91.111 K= 3 KK= 6
I= 10 214.111 88.111 K= 3 KK= 7
I= 11 233.111 99.111 K= 3 KK= 8
I= 12 336.111 85.111 K= 3 KK= 9
I= 13 240.111 73.111 K= 3 KK= 10

THE APPLICABLE ARRAY ARCINT FOLLOWS:
I= 1 92.717 81.111 K= 3 KK= 1
I= 2 18.111 88.111 K= 4 KK= 2
I= 3 28.111 86.111 K= 5 KK= 3
I= 4 336.111 99.111 K= 6 KK= 4
I= 5 338.111 83.111 K= 8 KK= 5
I= 6 55.615 85.111 K= 9 KK= 6
I= 7 60.111 91.111 K= 9 KK= 6

FIND SLICE WIDTH AND NO OF SLICES
FI= 00000 FO= 44986
FI= 44986 FO= 50.42
FI= 50.42 FO= 50566
FI= 50566 FO= 50599

THE SAFETY FACTOR FOR POINT 3IS 1.50599

TRIAL CIRCLE NO 4
CIRCLE CTR COORDS: X= X= 143.111 Y= 19.111
ENTRANCE PT COORDS: X= X= 160.111 Y= 9.111
TRIAL ARC RADIUS= 53.852

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	75	81
2	953	1
3	155	85
4	1897	4
5	160	9
6	11	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K	K	K
1	000	000	1	1	1
2	000	000	1	1	1
3	75	953	2	2	2
4	118	886	2	2	3
5	128	886	2	2	4
6	133	886	2	2	5
7	133	886	2	2	6
8	133	886	2	2	6
9	133	886	2	2	6
10	133	886	2	2	6
11	133	886	2	2	6
12	133	886	2	2	6
13	133	886	2	2	6
14	133	886	2	2	6
15	133	886	2	2	6
16	133	886	2	2	6
17	133	886	2	2	6
18	133	886	2	2	6
19	133	886	2	2	6
20	133	886	2	2	6
21	133	886	2	2	6
22	133	886	2	2	6
23	133	886	2	2	6
24	133	886	2	2	6
25	133	886	2	2	6
26	133	886	2	2	6
27	133	886	2	2	6
28	133	886	2	2	6
29	133	886	2	2	6
30	133	886	2	2	6
31	133	886	2	2	6
32	133	886	2	2	6
33	133	886	2	2	6
34	133	886	2	2	6
35	133	886	2	2	6
36	133	886	2	2	6
37	133	886	2	2	6
38	133	886	2	2	6
39	133	886	2	2	6
40	133	886	2	2	6
41	133	886	2	2	6
42	133	886	2	2	6
43	133	886	2	2	6
44	133	886	2	2	6
45	133	886	2	2	6
46	133	886	2	2	6
47	133	886	2	2	6
48	133	886	2	2	6
49	133	886	2	2	6
50	133	886	2	2	6
51	133	886	2	2	6
52	133	886	2	2	6
53	133	886	2	2	6
54	133	886	2	2	6
55	133	886	2	2	6
56	133	886	2	2	6
57	133	886	2	2	6
58	133	886	2	2	6
59	133	886	2	2	6
60	133	886	2	2	6
61	133	886	2	2	6
62	133	886	2	2	6
63	133	886	2	2	6
64	133	886	2	2	6
65	133	886	2	2	6
66	133	886	2	2	6
67	133	886	2	2	6
68	133	886	2	2	6
69	133	886	2	2	6
70	133	886	2	2	6
71	133	886	2	2	6
72	133	886	2	2	6
73	133	886	2	2	6

THE APPLICABLE ARRAY ARC INT FOLLOWS:

LINE NO	X	Y	K	K	K
1	000	000	3	3	1
2	75	953	4	4	2
3	118	886	5	5	3
4	128	886	6	6	4
5	133	886	8	8	5
6	133	886	9	9	6

FIND SLICE WIDTH AND NO OF SLICES

FI	FO	FO	FO	FO
000000	78490	78490	78490	78490
78490	87092	87092	87092	87092
87092	87647	87647	87647	87647
87647	87681	87681	87681	87681

THE SAFETY FACTOR FOR POINT 4 IS 1.87681

TRIAL CIRCLE NO 5
 CIRCLE CTR COORDS: X= 118.7 Y= 19.1
 ENTRANCE PT. COORDS: X= 160.1 Y= 19.1
 TRIAL ARC RADIUS= 50.478

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	8	K=	1	KK=	1
I=	2	000	3	K=	1	KK=	2
I=	3	000	3	K=	2	KK=	2
I=	4	885	8	K=	2	KK=	3
I=	5	111	8	K=	2	KK=	4
I=	6	111	8	K=	2	KK=	5
I=	7	111	8	K=	2	KK=	6
I=	8	111	8	K=	2	KK=	6
I=	9	111	8	K=	3	KK=	6
I=	10	111	8	K=	3	KK=	7
I=	11	111	8	K=	3	KK=	8
I=	12	111	8	K=	3	KK=	9
I=	13	111	7	K=	3	KK=	0

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	8	8	K=	3	KK=	1
I=	2	8	8	K=	4	KK=	2
I=	3	8	8	K=	5	KK=	3
I=	4	8	8	K=	6	KK=	4
I=	5	8	8	K=	8	KK=	5
I=	6	8	8	K=	9	KK=	6

FIND SLICE WIDTH AND NO OF SLICES

F=	00000	FO=	55968
F=	55968	FO=	6209
F=	6209	FO=	62537
F=	62537	FO=	62569

THE SAFETY FACTOR FOR POINT SIS $F_s = 6.2569$

TRIAL CIRCLE NO 6
 CIRCLE CTR COORDS: X= X= 22.11 Y= 19.11
 ENTRANCE PT. COORDS: X= 60.11 Y= 9.11
 TRIAL ARC RADIUS= 47.202

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 ***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
1	94	11
2	154	92
3	160	11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	8	K=	1	KK=	1
I=	2	000	3	K=	1	KK=	2
I=	3	000	3	K=	2	KK=	2
I=	4	94	8	K=	2	KK=	3
I=	5	111	8	K=	2	KK=	4
I=	6	111	8	K=	2	KK=	5
I=	7	111	8	K=	2	KK=	6
I=	8	111	8	K=	2	KK=	6
I=	9	111	8	K=	3	KK=	6
I=	10	111	8	K=	3	KK=	7
I=	11	111	8	K=	3	KK=	7
I=	12	111	8	K=	3	KK=	8
I=	13	111	9	K=	3	KK=	8

5.2 CONCLUSIONS AND RECOMMENDATIONS

The summary of the geological and geotechnical evaluations may be stated as follows:

1. The main formations in the vicinity of Haliç are Paleozoic graywacke, clayey shist and limestone. Surfaces of these fissured and folded formations are decomposed and their compressive strength and unit weight increase with depth.

2. The tertiary formations of sands and gravels are not common in the area. The sand and clay formations, which are cross-bedded and not cemented, are eroded and transported easily.

3. The quarternary clay formations are very common in the whole vicinity of Haliç and an artificial fill is encountered above sedimentary layer and fill are ^{not} uniform.

4. The eroded materials from all formations are transported to Haliç. These eroded materials are mostly decomposed graywacke and shales and consist of fine quarst sands, silts, clays, muscovite particles and organic materials?

5. The origin of the geotechnical problems in the vicinity of Haliç is soft sedimentary layer (usually contains soft silty clay) over the graywacke bedrock.

6. The natural water content of this silty clay formation is very high and the shear strength is very low.

7. In the transverse direction to the shore line, the thickness of clay layer increases in a considerably amount towards Haliç and causing differential settlement problems for the buildings which are located on the shore.

8. The steep slope of the bedrock surface towards Haliç causes stability problem for the clay formation.

9. From the evaluation of over 135 shear tests, it is determined that shear strength variation with depth is linear, (Akşit, 1977) and therefore it is concluded that the silty clay formation is Normally Consolidated.

10. It is determined that stability of shores is above dangerous limits. (In Fermececiler, between Azapkapı and Karaköy, minimum factor of safety for slope stability is found as 1.116) (See slope stability analysis for cross-section (3-3)B) Also, it is determined that shores dredging of bottom sludge can cause slides along the shores. (in cross-section (8-8)B, in Taşkızak, minimum factor of safety for slope stability after dredging is found as 0.95) So we have to take the necessary precautions. These precautions are explained in Recommendations.

For future geological and geotechnical studies and dredging of bottom sludge in vicinity of Haliç, the following recommendations are given:

1. Deeper boreholes should be drilled at certain locations and the samples should be kept for investigators to obtain detailed informations about soil properties.

2. The quantity of the materials transported and de-

posited by Creeks should be estimated.

3. The basic parameters and variation of these parameters with depth in artificial fill and sedimentary layer should be determined at various locations.

4. Because the stability of shores is above dangerous limits, great care has to be given, when constructing any major building along the shore. If possible the best solution is to leave a 100 to 200 meters wide band along the shore for parks, play grounds and picnic areas. This will contribute to the improvement of the touristic value of the area, and as well to the stability problem of the shores. Planted trees will help to decrease the water content of the soil and using this area as a park will reduce the distributed load which is present because of the existing structures. As an example the elimination of the surcharge will increase the Safety Factor from 1.116 to 1.21 at cross-section (3-3)B.

5. As it is seen from the results, during dredging, shores of Haliç may slide. To prevent sliding of shores, some precautions should be taken. Some methods used to prevent sliding are:

a) Loading on toe: (Masonry Wall)

The simplest way of toe loading is to built masonry wall. Better forms are to built reinforced retaining structure wood, concrete piles or palplanges. These structures are useful if they are dimensioned conveniently and hammered down deeply enough and no excavations are made under these structures. On the other hand the depth of the critical slope circle should be known.

In the case of the stabilisation of Haliç's shore , difficulties such as working under sea water necessitates convenient equipment. This method may not be economical. The same result can also be achieved easily by spreading a layer of sand or rock material upon the slope.(Peynircioğlu, 1961)

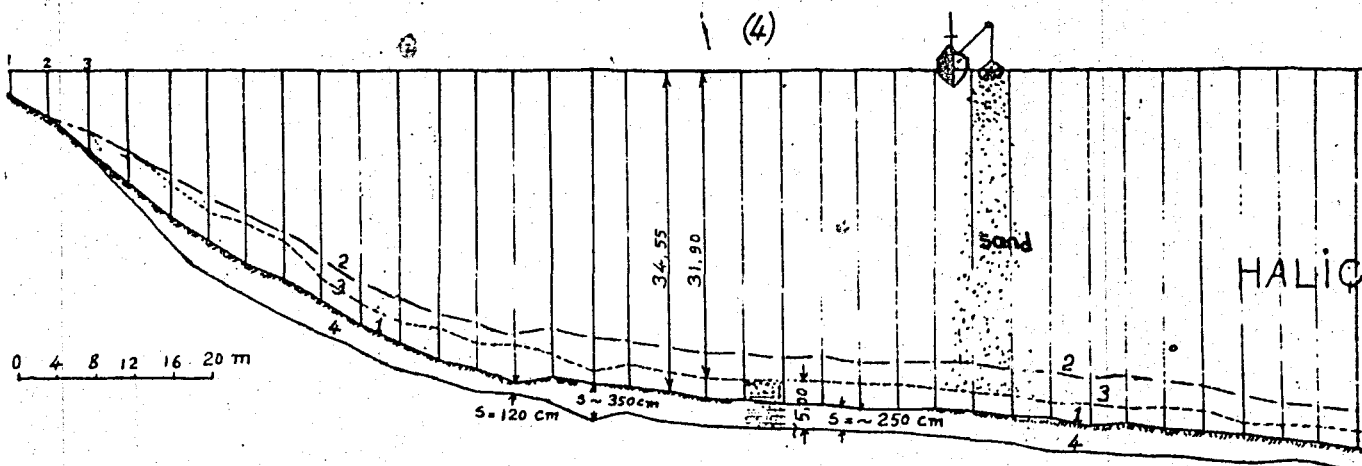


Fig. 5: Spreading layers of sand for stabilization of Ist. Commercial House's shore(Peynircioğlu,1961)

The situation after spreading the layer of sand or rock material is controlled by means of computer program.(The unit weight for the material γ_n is taken as 2.2 t/m^3) It is observed that the factor of safety in the most critical region , Taşkızak (8-8)^A, changed from 0.95 to 1.01 after this procedure. This may be more economical than building a retaining wall.

NO OF LINES = 10 NO OF LINE INTERSECT = 13
 NO OF SOILS = 5 NO OF EXTERNAL SOIL LINES = 3
 NO OF X INCREMENTS = 2 NO OF Y INCREMENTS = 2
 INITIAL SLICE WIDTH = 200

LINE END COORD MATRIX

LINE NO	NO	INT	X1	X2	Y1	Y2	LOPE	LINE INTER
1	1	1	50	62	00	00	000000	1
1	2	1	113	82	00	00	000000	5
1	3	1	40	53	00	00	000000	2
1	4	1	65	55	00	00	000000	4
1	5	1	95	66	00	00	000000	7
1	6	1	15	74	00	00	000000	3
1	7	1	175	88	00	00	000000	6
1	8	1		55	00	00	000000	8
1	9	1		62	00	00	000000	9
1	10	1		74	00	00	000000	10

INTERSECT ARRAY

LINE NO	X	Y
1	00	62
2	00	53
3	00	55
4	40	62
5	50	74
6	55	88
7	65	55
8	95	66
9	15	74
10	175	88

SOIL DATA ARRAY

LINE NO	LINE #	LEFT INT	RT INT	SAT	UNIT WT	PHI	COHESI ON
1	1	50	62	00	1.5	12	00
1	2	113	82	00	1.5	12	00
1	3	40	53	00	1.5	12	00
1	4	65	55	00	1.5	12	00
1	5	95	66	00	1.5	12	00
1	6	15	74	00	1.5	12	00
1	7	175	88	00	1.5	12	00
1	8		55	00	1.5	12	00
1	9		62	00	1.5	12	00
1	10		74	00	1.5	12	00

TRIAL CIRCLE NO 1
 CIRCLE CTR COORDS: X = 83 Y = 05
 ENTRANCE PT COORDS: X = 18 Y = 05
 TRIAL ARC RADIUS = 42.438

LINE NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 2 65 169 66 65
 3 70 994 64 440
 4 112 460 74 465
 5 118 111 8 111

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 I= 1 000 62 1 1 KK= 1
 I= 2 000 53 1 1 KK= 1
 I= 3 000 8 1 1 KK= 1
 I= 4 40 55 2 1 KK= 1
 I= 5 50 62 2 1 KK= 1
 I= 6 65 66 2 1 KK= 1
 I= 7 70 66 2 2 KK= 1
 I= 8 95 64 3 1 KK= 1
 I= 9 112 74 4 1 KK= 1
 I= 10 113 8 4 1 KK= 1
 I= 11 115 4 4 1 KK= 1
 I= 12 118 4 4 1 KK= 1
 I= 13 175 5 4 1 KK= 1
 I= 14 240 8 4 1 KK= 1
 I= 15 242 7 4 1 KK= 1
 I= 16 244 6 4 1 KK= 1
 I= 17 244 6 4 1 KK= 1

THE APPLICABLE ARRAY ARCINT FOLLOWS:
 I= 2 65 169 66 652 K= 7 KK= 1
 I= 3 70 994 64 440 K= 8 KK= 1
 I= 4 95 111 74 111 K= 9 KK= 1
 I= 5 112 460 74 465 K= 10 KK= 1
 I= 6 113 111 8 111 K= 11 KK= 1
 I= 7 118 111 8 111 K= 12 KK= 1

FIND SLICE WIDTH AND NO OF SLICES
 FI= 1.00000 FO= 1.02734
 FI= 1.02734 FO= 1.02950
 FI= 1.02950 FO= 1.02966

THE SAFETY FACTOR FOR POINT IS 1.02966

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 86.111 Y= 05.111
 ENTRANCE PT COORDS: X= 118.111 Y= 81.111
 TRIAL ARC RADIUS= 40.000

XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 2 70 532 68 27
 6 75 983 66 44
 7 11 797 74 45
 3 18 111 8 1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:
 I= 1 000 62 1 1 K= 1 KK= 1
 I= 2 000 53 1 1 K= 1 KK= 2
 I= 3 000 8 1 1 K= 1 KK= 3
 I= 4 40 55 1 1 K= 1 KK= 4
 I= 5 50 62 1 1 K= 1 KK= 5
 I= 6 65 62 1 1 K= 1 KK= 6
 I= 7 75 68 2 1 K= 2 KK= 6
 I= 8 75 66 4 1 K= 3 KK= 6
 I= 9 95 74 4 1 K= 3 KK= 7
 I= 10 11 74 4 2 K= 4 KK= 7
 I= 11 13 8 1 1 K= 4 KK= 8
 I= 12 13 8 1 1 K= 4 KK= 9
 I= 13 13 8 1 1 K= 4 KK= 9
 I= 14 13 8 1 1 K= 4 KK= 9
 I= 15 13 8 1 1 K= 4 KK= 9
 I= 16 24 77 4 1 K= 4 KK= 2
 I= 17 24 66 4 1 K= 4 KK= 3

THE APPLICABLE ARRAY ARCINT FOLLOWS:
 I= 1 70 532 68 27 K= 7 KK= 1
 I= 2 75 983 66 44 K= 8 KK= 2
 I= 3 95 11 797 74 45 K= 9 KK= 3
 I= 4 11 13 8 1 1 K= 13 KK= 4
 I= 5 11 13 8 1 1 K= 13 KK= 5
 I= 6 11 13 8 1 1 K= 13 KK= 6

FIND SLICE WIDTH AND NO OF SLICES
 FI= 00000 FO= 02768
 FI= 02768 FO= 02986
 FI= 02986 FO= 03003
 THE SAFETY FACTOR FOR POINT 2 IS 1.03003

TRIAL CIRCLE NO 3
 CIRCLE CTR COO DS: X= X= 83.711 = 08.711
 ENTRANCE PT. COORDS: X= X= 18.411 = 8.411
 TRIAL ARC RADIUS= 44.204

- XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY
 LINE NO X Y
 2 66 532 67 09
 6 72 756 65 14
 7 11 756 74 45
 3 18 111 8 1

1	0000	53	K	1	KK	2
2	0000	55	K	1	KK	4
3	0000	62	K	1	KK	5
4	0000	67	K	2	KK	6
5	40	65	K	3	KK	6
6	50	74	K	3	KK	7
7	66	74	K	4	KK	8
8	66	84	K	4	KK	9
9	72	84	K	4	KK	9
10	95	74	K	4	KK	0
11	113	84	K	4	KK	1
12	113	84	K	4	KK	2
13	113	84	K	4	KK	3
14	113	84	K	4	KK	3
15	113	84	K	4	KK	3
16	113	84	K	4	KK	3
17	113	84	K	4	KK	3

THE APPLICABLE ARRAY ARCINT FOLLOWS:

1	66	67	65	7	KK	1
2	72	74	74	9	KK	2
3	95	74	74	9	KK	3
4	113	84	84	11	KK	4
5	113	84	84	11	KK	5
6	113	84	84	11	KK	6

FIND SLICE WIDTH AND NO OF SLICES

FI= 000000 FO= 00414
 FI= 000414 FO= 00446

THE SAFETY FACTOR FOR POINT 3 IS 1.00446

TRIAL CIRCLE NO 4
 CIRCLE CTR COORDS: X= X= 86.711 Y= 108.711
 ENTRANCE PT. COORDS: X= X= 118.711 Y= 81.711
 TRIAL ARC RADIUS= 41.869

- XXX LINE 1 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 4 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 5 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 10 NOT INTERSECTED BY TRIAL CIRCL

ARC INTERSECT WITH LINE ARRAY

LINE NO	X	Y
2	71.969	68.70
6	77.703	67.0
7	110.981	74.43
3	118.011	81.71

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	0000	62	K	1	KK	1
2	0000	53	K	1	KK	2
3	0000	58	K	1	KK	3
4	40	55	K	1	KK	4
5	50	62	K	1	KK	5
6	65	67	K	2	KK	6
7	71	68	K	3	KK	6
8	77	67	K	3	KK	7
9	95	74	K	3	KK	7
10	110	74	K	4	KK	7
11	113	84	K	4	KK	8
12	113	84	K	4	KK	9

I=	14	73	54	K=	4	KK=	1
I=	15	240	81	K=	4	KK=	2
I=	16	242	77	K=	4	KK=	3
I=	17	244	66	K=	4	KK=	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	71	969	68	703	K=	7	KK=	1
I=	2	77	703	67	7095	K=	8	KK=	2
I=	3	95	11	74	11	K=	9	KK=	3
I=	4	10	98	74	435	K=	0	KK=	4
I=	5	13	11	81	11	K=	1	KK=	5
I=	6	18	11	81	11	K=	3	KK=	6

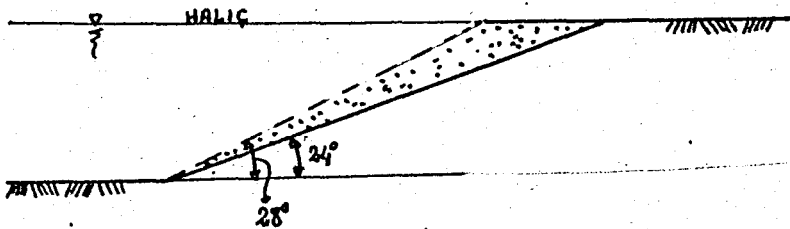
FIND SLICE WIDTH AND NO. OF SLICES

FI=	00000	FO=	000946
FI=	00946	FO=	01019

THE SAFETY FACTOR FOR POINT 415 1.01019
 END PROGRAM EXECUTION

b) Rearranging of slopes:

Slope angle should be decreased in order to compensate for extra loading caused by dredging.



This has been analyzed with the computer program. The slope angle is decreased from 28 to 24. It is observed that the factor of safety, in cross-section (3-3)_B, changed from 0.95 to 1.006. This may be also economical.

c) Protection of slopes:

The application of this method is impossible for Haliç shores because bottom sludge and clay layer are very soft and weak.

OF LINES = 9 NO OF LINE INTERSECT = 12
 OF SOILS = 3 NO OF EXTERNAL SOIL LINES = 3
 OF X INCREMENTS = 2 NO OF Y INCREMENTS = 2
 INITIAL SLICE WIDTH = 200

LINE NO	END NO	COORD INT	MATRIX X1	Y1	X2	Y2	SLOPE	LINE INTER
1	2	00	74	54	74	69	2023	47
2	3	00	63	36	63	07	2699	70
3	4	00	86	97	86	00	6666	69
4	5	00	194	60	33	00	0000	15
5	6	00	86	36	86	00	5807	58
6	7	00	88	94	24	00	4074	26
7	8	00	88	73	24	00	2259	93
8	9	00	88	127	24	00	1408	58
9	10	00	88	73	24	00	3571	22

INTERSECT ARRAY

X	Y
00	54
00	36
00	97
74	60
86	27
63	50
88	73
194	94
233	107
337	109
224	90

SOIL DATA ARRAY

LINE #	LEFT INT	RT INT	SAT	UNIT	WT	PHI	COHESI	ON
1	4	7	00	8	7	20	19	66
2	7	7	00	8	7	20	19	66
3	6	7	00	8	7	20	19	66
4	9	7	00	8	7	20	19	66
5	6	7	00	8	7	20	19	66
6	9	7	00	8	7	20	19	66
7	5	7	00	8	7	20	19	66
8	2	7	00	8	7	20	19	66
9	5	7	00	8	7	20	19	66
10	8	7	00	8	7	20	19	66
11	5	7	00	8	7	20	19	66
12	2	7	00	8	7	20	19	66
13	5	7	00	8	7	20	19	66
14	8	7	00	8	7	20	19	66
15	5	7	00	8	7	20	19	66
16	2	7	00	8	7	20	19	66
17	5	7	00	8	7	20	19	66
18	8	7	00	8	7	20	19	66
19	5	7	00	8	7	20	19	66
20	2	7	00	8	7	20	19	66

TRIAL CIRCLE NO 1
 CENTER COORDS: X = 82.11 Y = 161.11
 PERIPHERY COORDS: X = 192.11 Y = 107.11
 TRIAL ARC RADIUS = 122.540

- LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- LINE 6 NOT INTERSECTED BY TRIAL CIRCL
- LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- LINE 9 NOT INTERSECTED BY TRIAL CIRCL

ARC LINE NO	INTERSECT WITH LINE ARRAY	X	Y
16	698	57	49
46	906	43	74
181	026	88	78
192	111	107	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

LINE NO	X	Y	K
1	0	0	1
2	0	0	1
3	0	0	1
4	0	0	1
5	16	698	2
6	46	906	3
7	74	111	3
8	84	111	3
9	86	111	3
10	63	07	3
11	181	026	4
12	192	111	4
13	88	78	4
14	94	111	4
15	233	37	4
16	237	44	4
17	244	44	4
18	54	111	4
19	36	111	4
20	40	111	4
21	43	111	4
22	49	111	4
23	73	111	4
24	77	111	4
25	79	111	4
26	88	111	4
27	90	111	4

THE APPLICABLE ARRAY ARCINT FOLLOWS:

LINE NO	X	Y	K
2	0	0	4
3	0	0	5
4	0	0	6
5	16	698	8
6	46	906	9
7	74	111	10
8	84	111	11
9	86	111	11
10	63	07	11
11	181	026	11
12	192	111	11
13	88	78	11
14	94	111	11
15	233	37	11
16	237	44	11
17	244	44	11
18	54	111	11
19	36	111	11
20	40	111	11
21	43	111	11
22	49	111	11
23	73	111	11
24	77	111	11
25	79	111	11
26	88	111	11
27	90	111	11

FIND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50
 FI= 1.00000 FO= 1.00037

THE SAFETY FACTOR FOR POINT IS 1.00037

TRIAL CIRCLE NO 2
 CIRCLE CTR COORDS: X= 85.711 Y= 61.711
 ENTRANCE PT. COORDS: X= 92.711 Y= 67.711
 TRIAL ARC RADIUS= 19.854

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL

XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC LINE NO	INTERSECT WITH LINE ARRAY	X	Y
22	802	58	73
55	114	45	07
180	524	88	58
192	111	107	1

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

5	02	58	726	K=	2	KK=	3
6	02	45	726	K=	3	KK=	4
7	02	69	726	K=	3	KK=	5
8	02	27	726	K=	3	KK=	6
9	02	50	726	K=	3	KK=	7
10	02	07	726	K=	4	KK=	8
11	02	88	726	K=	4	KK=	9
12	02	73	726	K=	4	KK=	0
13	02	07	726	K=	4	KK=	1
14	02	94	726	K=	4	KK=	2
15	02	00	726	K=	4	KK=	3
16	02	90	726	K=	4	KK=	4

THE APPLICABLE ARRAY ARC INT FOLLOWS:

2	22	80	2	58	726	K=	4	KK=	1
3	55	11	4	45	726	K=	5	KK=	2
4	74	11	4	69	726	K=	6	KK=	3
5	86	11	1	50	726	K=	8	KK=	4
6	16	33	7	07	726	K=	9	KK=	5
7	18	00	5	88	726	K=	0	KK=	6
8	19	2	1	07	726	K=	1	KK=	7

FIND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50

FI= 00000 FO= 00228
 FI= 00228 FO= 00253

THE SAFETY FACTOR FOR POINT 2IS 1.00253

TRIAL CIRCLE NO 3
 CIRCLE CTR COORDS: X= X= 82.711 Y= 64.711
 ENTRANCE PT. COORDS: X= X= 192.711 Y= 107.711
 TRIAL ARC RADIUS= 123.891

- XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
- XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

1	18	427	57	84
2	50	498	44	32
3	180	215	88	45
4	192	111	07	11

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

1	0000	54	1	KK=	1		
2	0000	36	1	KK=	2		
3	0000	70	1	KK=	3		
4	18	427	57	84	KK=	4	
5	50	498	44	32	KK=	5	
6	74	11	4	69	726	KK=	6
7	86	11	1	50	726	KK=	7
8	16	33	7	07	726	KK=	8
9	18	00	5	88	726	KK=	9
10	19	2	1	07	726	KK=	0
11	18	8	1	73	726	KK=	1

I=	15	237	107	K=	4	KK=	0
I=	16	244	90	K=	4	KK=	12

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	18	57	K=	4	KK=	1
I=	2	50	44	K=	5	KK=	2
I=	3	74	69	K=	6	KK=	3
I=	4	86	50	K=	8	KK=	4
I=	5	63	77	K=	9	KK=	5
I=	6	80	88	K=	0	KK=	6
I=	7	92	07	K=	2	KK=	7

FIND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2750

FI=	100000	FO=	99844
FI=	99844	FO=	99826

THE SAFETY FACTOR FOR POINT 3 IS 99826.

TRIAL CIRCLE NO. 4
 ENTRANCE PT. COORDS: X= 85.71 Y= 164.71
 TRIAL ARC RADIUS= 121.235

XXX LINE 2 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 6 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 7 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 8 NOT INTERSECTED BY TRIAL CIRCL
 XXX LINE 9 NOT INTERSECTED BY TRIAL CIRCL

***LINE 2 IS NOT INTERSECTED BUT IS IN ARC

ARC INTERSECT WITH LINE ARRAY

LINE NO	24	557	59	08
	59	046	45	71
	74	657	88	22
	92	07	07	01

THE ARRAY WITH ALL INTERSECTIONS FOLLOWS:

I=	1	000	54	K=	1	KK=	1
I=	2	000	36	K=	1	KK=	2
I=	3	000	10	K=	1	KK=	3
I=	4	000	10	K=	2	KK=	3
I=	5	557	59	K=	3	KK=	3
I=	6	046	45	K=	3	KK=	4
I=	7	657	69	K=	3	KK=	5
I=	8	07	27	K=	3	KK=	6
I=	9	07	50	K=	3	KK=	7
I=	10	657	07	K=	4	KK=	7
I=	11	07	88	K=	4	KK=	8
I=	12	07	73	K=	4	KK=	8
I=	13	07	07	K=	4	KK=	9
I=	14	07	94	K=	4	KK=	9
I=	15	07	07	K=	4	KK=	0
I=	16	07	90	K=	4	KK=	12

THE APPLICABLE ARRAY ARCINT FOLLOWS:

I=	1	24	557	K=	4	KK=	1
I=	2	59	046	K=	5	KK=	2
I=	3	74	657	K=	6	KK=	3

I= 6
I= 7

179.657
192.111

88.222
107.111

K= 10 KK= 6
K= 12 KK= 7

FIND SLICE WIDTH AND NO OF SLICES

*****MAXIMUM SLICE WIDTH HAS BEEN INCREMENTED TO 2.50

FI= 1.00000 FO= 1.000348
FI= 1.000348 FO= 1.000387

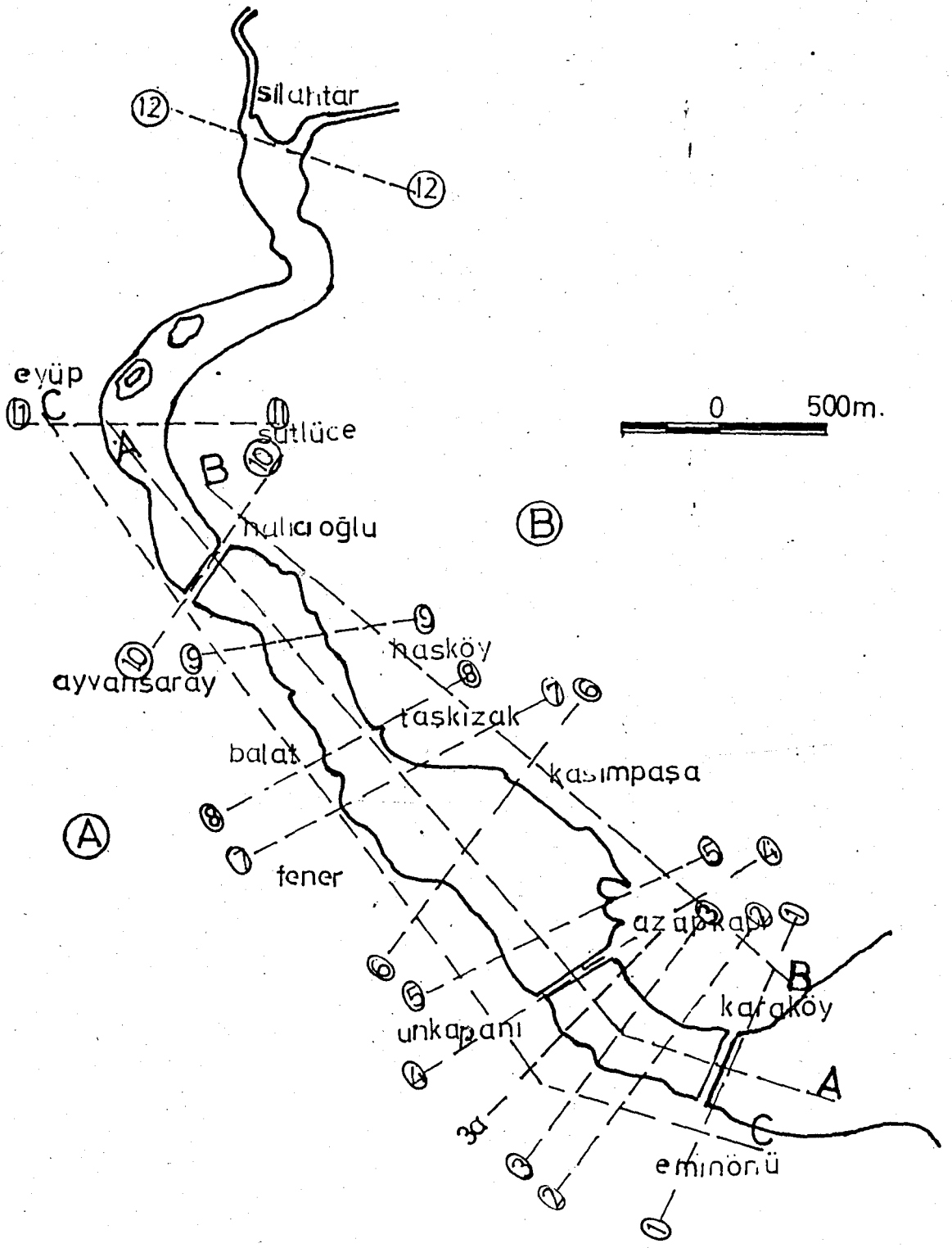
DBRKPT PRINTS

THE SAFETY FACTOR FOR POINT 4 IS 1.00387

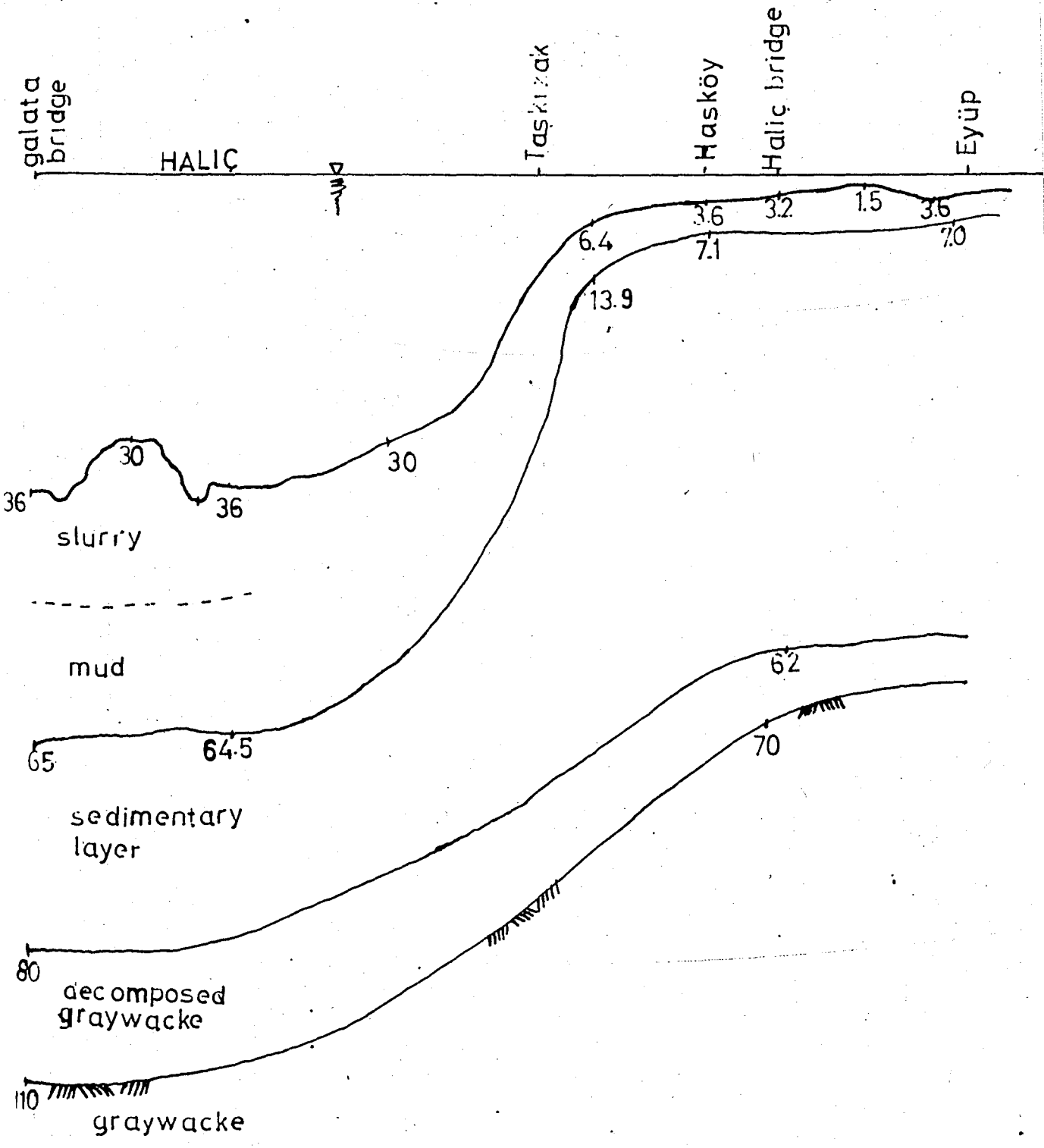
APPENDIX

CROSS - SECTIONS

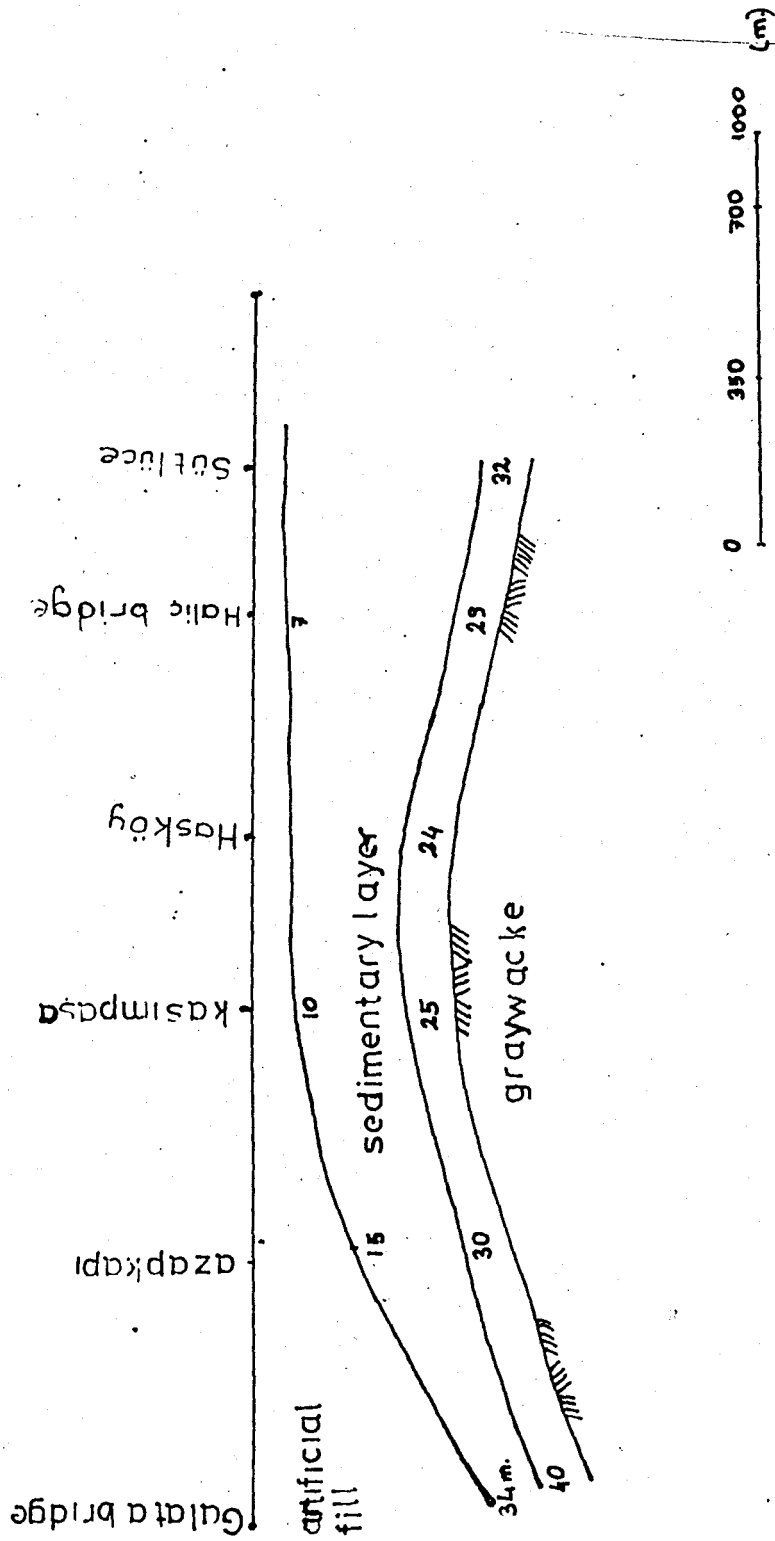
ALONG HALIC

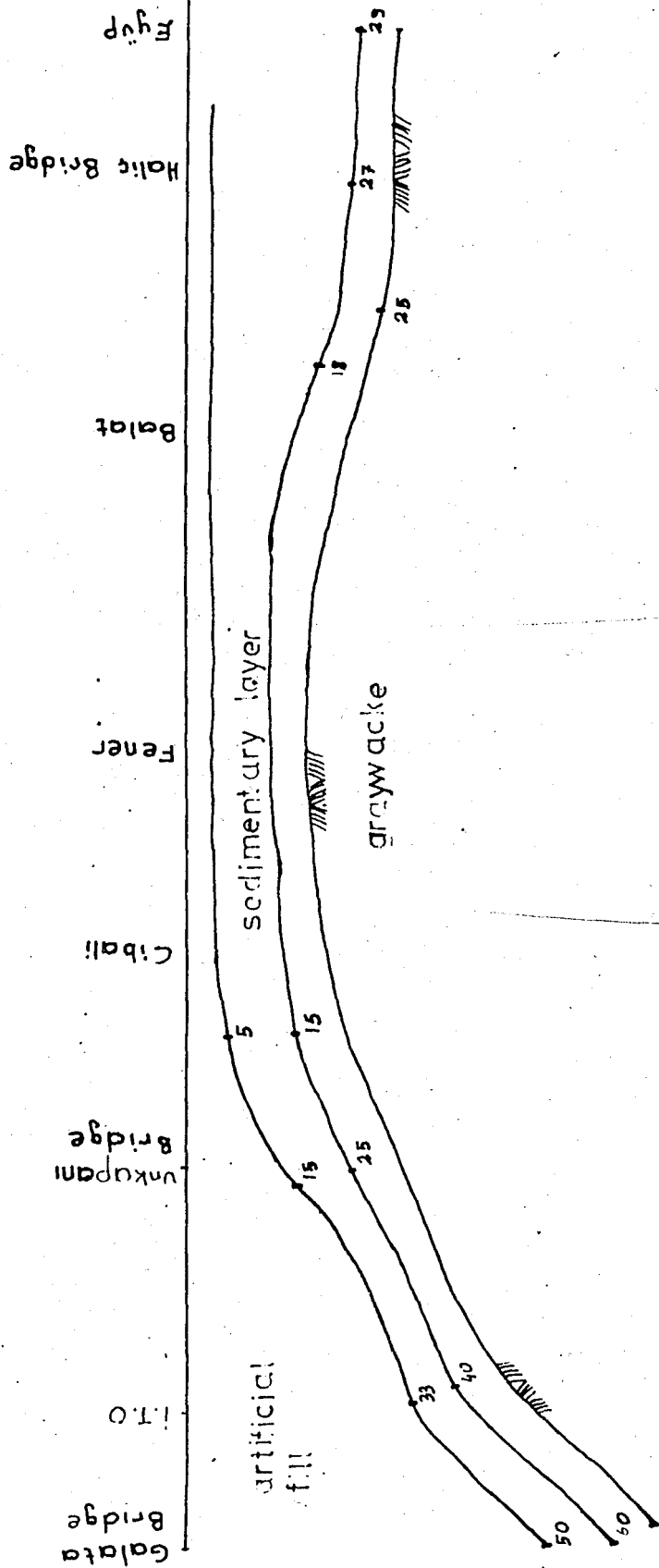


(A) - (A)

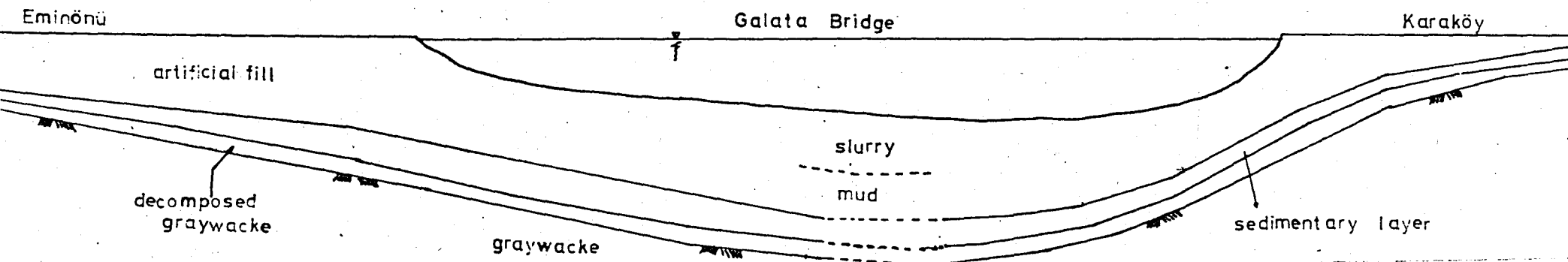


(B) - (B)





(I-I)



Eminönü

Galata Bridge

Karaköy

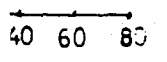
artificial fill

decomposed
graywacke

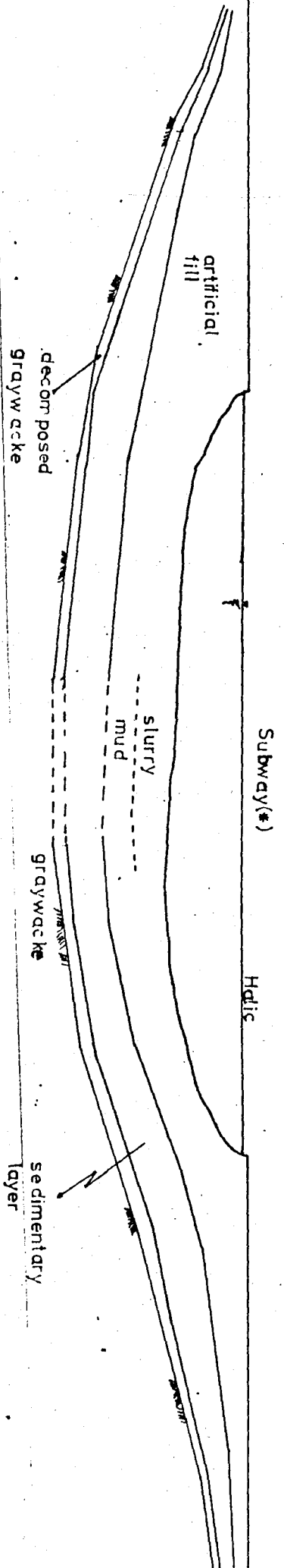
graywacke

slurry
mud

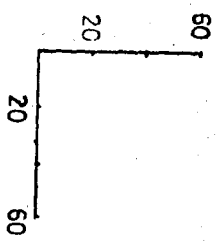
sedimentary layer



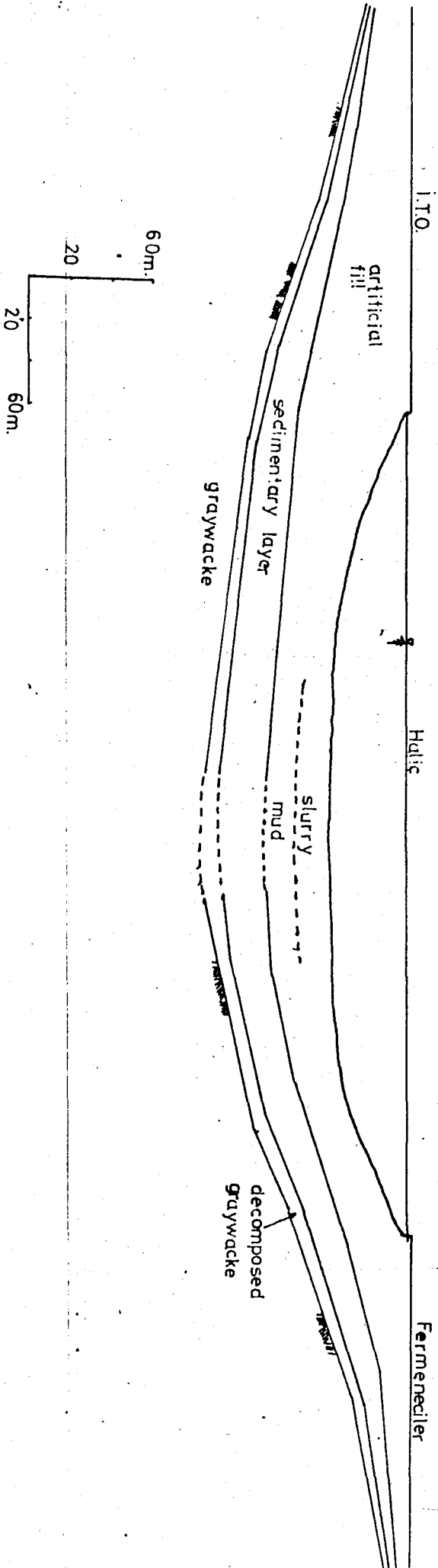
2-2

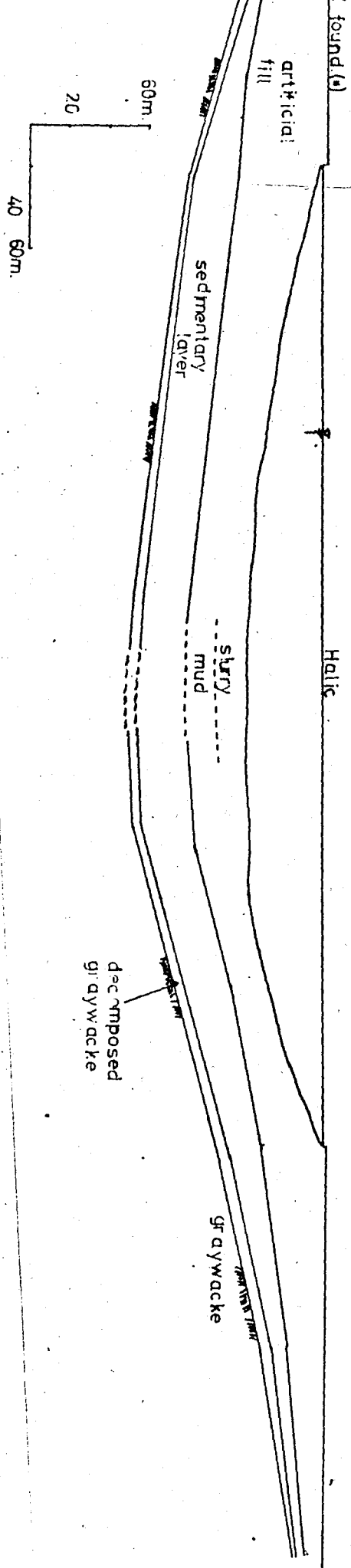


(*) Sayar, 1961



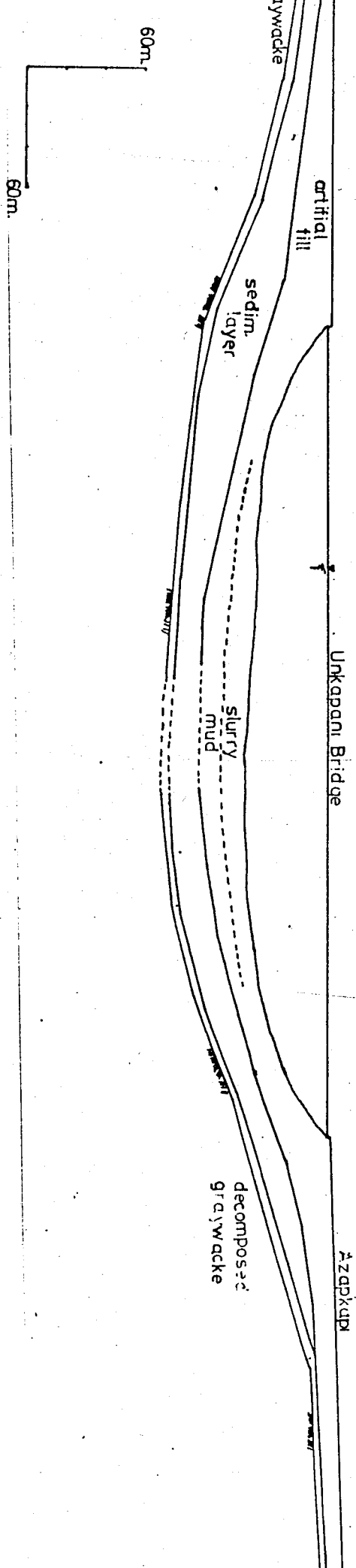
3-3





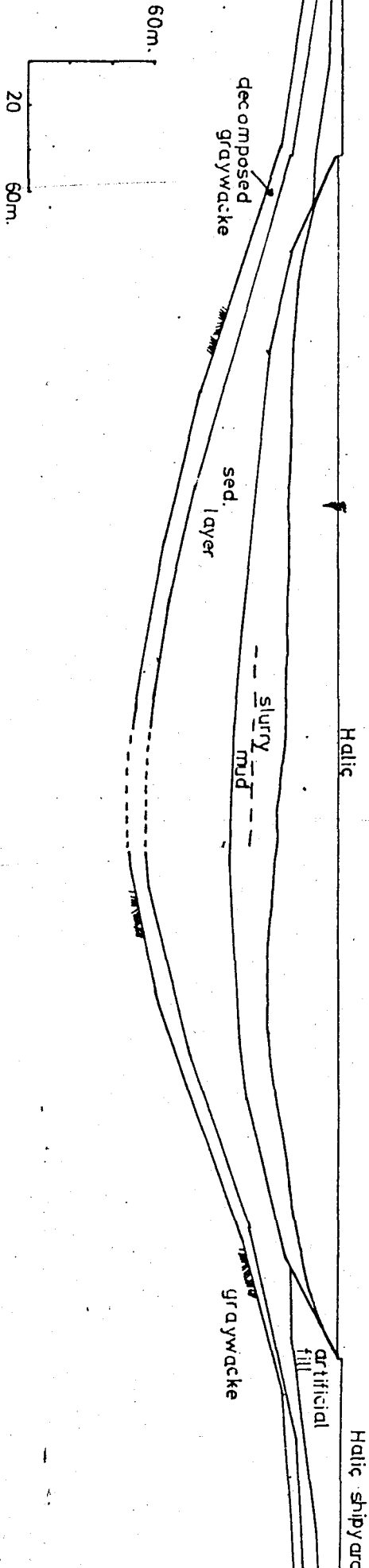
3a - 3a

(v) Peynircioglu (1961)



4-4

5-5



sed. layer

graywacke

graywacke

slurry mud

graywacke

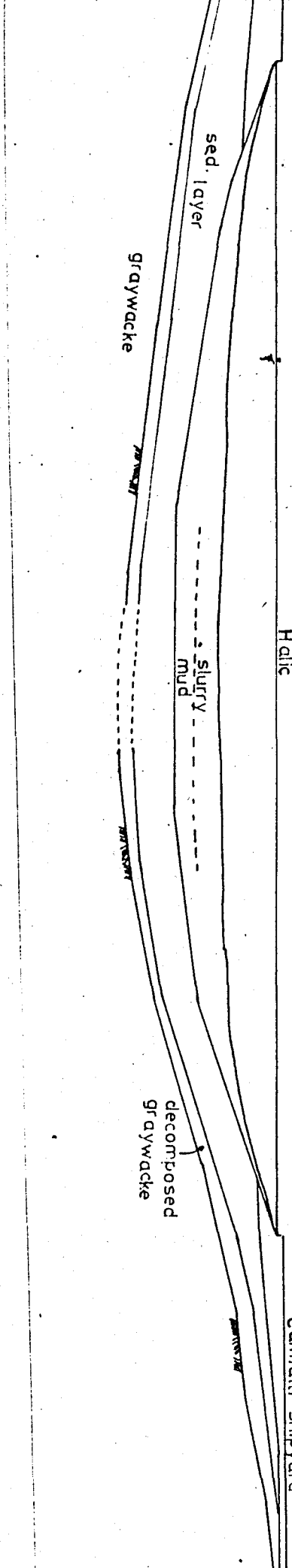
decomposed graywacke

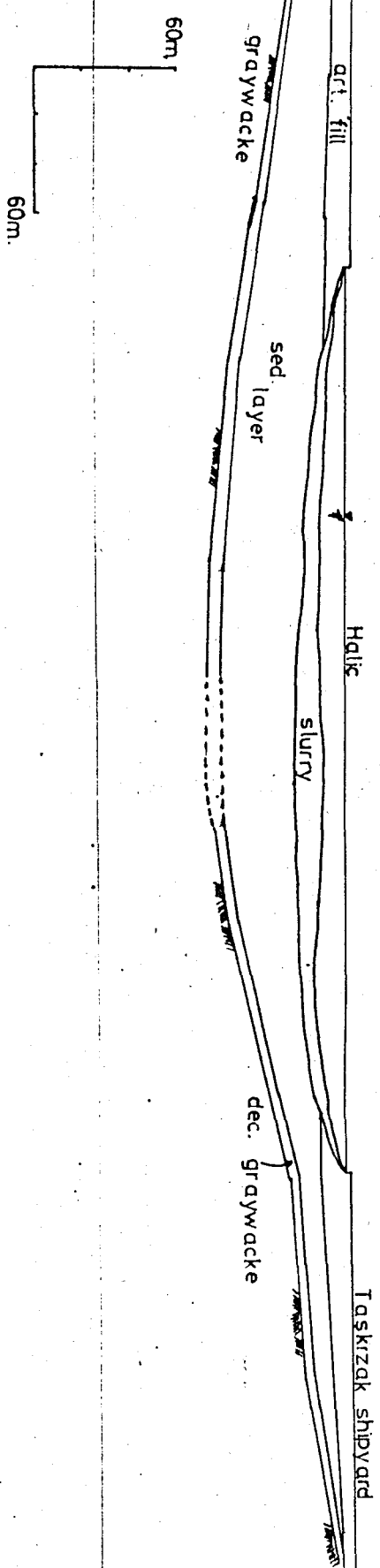
graywacke

Halib

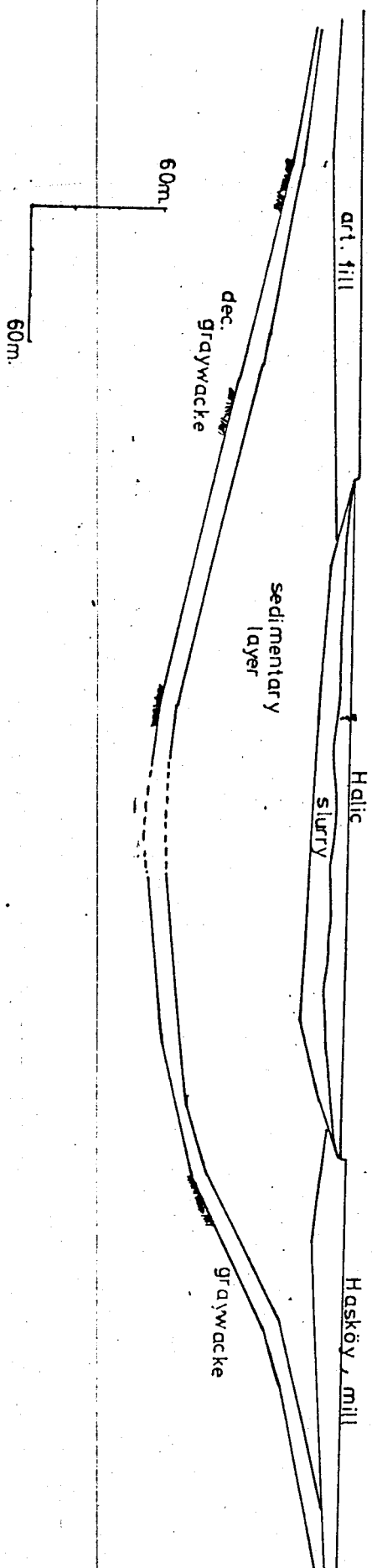
Camialti shipyard

7-7

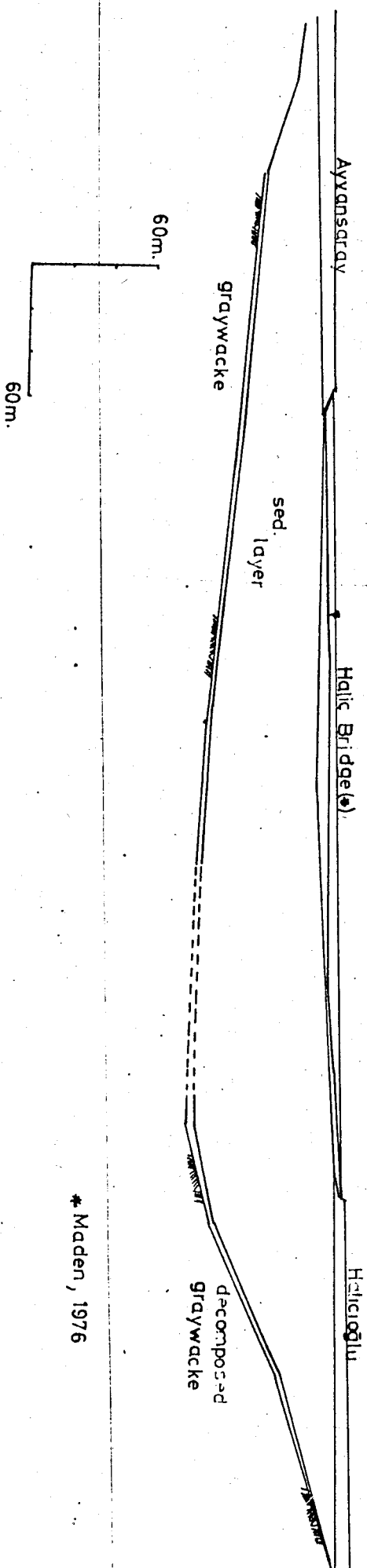




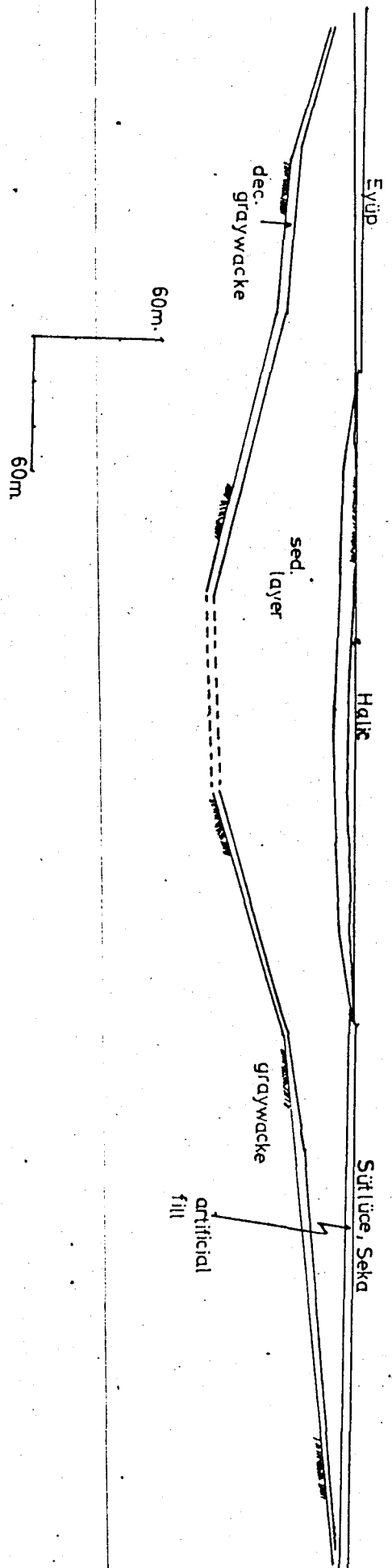
8-8



9-9



* Maden, 1976



Eyüp

dec.
graywacke

sed.
layer

Halk

Sutlüce, Seka

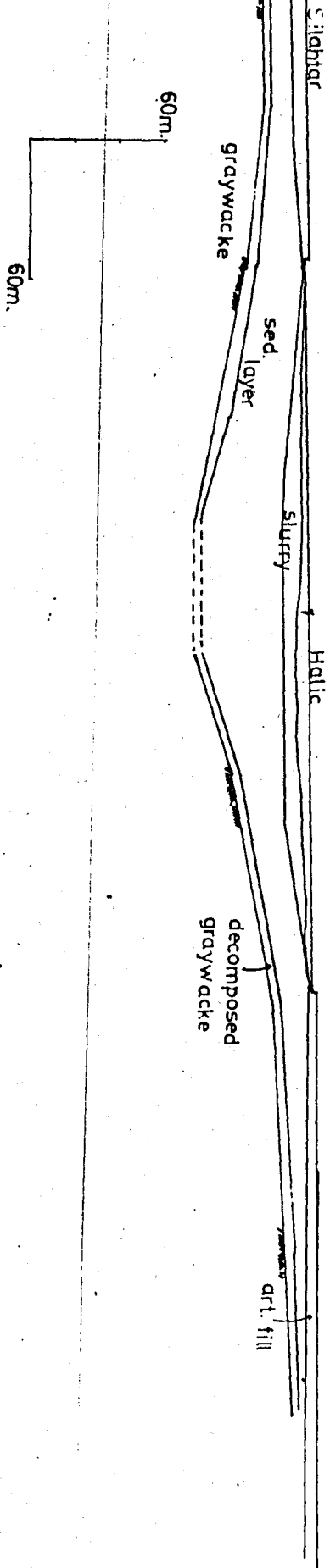
graywacke

artificial
fill

60m.

60m.

11-11



12-12

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