





**ISTANBUL TECHNICAL UNIVERSITY ★ GRADUATE SCHOOL OF SCIENCE**  
**ENGINEERING AND TECHNOLOGY**

**STATISTICAL CRYOGENIC MODELING METHODOLOGY OF MOSFET  
DC CHARACTERISTICS IN BSIM3**

**M.Sc. THESIS**

**Aykut KABAOĞLU**

**Department of Electronics and Communication Engineering**

**Electronics Engineering Programme**

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**Aykut KABAOĞLU**  
**(504161205)**

**Department of Electronics and Communication Engineering**

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**Thesis Advisor: Asst. Prof. Dr. Mustafa Berke YELTEN**

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**İSTANBUL TEKNİK ÜNİVERSİTESİ ★ FEN BİLİMLERİ ENSTİTÜSÜ**

**MOSFET DC KARAKTERİSTİĞİNİN KRIYOJENİK KOŞULLARDA BSIM3 İLE  
İSTATİSTİKSEL OLARAK MODELLENMESİ**

**YÜKSEK LİSANS TEZİ**

**Aykut KABAOĞLU  
(504161205)**

**Elektronik ve Haberleşme Mühendisliği Anabilim Dalı**

**Elektronik Mühendisliği Programı**

**Tez Danışmanı: Asst. Prof. Dr. Mustafa Berke YELTEN**

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Ayktut KABAOĞLU, a M.Sc. student of ITU Graduate School of Science Engineering and Technology 504161205 successfully defended the thesis entitled “STATISTICAL CRYOGENIC MODELING METHODOLOGY OF MOSFET DC CHARACTERISTICS IN BSIM3”, which he/she prepared after fulfilling the requirements specified in the associated legislations, before the jury whose signatures are below.

**Thesis Advisor :**     **Asst. Prof. Dr. Mustafa Berke YELTEN** .....  
Istanbul Technical University

**Jury Members :**     **Asst. Prof. Dr. Onur FERHANOĞLU** .....  
Istanbul Technical University

**Prof. Dr. Günhan DÜNDAR** .....  
Boğaziçi University

.....

**Date of Submission :**   **3 May 2019**

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## TABLE OF CONTENTS

	<u>Page</u>
<b>FOREWORD</b> .....	vii
<b>TABLE OF CONTENTS</b> .....	ix
<b>ABBREVIATIONS</b> .....	xi
<b>SYMBOLS</b> .....	xiii
<b>LIST OF TABLES</b> .....	xv
<b>LIST OF FIGURES</b> .....	xvii
<b>SUMMARY</b> .....	xix
<b>ÖZET</b> .....	xxi
<b>1. INTRODUCTION</b> .....	<b>1</b>
1.1 Literature Review .....	2
1.2 The Temperature Dependency Parameters .....	3
1.2.1 Mobility ( $\mu$ ).....	3
1.2.2 Threshold voltage ( $V_{th}$ ).....	4
1.2.3 Saturation velocity ( $v_{sat}$ ).....	5
1.2.4 Drain-source parasitic resistance ( $R_{ds}$ ).....	5
<b>2. PROPOSED MODEL</b> .....	<b>7</b>
2.1 Temperature Model Parameter Calibration Methodology .....	7
2.1.1 Processing the target data .....	8
2.1.2 Fixing BSIM equations.....	9
2.1.3 Parameter extraction algorithm .....	10
2.1.4 Computation cost of the methodology .....	11
<b>3. EXPERIMENTAL RESULTS</b> .....	<b>13</b>
3.1 Measurement Setup .....	14
3.2 Comparison of the Measurements between Cryogenic Temperature and Room Temperature .....	15
3.2.1 Measurements at various intermediate temperatures.....	20
3.2.2 Extracted model parameters .....	22
3.2.2.1 Model usage in simulation.....	22
3.2.2.2 Comparison of default and extracted model .....	25
3.2.2.3 Circuit measurements .....	31
<b>4. CONCLUSION</b> .....	<b>35</b>
<b>REFERENCES</b> .....	<b>37</b>
<b>APPENDICES</b> .....	<b>41</b>
APPENDIX A.1 - Source Code of Main Function.....	43
<b>CURRICULUM VITAE</b> .....	<b>53</b>



## ABBREVIATIONS

<b>CAD</b>	: Computer Aided Design
<b>MOSFET</b>	: Metal Oxide Semiconductor Field Effect Transistor
<b>UMC</b>	: United Microelectronics Corporation
<b>BSIM</b>	: Berkeley Short-channel Insulated-Gate-Field-Effect-Transistor Model
<b>CAD</b>	: Computer Aided Design
<b>EKV</b>	: Transistor Model Developed by C. C. Enz, F. Krummenacher and E. A. Vittoz
<b>PSP</b>	: Penn State Philips Transistor Model
<b>VDSAT</b>	: Drain Saturation Voltage
<b>VSAT</b>	: Velocity Saturation
<b>NMOS</b>	: n-type MOSFET
<b>PMOS</b>	: p-type MOSFET
<b>VDS</b>	: Drain-Source Voltage
<b>VGS</b>	: Gate-Source Voltage
<b>VTH</b>	: Threshold Voltage
<b>RF</b>	: Radio Frequency
<b>LN2</b>	: Liquid Nitrogen
<b>GHZ</b>	: Gigahertz





## SYMBOLS

$^{\circ}C$	: Temperature in Celcius
$I$	: Current
$V$	: Voltage
$A$	: Ampere
$\sigma$	: Standard Deviation
$\rho$	: Fixing coefficient for current equations
$\mu$	: Micro
$V_{th0}$	: Threshold voltage at $V_{BS} = 0$ for Large length
$V_{fb}$	: Flat-band voltage
$K1$	: First order body effect coefficient
$K2$	: Second order body effect coefficient
$U_0$	: Mobility at Temp. = $27^{\circ}C$
$U_a$	: First-order mobility degradation coefficient
$U_b$	: Second-order mobility degradation coefficient
$U_c$	: Body-effect of mobility degradation coefficient
$UTE$	: Mobility temperature exponent
$KT_1$	: Temperature coefficient for threshold voltage
$KT_{1L}$	: Channel length dependence of temperature coefficient for threshold voltage
$KT_2$	: Body-bias coefficient of $V_{th}$ temperature effect
$U_{a1}$	: Temperature coefficient for $U_a$
$U_{b1}$	: Temperature coefficient for $U_b$
$U_{c1}$	: Temperature coefficient for $U_c$
$AT$	: Temperature coefficient for saturation velocity



## LIST OF TABLES

	<u>Page</u>
<b>Table 3.1</b> : Device names and sizes.....	13
<b>Table 3.2</b> : Threshold Voltage increase amounts.....	18
<b>Table 3.3</b> : The maximum current value comparison of transistors both at the room temperature and cryogenic temperature .....	20
<b>Table 3.4</b> : Error rates of $I_D - V_{DS}$ curves @ $ V_{GS}  = 1.8V$ with extracted model files at $-196^{\circ}C$ for transistors of every size and the model performance at different temperatures .....	28
<b>Table 3.5</b> : Error rates of $I_D - V_{DS}$ curves of different parameter sets for each transistor with lower gate biasing at $-196^{\circ}C$ .....	31
<b>Table 3.6</b> : Comparison of oscillation frequency for the ring oscillator at nominal and liquid nitrogen temperatures .....	33



## LIST OF FIGURES

	<u>Page</u>
<b>Figure 2.1</b> : The flowchart of the proposed methodology [1] .....	7
<b>Figure 2.2</b> : Demonstration of the extrapolation method for $V_{TH}$ extraction .....	9
<b>Figure 2.3</b> : Demonstration of the second derivative method for $V_{TH}$ extraction .	9
<b>Figure 2.4</b> : Demonstration of the extraction of $V_{DSAT}$ change between the room and cryogenic temperature .....	10
<b>Figure 2.5</b> : Parameter Extraction Algorithm.....	11
<b>Figure 3.1</b> : The measurement bench and probe station.....	14
<b>Figure 3.2</b> : The device under test.....	15
<b>Figure 3.3</b> : The die layout observed with a microscope .....	16
<b>Figure 3.4</b> : NMOS $I_D - V_{GS}$ Curve @ $V_{DS} = 0.05V$ demonstrating $V_{TH}$ increase as temperatures drop down .....	17
<b>Figure 3.5</b> : PMOS $I_D - V_{GS}$ Curve @ $V_{DS} = 0.05V$ demonstrating $V_{TH}$ increase as temperatures drop down .....	19
<b>Figure 3.6</b> : $I_D - V_{GS}$ Curve @ $V_{DS} = 0.05V$ demonstrating $V_{TH}$ increase as temperatures drop down .....	20
<b>Figure 3.7</b> : The mean result and variations of NMOS measurements at $24^{\circ}C$ and $-196^{\circ}C$ .....	21
<b>Figure 3.8</b> : The mean result and variations of PMOS measurements at $24^{\circ}C$ and $-196^{\circ}C$ .....	22
<b>Figure 3.9</b> : The mean result and variations of RF and Low $V_{TH}$ NMOS measurements at $24^{\circ}C$ and $-196^{\circ}C$ .....	23
<b>Figure 3.10</b> : $I_D - V_{DS}$ measurements of NMOS devices from $-40^{\circ}C$ to $-196^{\circ}C$ .....	23
<b>Figure 3.11</b> : $I_D - V_{DS}$ measurements of PMOS device from $-40^{\circ}C$ to $-196^{\circ}C$ .	24
<b>Figure 3.12</b> : Comparison of the default model and extracted models of NMOS with measurement results at $-196^{\circ}C$ .....	26
<b>Figure 3.13</b> : Comparison of the default model and extracted models of PMOS with measurement results at $-196^{\circ}C$ .....	27
<b>Figure 3.14</b> : Comparison of the default model and extracted models of PMOS with measurement results at $-196^{\circ}C$ .....	28
<b>Figure 3.15</b> : Comparison of the default model and extracted model of NMOS with measurement results at $-196^{\circ}C$ .....	29
<b>Figure 3.16</b> : Comparison of the default model and extracted model of PMOS with measurement results at $-196^{\circ}C$ .....	30
<b>Figure 3.17</b> : Comparison of the default model and extracted model of RF NMOS and Low $V_{TH}$ NMOS with measurement results at $-196^{\circ}C$ .	31
<b>Figure 3.18</b> : Measured spectrum of the ring oscillator at $-196^{\circ}C$ (blue) and $24^{\circ}C$ (red).....	32

**Figure 3.19:** Measured oscillation frequencies of the ring oscillator from  $-196^{\circ}\text{C}$  to  $24^{\circ}\text{C}$  and proposed model results at  $-196^{\circ}\text{C}$ ,  $-170^{\circ}\text{C}$  and  $-145^{\circ}\text{C}$  with  $\pm 3\sigma$  values ..... 33



## STATISTICAL CRYOGENIC MODELING METHODOLOGY OF MOSFET DC CHARACTERISTICS IN BSIM3

### SUMMARY

Electronic design automation tools (EDA) and electronic computer-aided design softwares (ECAD) use industrial standard models to converge the simulation results to realistic attitudes of devices. These models can satisfy meaningful simulation results only for a specific temperature range and they are generally extracted under room temperature circumstances. BSIM3 is one of the most commonly used model standard in the industry and supports only between  $-55^{\circ}\text{C}$  and  $125^{\circ}\text{C}$ . There is a need to model cryogenic conditions to be able to produce trustworthy designs for extreme environment electronics such as military and space applications. A methodology has developed to produce a new model file with only modifying temperature dependency parameters analytically; therefore, there is no need to use iterative model extraction methods also, more robust model files can be obtained with this methodology. In the proposed automation system, mobility, threshold voltage and velocity saturation changes are taken into account and BSIM3 equations are used to compute the temperature dependency parameters of these phenomenas.

The methodology has been developed in MATLAB to calibrate temperature dependency parameters of BSIM3. Rather than modifying BSIM3 equations, the algorithm only changes the values of relevant parameters through analytical operations. Resulting cryogenic models have been extensively verified through device measurements performed on a cryogenic probe station cooled by liquid nitrogen ( $-196^{\circ}\text{C}$ ). The model can estimate with an error of less than 5% the  $I_D - V_{GS}$  and  $I_D - V_{DS}$  curves of transistors having different channel lengths and widths. Statistical analysis of cryogenic measurements is used to introduce variation levels on top of regular cryogenic operations to identify the impact of process variations of cryogenic conditions. Models adjusted to various temperatures between  $-196^{\circ}\text{C}$  and  $-40^{\circ}\text{C}$  are have been accomplished for applications requiring a broader range of cryogenic operating temperature. Experimental data collected from a ring oscillator is used to visualize the model performance in estimating the cryogenic characteristics of a circuit. Distortions on the I-V curves of simulation results have been suppressed and average errors of various sizes NMOS and PMOS transistors for  $0.18\ \mu\text{m}$  technology has been reduced significantly by using this methodology.





# MOSFET DC KARAKTERİSTİĞİNİN KRİYOJENİK KOŞULLARDA BSIM3 İLE İSTATİSTİKSEL OLARAK MODELLENMESİ

## ÖZET

Elektronik devre tasarımları bilgisayar destekli benzetim programları aracılığıyla test edilirken endüstriyel model standartları kullanılır ve bu standartlar transistör seviyesinde hesaplamalar yaparak istenilen çıktıları gösterir. Simülasyon programlarında kullanılan model standartları elle çözülemeyecek kadar karmaşık seviyede akım-gerilim denklemlerinden oluşur ve bu denklemlerin içerisinde sıcaklığa bağımlı birçok parametre yer alır. Kullanılan transistör teknolojisine göre üreticiler model parametrelerini tasarımcılara verirler ve bu parametreler yalnızca belli bir sıcaklık aralığında anlamlı sonuçlar üretirler. Bu aralık dışında gerçekleştirilen benzetimler; sıcaklık aralığından uzaklaştıkça gerçeğe daha uzak sonuçlar vermektedirler.

Sağlanan model parametreleri oda sıcaklığı referans alınarak oluşturulurlar. Endüstride en çok kullanılan modellerden bir tanesi BSIM3 standartlarıdır. BSIM3,  $-55^{\circ}C$  ile  $125^{\circ}C$  derece sıcaklık aralığında düzgün sonuç verebileceğini garanti eder ve yapılan benzetimlerde oda sıcaklığından uzaklaştıkça hata miktarı bu aralıkta kalınsa bile artmaktadır. Çünkü sıcaklığa bağlı parametreler, benzetim sıcaklığının oda sıcaklığından farkı ile çarpan durumundadırlar ve oda sıcaklığından uzaklaştıkça parametrenin sonuca etkisi artmaktadır. Düşük sıcaklıklarda çalışılması gereken ortamlarda bu etki dikkate alınmalıdır, standart modeller kullanıldığında devre performansı tamamen değişmektedir. Oda sıcaklığından çok daha düşük sıcaklıklarda çalışılan alanların başında uzay elektroniği, kuantum elektroniği ve savunma sanayii gelmektedir. Çalışmada hedef olarak uzay koşulları seçilmiştir. Ay yüzeyi veya Uluslararası Uzay İstasyonu dikkate alındığında  $-150^{\circ}C$  derece sıcaklıklar görülmekte, uzay boşluğunda ise bu değer  $-270^{\circ}C$  derecelere ulaşabilmektedir. Üreticilerin yayınladığı standart modeller bu sıcaklıklar için kullanılamazlar aksi halde devre performansı beklenenden çok farklı olur veya devre tamamıyla çalışmaz hale gelebilir. Üretim sonrası bu tip sorunlarla karşılaşmamak için benzetim sonuçlarının düşük sıcaklıklar için de gerçek performans değerlerine yakınsanması gerekmektedir.

Yaklaşık olarak  $-150^{\circ}C$  derecenin altında sıcaklığa sahip ortamlar kriyojenik olarak adlandırılır. Kriyojenik koşullar gibi uç noktalarda çalışacak devreler için yeni transistör modelleri oluşturulması gerekmektedir aksi durumda benzetim sonuçları üretilecek devre ile çok farklı olacaktır. Bu çalışmada kriyojenik ortamlarda transistörlerin DC karakteristiğindeki değişimler incelenmiş ve endüstriyel seviyede kullanılan benzetim programlarının anlamlı sonuç üretebilmesi için BSIM3 standardı bozulmadan MOSFET modellerinin; sıcaklık katsayılarının otomatik olarak değiştirilebileceği bir yöntem bilim önerilmiş ve gerçekleştirilmiştir. Model oluşturmak için üreticilerin de kullandığı çeşitli programlar mevcuttur ancak bu programlar iteratif yöntemlerle ölçüm sonuçlarını, model sonuçlarına yakınsayarak model parametreleri üzerinde rastlantısal değişiklikler gerçekleştirerek en uygun değerleri

elde etmeye çalışırlar. Önerilen yöntemde ise geliştirilen algoritma iteratif yöntemleri değil, BSIM denklemlerini ele alarak ölçüm sonuçlarında gözlemlenen değişimlerin fiziksel etkilerini ayrı ayrı inceler ve gerekli denklemleri bağımsız olarak ele alır. Fiziksel etkiyi modelleyen parametreyi, denklemlerin ölçüm sonuçlarına eşitlenerek çözdürülmesiyle elde eder. Bu sayede yeni parametre setinin fiziksel olarak anlamlı şekilde oluşturulmasıyla daha geniş sıcaklık aralığında da sonuçların benzer kalması ve hata oranlarının doğrusal olarak değişmesi beklenmektedir.

Sıcaklık düştükçe transistör karakteristiğinde en dikkat çekici iki fiziksel etki; mobilite ve eşik gerilimindeki değişimlerdir. Mobilite, yük taşıyıcılarının elektrik alan içerisindeki hareket kabiliyetlerini temsil eder ve sıcaklık düştükçe taşıyıcıların saçılma miktarlarında düşüş yaşandığı için mobilitede artış yaşanır. Mobilitedeki artış aynı gerilim altında bir MOSFET'in üzerinden geçen akım miktarının artması demektir ve akım değerleri transistör boyutuna bağlı olarak oda sıcaklığı referans alındığında 3 katın üzerine çıkabilmektedir. Kanal boyu daraldıkça akım artış miktarı uzun kanallara göre daha azdır. Yine sıcaklık düşüşü ile birlikte MOSFET içerisinde yüzey gerilimindeki artıştan kaynaklı olarak fakirleşmiş bölgenin genişlediği gözlemlenir bu sebeple MOSFET'in aktif hale geçtiği bir başka deyişle eşik gerilimine ulaştığı anda kanalda yer alması gereken taşıyıcı yoğunluğuna erişmek için daha çok enerjiye ihtiyaç duyulur; yani eşik gerilimi sıcaklığın düşmesiyle birlikte artar.

Çalışma içerisinde önerilen yöntem ile fiziksel etkileri temsil eden eşitlikler içerisindeki sıcaklığa bağımlı parametreler MATLAB üzerinde gerçekleştirilen algoritma aracılığı ile sırayla hesaplanır. Algoritma Cadence Analog Design Environment benzetim programı ile paralel olarak çalışır. BSIM3 standardının, MOSFET'lerin DC karakteristiğini simgeleyen yayınlanmış tüm eşitlikleri algoritma içerisine eklenmiştir. Ancak yayınlanan BSIM3 eşitlikleri tüm denklemleri içermez ve benzetim programları yayınlanmış denklemler dışında hesaplamaları da sisteme dahil ederler. Simülatörlerin kullandığı eşitlikler ile algoritmaya dahil edilmiş BSIM eşitliklerini örtüştürmek için MATLAB'de hesaplanan akım değeri ile simülatörden elde edilen akım değeri arasındaki fark bir katsayı yardımı ile giderilir ve bu hesaplanan katsayı algoritma içerisinde daha sonra tekrar kullanılacak olan BSIM3 eşitlikleri içerisine dahil edilir. Hesaplamanın gerçekleştirilmesi için kullanılacak olan teknolojideki bir MOSFET'in istenen sıcaklıkta ölçümü alınmalı ve bu ölçüm sonucu algoritmaya dahil edilmelidir. Sistem önce soğuktaki ölçüm sonuçlarını alıp BSIM eşitliklerini kullanarak ölçümü yapılan sıcaklıkta hesaplama yapar ve hesaplanan ile ölçüm arasındaki farkı sıcaklık ile çarpan olarak gelen parametreleri değiştirerek giderir. Parametrelerin değiştirilmesi önce eşik geriliminin hesaplanması ile başlar. Yeni eşik gerimi oluşturulduktan sonra tekrar benzetim yapılır ve elde edilen sonuçlar sisteme dahil edilerek sırasıyla mobilite ve doyma hızı parametreleri hesap edilir. Bu fiziksel etkileri gövde gerilimi sıfır olmayan durumlar için modelleyen ayrı parametreler vardır. Her bir eşitlik tekrardan farklı gövde gerilimi ölçümü dikkate alınarak hesap edilir. Tüm işlemlerin sonunda algoritma kriyojenik ölçüm sonuçlarını yakınsayacak yeni bir parametre dosyası oluşturur ve bu dosya BSIM3 standardını destekleyen herhangi bir benzetim programı üzerinde çalıştırılarak karmaşık devrelerin kriyojenik ortamlar için davranışı incelenebilir.

Çalışmada, algoritmanın doğrulanması için 0.18  $\mu\text{m}$  teknolojisinde farklı kanal boyu ve genişliklere sahip MOSFET'ler sıvı azot altında ölçülmüştür. Sıvı azot  $-196^{\circ}\text{C}$  derece kaynama sıcaklığına sahiptir ve uzay boşluğu hariç uzay koşullarına

benzer koşulları elde edebilmek için doğada bulunan en uygun ve en çok kullanılan malzemedir. İTÜ VLSI Duran Leblebici Laboratuvarı'nda bulunan kriyojenik ölçüm istasyonu vasıtasıyla ölçümler alınmıştır. Ölçümler paketsiz olarak üretilmiş olan kırmıklar üzerinde yapılmış ve farklı boyutta transistörler kullanılmıştır. Her boyuttaki transistör için 10'ar adet ölçüm yapılarak istatistiksel analizler elde edilmiştir. Daha sonra ölçüm sonuçları algoritma üzerinde çalıştırılarak yeni model dosyaları oluşturulmuş ve bu model dosyaları Cadence Analog Design Environment benzetim programı üzerinde çalıştırılarak, ham BSIM3 model sonuçları ile karşılaştırılmıştır. Değiştirilmemiş model parametreleri ile yapılan benzetim sonuçlarıyla ölçüm sonuçları arasında %100'e kadar varabilen hatalar gözlemlenirken, algoritma vasıtasıyla oluşturulan yeni modellerin hata oranları farklı boyutlara sahip tüm MOSFET'ler için %5'in altına indirilmiştir. Farklı boyutlara sahip MOSFET'ler üzerinde sıcaklık değişiminin etkisi incelenmiş ve sonuçlar aktarılmıştır. MOSFET seviyesinde gösterilen sonuçların ardından modeller ring osilatör devresi üzerinde de kullanılmış ve ölçüm sonuçları ile doğrulanmıştır. Böylelikle kriyojenik koşulların MOSFET'ler üzerindeki fiziksel etkileri incelenmiş, bu koşullar için model üreten algoritma oluşturulmuş, farklı boyutlardaki MOSFET'lerden,  $-196^{\circ}C$  derecede sonuçlar alınmış ve bu sonuçlar ile modeller üretilip benzetim sonuçları, ölçüm sonuçları ile kıyaslanmıştır. Hem ölçüm sonuçlarının hem de yeni oluşturulan modellerin istatistiksel analizleri paylaşılarak modelleme için tüm kriterler çalışma içerisinde incelenmiş ve sonuçlarla sergilenmiştir.



## 1. INTRODUCTION

Semiconductor device characteristics strongly depend on operation temperature thus the circuit performance alters in response to a temperature change. This performance variation should be carefully captured to model and design electronic circuits for extreme environments (such as space applications). Traditional models are not sufficient to account for these changes as they only focus on a limited temperature range considered as nominal. Most of the designs which have been realized using a CAD (computer aided design) tool at typical conditions may not work properly in low temperature environments. Hence, the equations have been derived to model the low temperature characteristics of MOSFETs. These equations are mostly semi-empirical and new parameters have been introduced to fit the measurement data by using polynomial equations without considering common model standards in the industry [2]. The situation gets even more complicated when these equations are translated into simulations because, a new module should be designed and implemented into the simulation tool. Therefore, there is a need to optimize the current model files used in simulations for low temperature (also called cryogenic) applications. Circuits in space or other extreme environment applications must be accurate and reliable. When developing models for such applications, a more mature technology is preferred as it contains the least number of manufacturing variations. In this work, UMC 180 nm technology along with its BSIM 3v3 model are used to improve the current transistor model at cryogenic conditions. In BSIM3, thermal changes are modeled by inserting binning parameters into equations of mobility, threshold voltage, drain-source parasitic resistance and saturation velocity [3]. Because temperature binning parameters are fit in a limited temperature range, they cannot describe the correct  $I$ - $V$  characteristics of a MOSFET in cryogenic conditions. Thus, an automated tool is developed to find revised binning parameters that will hold in cryogenic conditions without creating new equations and substantially changing the transistor model. After parameters have been

extracted by the algorithm, resulting model file can be employed within any simulation tool that supports BSIM3.

## 1.1 Literature Review

Cryogenic operation of MOSFETs has been a focus of research for the last few decades [4]. The main effect in all studies concentrated on an accurate modeling strategy to capture the DC characteristics of MOSFETs at cryogenic temperatures [2,5–15]. These modeling approaches have been implemented in different MOSFET model standards including BSIM, EKV and PSP.

The contribution of this thesis mainly lies in extending the capabilities of a cryogenic transistor model to include the impact of device variability as well as to investigate the device characteristics over a broader range of low temperatures. These aspects are especially crucial for circuits that will be used in an application when the operation temperature is not fixed and can vary significantly as in the case of space electronics. Besides, device variability can also alter the cryogenic circuit behavior and should properly be accounted for the transistor model so that designers become sufficiently informed in advance how the cryogenic characteristics are changed with process variations. The major points of our approach can be summarized as follows: 1) BSIM3 equations are kept in fact and an algorithm to calibrate the temperature dependency parameters has been developed thereby avoiding iterative solutions. 2) The impact of device sizes on the cryogenic operation has been investigated. It is shown that the channel length has a decisive role in the device characteristics changes observed and transistor model should be crafted such that this role is correctly reflected in them. 3) Different intermediate low temperatures between the liquid nitrogen temperature ( $-196^{\circ}C$ ) and the room temperature have been considered for model extraction. Various measurements have been performed to analyze device variability; additionally,  $\pm 3\sigma$  (of the measurement variation) values have been introduced to the model to represent the "corners" of the measurement data. Resulting models have been validated experimentally on a 7 stage ring oscillator.

The thesis organization can be given as follows: Section I describes the temperature dependent BSIM parameters and the coefficients that control the level of this temperature dependency. Section II explains in detail the modeling methodology.

Experimental results as well as the performance of the proposed modeling approach are discussed in Section III. Finally, conclusions are provided in Section IV.

## 1.2 The Temperature Dependency Parameters

### 1.2.1 Mobility ( $\mu$ )

The mobility of charge carriers describes the relationship of the velocity of charge carriers with the electric field acting on them [16]. The major scattering mechanisms that limit the carrier mobility are phonon scatterings and surface roughness [17] [18]. The decrease in lattice vibration due to temperature drop causes scattering mechanisms to reduce in magnitude; moreover, the mobility increases because of this reduction. At high temperatures, the carrier density is proportional to the intrinsic carrier concentration and when the temperature is close to the room temperature, the carrier density is assumed to be equal to the doping concentration. However, the carrier density decreases at lower temperatures and the freeze-out effect can take place [19]. While the temperature is decreasing, the mobility does not increase anymore and it starts to fall below a certain temperature depending on the technology due to lack of kinetic energy of charge carriers. The freeze-out impact becomes evident at much lower temperatures as the device technology scales down since the doping concentration increases with every technology node [20]. In addition to device sizes, lateral non-uniform doping techniques change the freeze-out effect onset temperature depending on the doping concentration.

Generally, the vertical electric field of MOSFETs degrades mobility. When the gate voltage increases, mobility degradation effect rises due to scattering becomes enhanced [21]. The mobility degradation is also affected by device scaling, as it increases when the channel length is scaled down [22].

In BSIM3, three distinct mobility models are used and each mobility model has four different parameters which are  $U_0, U_a, U_b$  and  $U_c$  as shown in (1.1-1.5) [23].

$$\mu_{eff} = U_0 / (1 + (U_a + U_c V_{bseff}) \frac{(V_{gsteff} + 2V_{th})}{T_{ox}} + U_b \frac{(V_{gsteff} + 2V_{th})^2}{T_{ox}}) \quad (1.1)$$

The zero field mobility  $U_0$  has a temperature dependency parameter  $UTE$  which changes  $U_0$  exponentially in response to a temperature change (1.2).  $U_a$  (first

order mobility degradation),  $U_b$  (parabolic mobility degradation) and  $U_c$  (body effect coefficient of mobility degradation) are binning parameters to model the effective gate voltage impact [24].  $U_{a1}, U_{b1}$  and  $U_{c1}$  are sub-parameters of  $U_a, U_b$  and  $U_c$  to indicate their temperature dependence, respectively (1.3-1.5).  $UTE$  has the dominant impact on the mobility change among all.

$$U_0(T) = \mu_0 \cdot (T/T_{nom})^{UTE} \quad (1.2)$$

$$U_a(T) = UA + UA1 \cdot (T/T_{nom} - 1) \quad (1.3)$$

$$U_b(T) = UB + UB1 \cdot (T/T_{nom} - 1) \quad (1.4)$$

$$U_c(T) = UC + UC1 \cdot (T/T_{nom} - 1) \quad (1.5)$$

### 1.2.2 Threshold voltage ( $V_{th}$ )

The intrinsic doping concentration has an exponential dependence of temperature and more gate voltage is needed to obtain the same channel charge concentration at lower temperatures [25]. Temperature changes affect the work function. Increase in surface potential leads to a larger depletion charge; additionally, the decrease in thermal energy causes slower ionization of channel dopants. [5]. In short, the increase in Fermi potential causes a rise in  $V_{th}$  [20]. In BSIM3,  $V_{th}$  is described in a tedious equation (1.6) and temperature dependency of the threshold voltage is included within the parameter  $V_{th0}$  [23].  $V_{th0}(T_{nom})$  specifies the threshold voltage of a device without short channel effects at zero body bias. Three further parameters,  $KT1, KT1L, KT2$ , characterize  $V_{th0}(T)$  at an arbitrary temperature  $T$  as shown in (1.7) [23].

$$\begin{aligned} V_{th} = & V_{th0}(T) + K_1 \sqrt{\phi_s - V_{bseff}} - K_2 V_{bseff} + K_1 \left( \sqrt{1 + \frac{N_{tx}}{L_{eff}}} \right. \\ & - 1) \sqrt{\phi_s} + (K_3 + K_{3b} V_{bseff}) \left( \frac{T_{ox}}{W_{eff} + W_0} \right) \phi_s \\ & - D_{vt0w} \left( e^{-\frac{D_{vt1w} W_{eff} L_{eff}}{2l_{tw}}} + 2e^{-\frac{D_{vt1w} W_{eff} L_{eff}}{l_{tw}}} \right) (V_{bi} - \phi_s) \\ & - D_{vt0} \left( e^{-\frac{D_{vt1} L_{eff}}{2l}} + 2e^{-\frac{D_{vt1} L_{eff}}{l}} \right) (V_t \ln \left[ \frac{N_{ch} N_{DS}}{n_i^2} \right] - \phi_s) \\ & - \left( e^{-\frac{D_{sub} L_{eff}}{2l_{io}}} + 2e^{-\frac{D_{sub} L_{eff}}{l_{io}}} \right) (E_{tao} + E_{tab} V_{bseff}) V_{DS} \end{aligned} \quad (1.6)$$

$$\begin{aligned} V_{th0}(T) = & V_{th0}(T_{nom}) + (KT1 + KT1L/L_{eff} \\ & + KT2 \cdot V_{bseff}) \cdot (T/T_{nom} - 1) \end{aligned} \quad (1.7)$$



While  $KT1$  is the dominant parameter to describe the temperature dependency of  $V_{th}$ ,  $KT1L$  improves the fitting for various channel length sizes and  $KT2$  models the temperature dependency of the body effect on  $V_{th0}$  [24].

### 1.2.3 Saturation velocity ( $v_{sat}$ )

In short channel devices, drain saturation voltage ( $V_{dsat}$ ) is used to mark the onset of velocity saturation rather than the conventional pinch-off assumption [2]. When a certain lateral electric field is attained, MOSFETs get into saturation region since carriers cannot move faster than  $v_{sat}$  [3]. The temperature dependence of  $v_{sat}$  is given in (1.8) [23].

$$v_{sat}(T) = v_{sat}(T_{nom}) - AT \cdot (T/T_{nom} - 1) \quad (1.8)$$

With temperature change,  $v_{sat}$  has a less evident impact compared to other parameters [26].

### 1.2.4 Drain-source parasitic resistance ( $R_{ds}$ )

$R_{ds}$  is called the parasitic drain-source resistance which includes different resistances such as the contact resistance, the diffusion resistance between the contact and the gate edge and the crowding resistance near the gate [2]. In BSIM3,  $R_{ds}$  has a fitting parameter  $R_{dsw}$  in (1.9); additionally, (1.10) is used to characterize the temperature dependence where  $PRT$  is the temperature coefficient [23]. Even though some methods have been developed to extract the drain-source parasitic resistance,  $R_{ds}$  change resembles mobility degradation and they can be treated similarly [27].

$$R_{ds} = (R_{dsw}[1 + P_{rwg} \cdot V_{gsteff} + P_{rwb} \times (\sqrt{\phi_s - V_{bseff}} - \sqrt{\phi_s})]) / (10^6 \cdot W_{eff'})^{(W_r)} \quad (1.9)$$

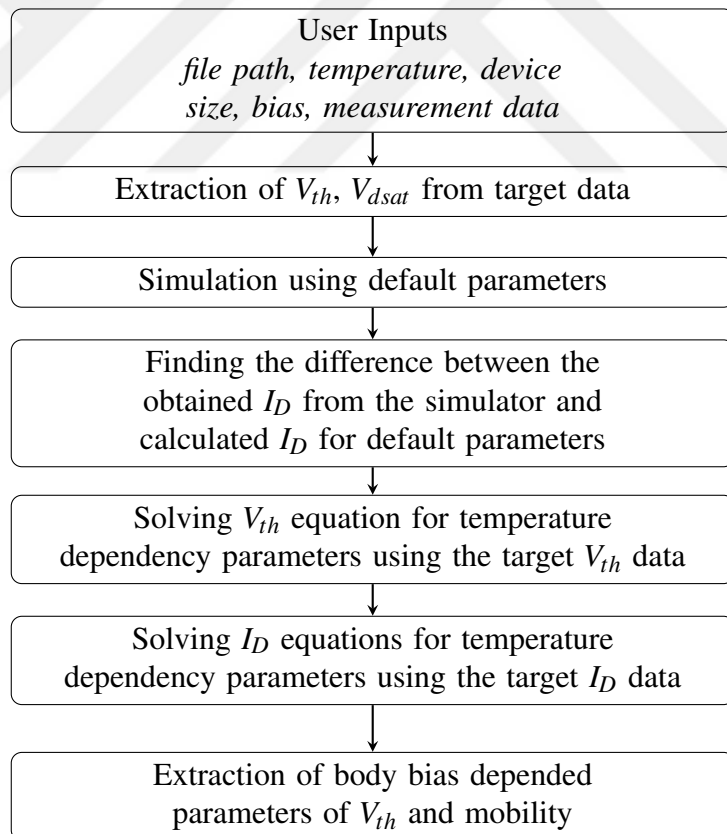
$$R_{dsw}(T) = R_{dsw}(T_{nom}) + PRT \cdot (T/T_{nom} - 1) \quad (1.10)$$



## 2. PROPOSED MODEL

### 2.1 Temperature Model Parameter Calibration Methodology

An algorithm is developed to change the temperature dependency model parameters in BSIM3(3v3) to make the models accurate for cryogenic applications. In this methodology, there is no need to adjust all coefficients of relevant equations as most model optimizers typically do. The algorithm modifies only the coefficients of temperature analytically. BSIM3 equations are used directly to calculate these parameters analytically. Because no equation of BSIM3 was manipulated, the extracted model can be used with any simulation tool supporting BSIM model file.



**Figure 2.1** : The flowchart of the proposed methodology [1]

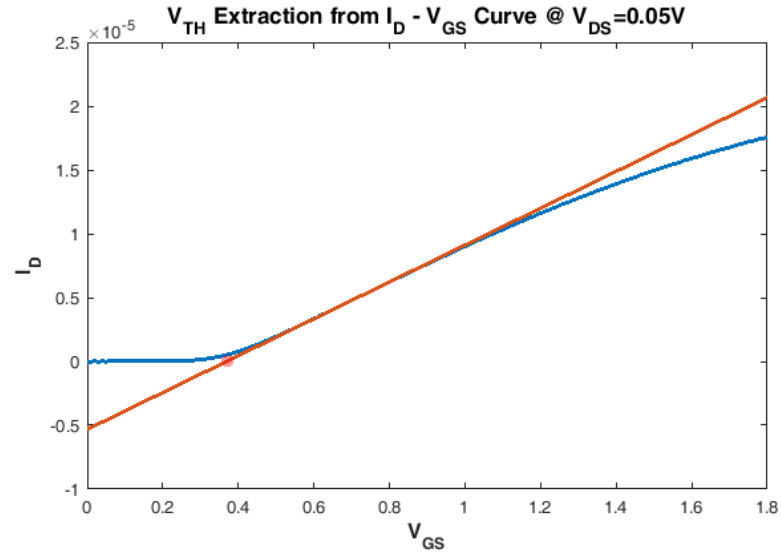
The algorithm was developed on MATLAB and the MATLAB runs circuit simulations on CADENCE Design Systems Spectre by using Ocean scripts. When MATLAB

got the necessary input data, it calls the Ocean scripts and imports simulation results which were written to a file after completion of simulations. Inputs required are the temperature of the experiment,  $I - V$  curves of measurements, biasing information, device sizes and the model file path. Subsequently, MATLAB starts to compute the temperature dependency parameters step by step through backward solving of BSIM3 equations. All steps to extract a new model file from measurement data are shown in Fig. 2.1

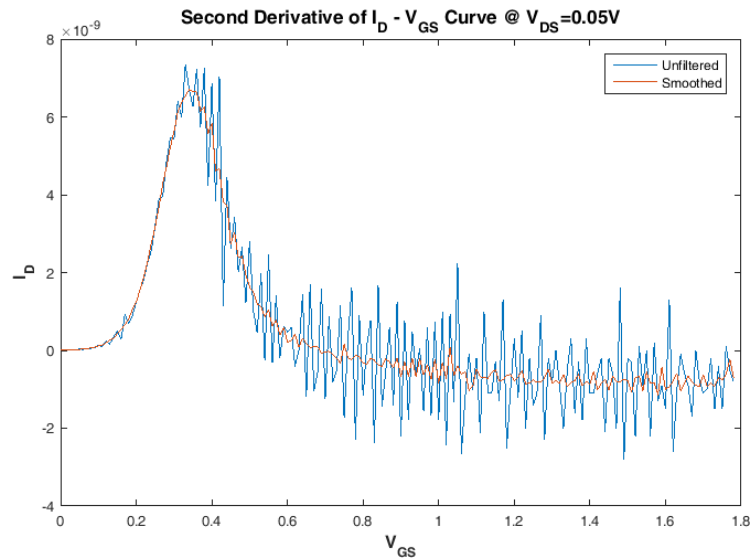
### 2.1.1 Processing the target data

When the temperature of interest is not within the range of BSIM (i.e. below  $-55^{\circ}C$ ), device measurements should be collected to optimize relevant BSIM parameters for the desired temperature. Firstly, the algorithm extracts the maximum device current at  $V_{DS} = V_{GS} = 1.8V$ , as well as corresponding  $V_{th}$  and  $V_{dsat}$ . There are numerous methods in the literature to extract  $V_{th}$  from the  $I - V$  curve of a transistor. In this work, two of these methods were considered; the first one is finding the intersection point of the voltage axis and the line extrapolated at the maximum value of the first derivative of the  $I_D - V_{GS}$  curve as shown in Fig. 2.2. The second one is taking the voltage that points the maximum value of second derivative of the normalized  $I_D - V_{GS}$  curve (Fig. 2.3). In order to remove the computational noise, a smoothing filter should be applied so that a meaningful threshold voltage value can be obtained [28]. This method sometimes results in an error because of the floating measurement data and insufficient filtering. Nevertheless, the second derivative method has been tested using the room temperature data and it yields a more accurate  $V_{th}$  value with respect to simulation results. Therefore, both the  $I - V$  curve extrapolation and second derivative methods are used concurrently for a reliable and accurate  $V_{th}$  extraction. Both procedures were applied at low  $V_{DS}$  as traditional  $V_{th}$  extraction methodology requires.

Another necessary step to mark the velocity saturation is  $V_{dsat}$  extraction from the  $I_D - V_{DS}$  curve. Both room temperature and cryogenic measurements were taken into account and the difference in  $V_{dsat}$  values of both curves are extracted because there is no exact method to determine  $V_{dsat}$  value alone using the  $I - V$  curve of the device. Fig. 2.4 shows the extraction method where two lines are drawn by extrapolating  $I - V$  curve at the minimum and maximum value points of the first derivative. Intersection



**Figure 2.2** : Demonstration of the extrapolation method for  $V_{TH}$  extraction

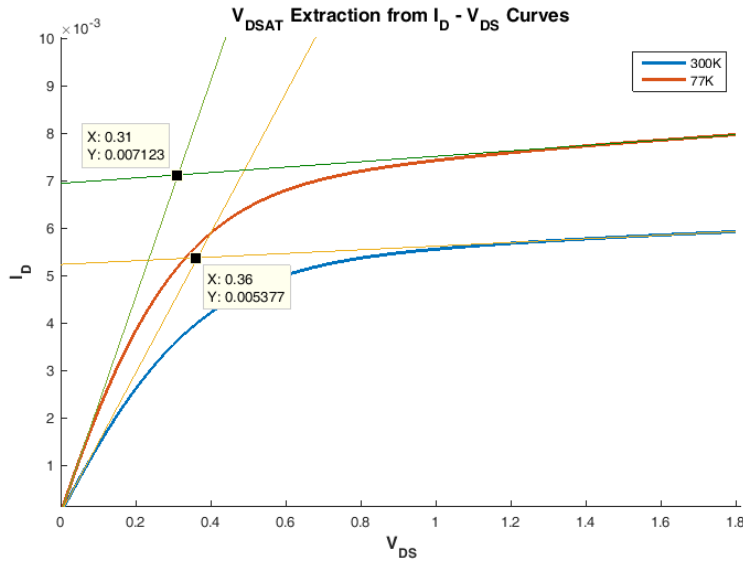


**Figure 2.3** : Demonstration of the second derivative method for  $V_{TH}$  extraction

points of these lines are taken as  $V_{dsat}$ . The difference of the  $V_{dsat}$  values are then used by the proposed modeling algorithm to calculate the temperature dependency parameter of  $v_{sat}$ .

### 2.1.2 Fixing BSIM equations

Published BSIM equations do not exactly correspond to the equations used in the simulator [23]. Since the simulator has a modified version of published BSIM equations, results of the equations calculated in MATLAB should be adjusted. A correction coefficient ( $\rho$ ) has been introduced to the  $I_D$  equation to eliminate this difference.  $\rho$  is extracted by subtracting the current value calculated with the



**Figure 2.4** : Demonstration of the extraction of  $V_{DSAT}$  change between the room and cryogenic temperature

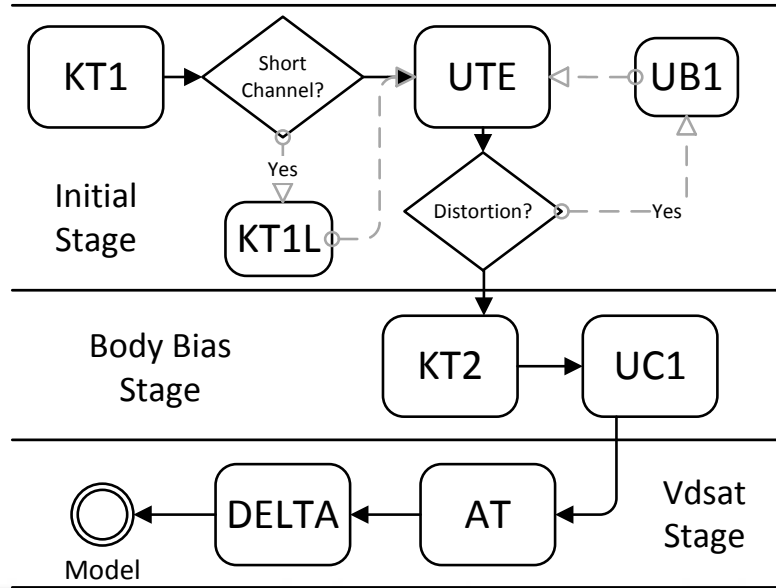
BSIM equations in MATLAB, from the current value simulated with initial model parameters at the highest bias used in measurements, i.e.  $V_{DS} = V_{GS} = 1.8 V$ . This choice of the bias will result in the maximum  $I_D - V_{DS}$  error to be observed. Based on this coefficient, MATLAB can produce the current values closest to the simulator result so that equations can be used to solve the revised values of temperature dependency parameters in cryogenic conditions.

### 2.1.3 Parameter extraction algorithm

The algorithm employs target measurement data to extract the temperature dependency parameters vector in (2.1) that minimizes the modeling error.

$$\vec{v}=[KT1, KT1L, KT2, UTE, UB1, UC1, AT, DELTA] \quad (2.1)$$

The extraction methodology is composed of eight steps and they can be grouped 3 stages as shown in Fig. 2.5 which are 1) parameter extraction without body effect, 2) parameter extraction at a specified body bias, 3)  $V_{dsat}$  difference elimination. In the first stage  $KT1, UTE$  and  $UB1$  will be evaluated without including the body effect. Then,  $KT2$  and  $UC1$  will be obtained at a specified body bias.  $V_{dsat}$  difference elimination consists of  $AT$  and  $DELTA$  extraction. If the modeling of the channel length scaling for the threshold voltage is desired, finding  $KT1L$  constitutes the sub-stage of the first stage and it is calculated after  $KT1$  parameter has been obtained. A long channel



**Figure 2.5 :** Parameter Extraction Algorithm

and a short channel device are necessary for this sub-stage. All other steps can be implemented considering a long channel device. If a designer wants to use just short channel devices in his/her own design, there is no need to use  $KT1L$  parameter, other stages will suffice to produce an accurate model for cryogenic conditions.  $R_{DS}$  was not included to the model extraction procedure due to the similarity between  $R_{DS}$  effect and mobility degradation.

Temperature change is modeled using  $KT1, KT2, KT1L$  for the threshold voltage;  $UTE, UB1, UC1$  for the mobility and  $AT$  for the  $V_{dsat}$ . Additionally,  $DELTA$  specifies the smoothness of the discontinuity between the linear and saturation region of a transistor in the  $I_D-V_{DS}$  curve.

#### 2.1.4 Computation cost of the methodology

The computation cost of the methodology consists of mostly circuit simulations done by the simulator, which means that the parameter extraction procedure takes much smaller time to complete. Extracted parameters are imported into the model file to perform simulations. Outcomes of these simulations are then used to validate new model parameters. Since the model generated should operate at different bias voltages for various device sizes, multiple simulations should run successively during model generation. Despite this simulation cost, the algorithm achieves its goal of providing a new model file suitable for the input cryogenic conditions in around 6 to 15 minutes

depending on device properties. It should be mentioned that the model generation is done only once for a given device type to be operated at cryogenic temperatures. Furthermore, the algorithm is made robust toward handling numerical problems that might occur during analytic operations to extract the new device model parameters.





### 3. EXPERIMENTAL RESULTS

A tape-out using the commercially available 180 nm technology has been accomplished to experimentally verify the algorithm, with regular n-type and p-type MOSFETs that were measured at cryogenic conditions. NMOS and PMOS devices of 5 different sizes are used to investigate the size dependency of MOSFETs' operational behavior at low temperatures. Additionally, an RF NMOS and low threshold voltage NMOS are included in measurement chip to investigate the effects of different MOSFET designs; also, RF MOSFETs will be used for fundamental applications of space electronics. All measured transistor types and their sizes are itemized in Table 3.1 and these items numbers will be referred throughout the rest of this thesis to specify each transistor.

**Table 3.1** : Device names and sizes

No	Type	Width	Length	No	Type	Width	Length
1	NMOS	0.24 $\mu m$	0.18 $\mu m$	7	PMOS	0.24 $\mu m$	0.18 $\mu m$
2	NMOS	10 $\mu m$	0.18 $\mu m$	8	PMOS	10 $\mu m$	0.18 $\mu m$
3	NMOS	0.24 $\mu m$	10 $\mu m$	9	PMOS	0.24 $\mu m$	10 $\mu m$
4	NMOS	10 $\mu m$	10 $\mu m$	10	PMOS	10 $\mu m$	10 $\mu m$
5	NMOS	35 $\mu m$	0.5 $\mu m$	11	PMOS	35 $\mu m$	0.5 $\mu m$
6	Low $V_{TH}$ NMOS	35 $\mu m$	0.5 $\mu m$	12	RF NMOS	35 $\mu m$	0.18 $\mu m$

A large size transistor 4 was chosen to analyze physical changes in MOSFETs at low temperatures without considering short channel and narrow width effects. Transistors 2 and 3 are employed to check these effects individually at cryogenic conditions. Additionally, the smallest size transistor is used to observe both effects together. Transistor 5 is a control device and it has a moderately long channel with regard to transistor 1 and 4. Transistors like 5 are typically used in analog circuits. Besides, the cryogenic behavior of 5 acts as a bridge between the cryogenic characteristics of the long channel and short channel devices. The transistor numbers between 7-11 are same size PMOS transistor of 1-5 transistors. Therefore, the effects of cryogenic conditions on n-type and p-type transistors can be investigated separately and change of

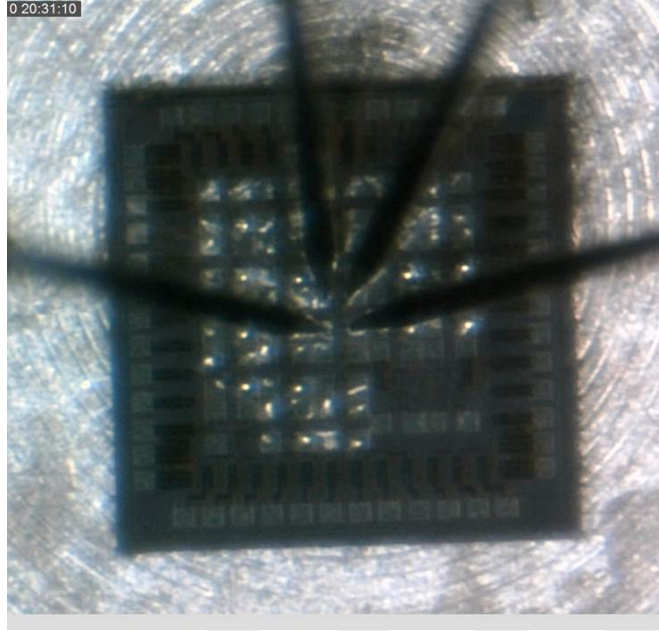


**Figure 3.1** : The measurement bench and probe station

model parameters can be considered individually. Aside from these, an RF transistor is considered to extract a model for RF circuit designs operating at very low temperatures. Because of the threshold voltage increase with temperature decrease, a low threshold voltage device 6 is considered of interest for digital applications. At least 10 chips from 3 wafers were put under test. Hence, the process variation and measurement errors can be considered in the research.

### **3.1 Measurement Setup**

Unpackaged dies from 3 different wafers have been measured using the MDC 441 cryogenic probe station. Agilent Technology B1500A semiconductor device analyzer is used to extract  $I$ - $V$  curves at different bias voltages. The temperature of the probe station chuck is monitored by a Keithley 2000 multimeter. The probe station is cooled by liquid nitrogen hence the chuck temperature decreased down to  $-196^{\circ}\text{C}$ . In the probe station, the chips are vacuumed by a compressor for avoiding undesirable slide. The typical supply voltage for this technology is 1.8 V and the devices under test were biased at  $V_{GS}$  values between 0.6 V and 1.8 V to extract  $I_D - V_{DS}$  curves. Also, the body effect was taken into account by changing  $V_{BS}$  from 0 down to  $-0.4$  V.  $I_D - V_{GS}$  curves were extracted in the same  $V_{BS}$  range by using two different  $V_{DS}$  values which

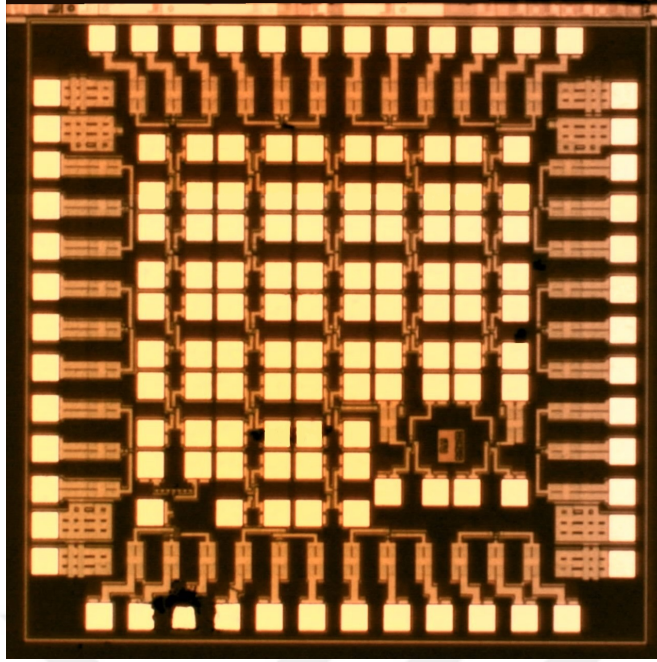


**Figure 3.2 :** The device under test

are 0.05 V and 1.8 V. Low  $V_{DS}$  is needed to capture the device threshold voltage. The measurement setup and the chip under test on the probe station are shown in Figs. 3.1 and 3.2. The measured dies are observed by microscope and DC probes of cryogenic measurement station are contacted with pads of each MOSFETs that are gate, drain, source, body contacts. The probes are moved manually and due to the sensitivity of measurement setup, these contacts are sometimes shorted as a result of touching probes to wrong areas. Therefore, some chips got lost and measurements were repeated again. This situation also creates measurement variation due to probe-pad contact. Before creating new model files, this case was taken into account and mean current values of measurements were used in the algorithm to suppress this measurement variation. The contacts of MOSFETs can be seen in the Fig. 3.3. The size of the die is  $1.5m^2$  and each group of 4 pad represents one MOSFET.

### **3.2 Comparison of the Measurements between Cryogenic Temperature and Room Temperature**

At both room temperature and cryogenic conditions, 10 different dies were measured for each size of NMOS and PMOS devices to extract the correct model parameters. The Figs. 3.4, 3.5 and 3.6 show  $I_D - V_{GS}$  measurements at  $V_{DS} = 0.05V$  to indicate  $V_{TH}$  increase as temperatures drop down. In Figs. 3.4a-3.4e, comparison of  $I - V$

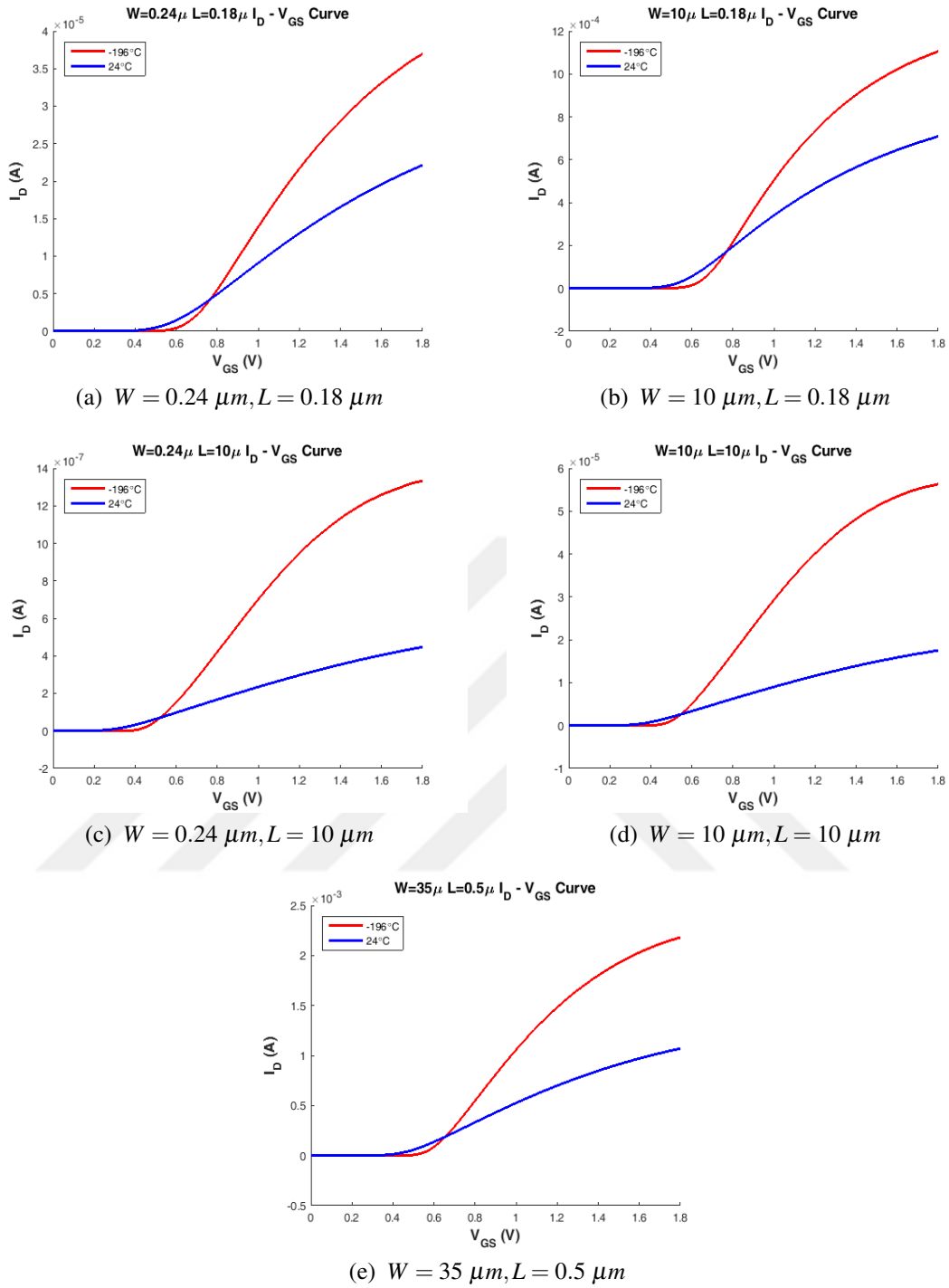


**Figure 3.3** : The die layout observed with a microscope

for NMOS devices of various sizes and in Figs. 3.5a-3.5e, comparison of  $I - V$  for PMOS devices of various sizes are shown both at room and cryogenic temperatures. Additionally an RF-NMOS transistor with size of  $35 \mu m \times 0.18 \mu m$  and a low threshold voltage NMOS device with the same reference size transistor's measurement result are shown in Fig. 3.6a,3.6b.

The Figs. 3.7, 3.8 and 3.9 represent mean  $I_D - V_{DS}$  curves of 10 measurements for each kind of transistor at  $V_{GS} = 1.8V$  and  $\pm 3\sigma$  values are found using the experimental data to show the statistical variance of transistors. All size of NMOS and PMOS device measurements are shown in Figs. 3.7a-3.7e and Figs. 3.8a-3.8e respectively. The RF-NMOS transistor and the low threshold NMOS device measurement results are also shown in Fig. 3.9a,3.9b.

The mean curve of NMOS devices has variations between %0.9 and %6.6, in comparison to the simulation results at the typical (TT) corner found by simulating the default model parameter set provided by the manufacturing company. Current increase rates of devices with temperature decrease are not equal, they depend on device sizes. It is clear from Table 3.3, that the current increase ratios are strongly correlated with device lengths. Transistors 1 and 2 have the same length, different width and the increase rates are almost the same. When the device length is raised to



**Figure 3.4 :** NMOS  $I_D - V_{GS}$  Curve @  $V_{DS} = 0.05V$  demonstrating  $V_{TH}$  increase as temperatures drop down

$10 \mu\text{m}$  from  $0.18 \mu\text{m}$ , current increase ratios became around 6 times higher for NMOS devices and 5 times higher for PMOS devices. As the increase ratio became higher, larger device widths have a slight impact on the ratio. If process variations are taken into account, the ratio change due to width difference can be practically ignored. The situation can be explained as the basis of the difference between the short channel and

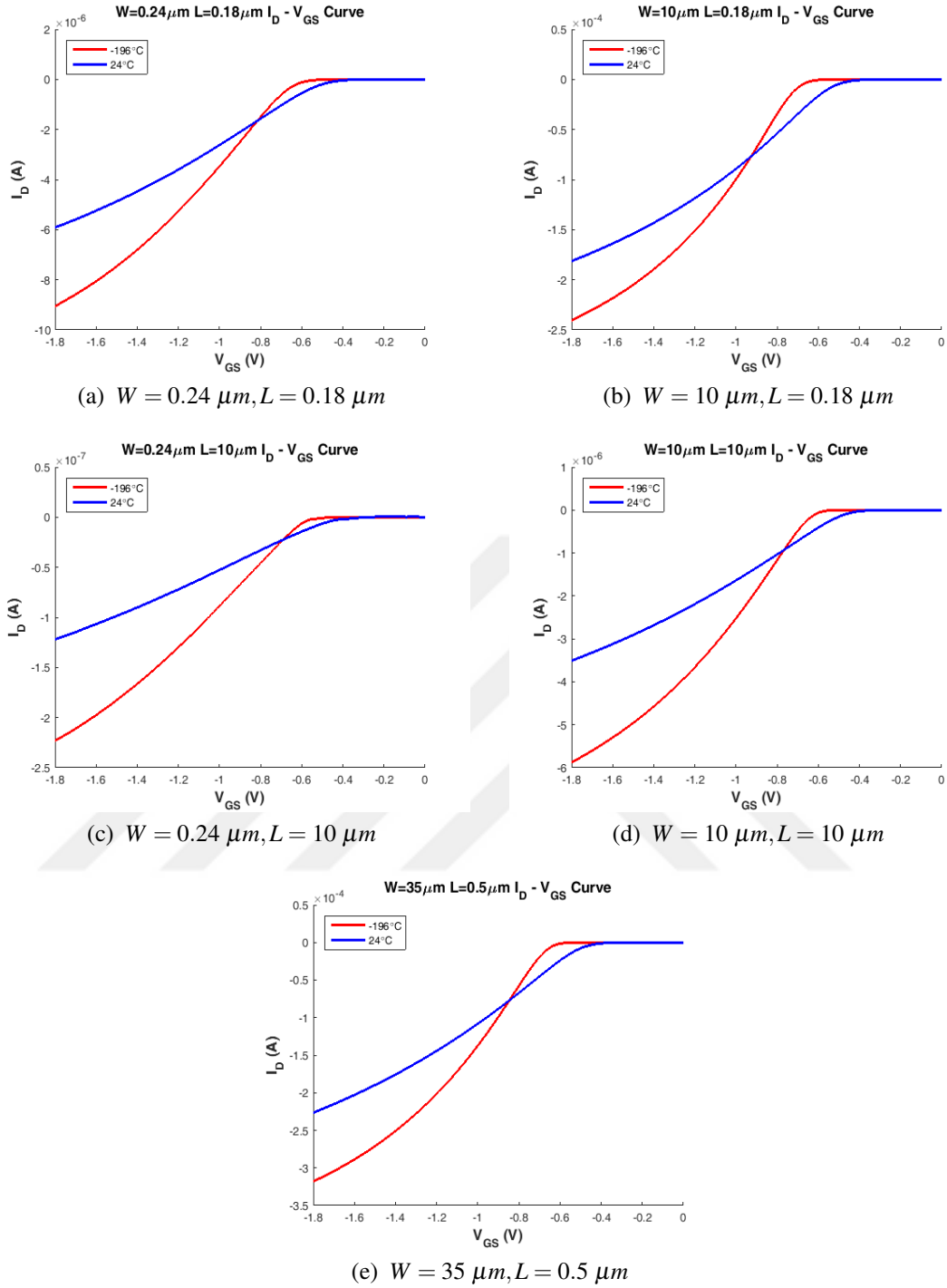
long channel transistors: In short channel transistors, charge carriers already operate at a large longitudinal electric field thus they are close to the velocity saturation regime, in which, the increase of the mobility at cryogenic temperatures does not increase the drain current. Conversely, in long channel transistors, charge carriers are far from velocity saturation, thus the low field mobility increase makes a greater impact on the drain current of the long channel transistor [25]. Because holes have less mobility, PMOS current increase amounts are not as remarkable as those of NMOS devices (Fig. 3.8a-3.8b).

Threshold voltage increase amounts for various transistors are shown in Table 3.2. These  $V_{TH}$  values are extracted from graphs with the method mentioned in section PROPOSED MODEL. Because of the threshold voltage extraction procedure sensitivity, it is hard to comment on the relationship between transistor sizes and threshold voltage increase. Thus, the size dependence of the threshold voltage increase can be practically ignored. All of the transistors have similar threshold voltage increase amounts because the bulk Fermi potential increase is independent of device size and the transistors get into the strong inversion regime when surface potential equals twice the bulk potential [29]. Therefore, it is assumed that the necessary gate voltage does not change with different device sizes to create the same surface potential.

**Table 3.2** : Threshold Voltage increase amounts

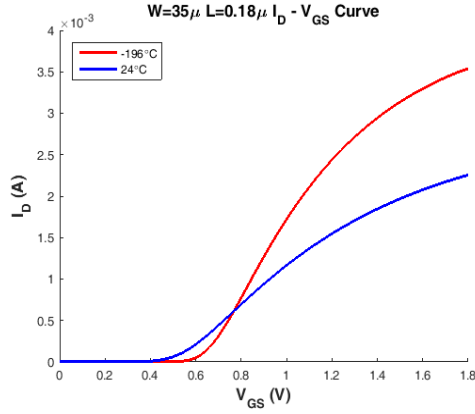
Type	Size( $W \times L$ )	Room Temp.	Cryogenic	Difference
NMOS	$0.24 \mu m \times 0.18 \mu m$	0.54 V	0.69 V	0.15 V
NMOS	$10 \mu m \times 0.18 \mu m$	0.53 V	0.64 V	0.11 V
NMOS	$0.24 \mu m \times 10 \mu m$	0.30 V	0.46 V	0.16 V
NMOS	$10 \mu m \times 10 \mu m$	0.34 V	0.5 V	0.16 V
NMOS	$35 \mu m \times 0.5 \mu m$	0.44 V	0.56 V	0.12 V
PMOS	$0.24 \mu m \times 0.18 \mu m$	-0.49 V	-0.64 V	-0.15 V
PMOS	$10 \mu m \times 0.18 \mu m$	-0.52 V	-0.69 V	-0.17 V
PMOS	$0.24 \mu m \times 10 \mu m$	-0.42 V	-0.55 V	-0.13 V
PMOS	$10 \mu m \times 10 \mu m$	-0.46 V	-0.62 V	-0.16 V
PMOS	$35 \mu m \times 0.5 \mu m$	-0.49 V	-0.66 V	-0.17 V
RF NMOS	$35 \mu m \times 0.18 \mu m$	0.51 V	0.63 V	0.12 V
Low $V_{TH}$ NMOS	$35 \mu m \times 0.5 \mu m$	0.16 V	0.29 V	0.13 V

The drift current is related to the lateral electric field and the drain current saturates after a specific electric field  $E_{SAT}$ . The voltage that generates  $E_{SAT}$  is called  $V_{dsat}$ . If the electric field magnitude is below  $E_{SAT}$ , the carrier velocity is determined by

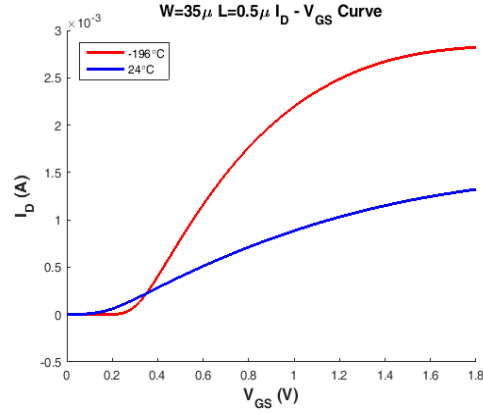


**Figure 3.5 :** PMOS  $I_D - V_{GS}$  Curve @  $V_{DS} = 0.05V$  demonstrating  $V_{TH}$  increase as temperatures drop down

the low-field mobility. After  $V_{DS}$  reaches the  $V_{dsat}$  value the average carrier velocity becomes equal to the saturation velocity. Mobility has a much higher increase compared to  $v_{sat}$ ; hence, carriers reach  $v_{sat}$  value faster at lower temperatures and  $V_{dsat}$  becomes smaller. Even though the saturation velocity increases with temperature decrease,  $V_{dsat}$  cannot increase along with the saturation velocity because of the



(a) RF-NMOS  $W = 35 \mu m, L = 0.18 \mu m$



(b) Low  $V_{TH}$  NMOS  $W = 35 \mu m, L = 0.5 \mu m$

**Figure 3.6** :  $I_D - V_{GS}$  Curve @  $V_{DS} = 0.05V$  demonstrating  $V_{TH}$  increase as temperatures drop down

**Table 3.3** : The maximum current value comparison of transistors both at the room temperature and cryogenic temperature

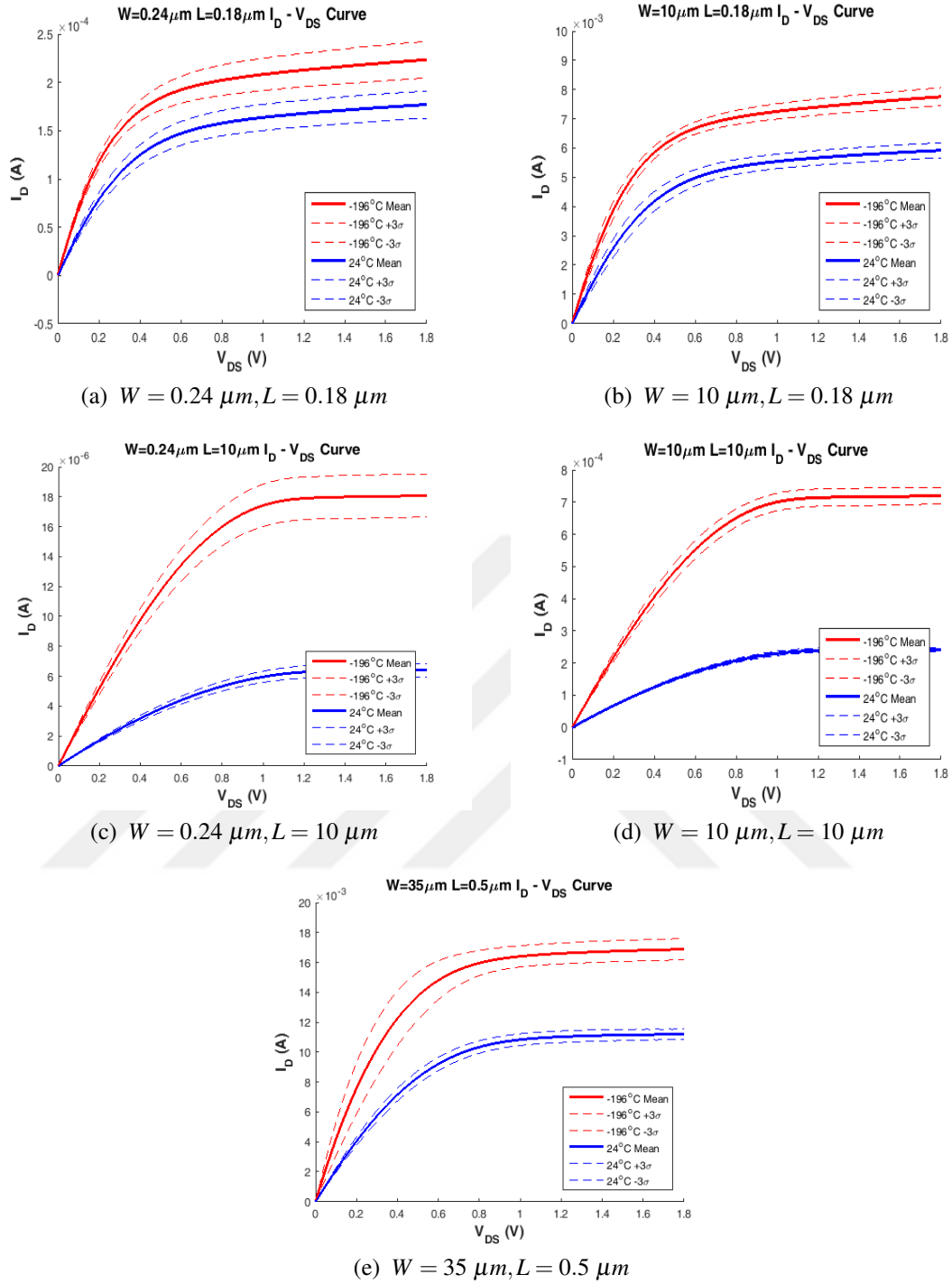
Type	Size(WxL)	Room Temp.	Cryogenic	Difference	Increase
NMOS	$0.24 \mu m \times 0.18 \mu m$	0.177 mA	0.223 mA	0.057 mA	%32
NMOS	$10 \mu m \times 0.18 \mu m$	5.92 mA	7.75 mA	1.83 mA	%31
NMOS	$0.24 \mu m \times 10 \mu m$	$6.39 \mu A$	$18.0 \mu A$	$11.6 \mu A$	%181
NMOS	$10 \mu m \times 10 \mu m$	0.241 mA	0.719 mA	0.478 mA	%198
NMOS	$35 \mu m \times 0.5 \mu m$	11.2 mA	16.92 mA	5.72 mA	%51
PMOS	$0.24 \mu m \times 0.18 \mu m$	$-70.7 \mu A$	$-81.5 \mu A$	$-10.8 \mu A$	%15
PMOS	$10 \mu m \times 0.18 \mu m$	$-2.29 mA$	$-2.65 mA$	$-0.36 mA$	%15
PMOS	$0.24 \mu m \times 10 \mu m$	$-1.41 \mu A$	$-2.44 \mu A$	$-1.03 \mu A$	%73
PMOS	$10 \mu m \times 10 \mu m$	$-40.5 \mu A$	$-62.9 \mu A$	$-22.4 \mu A$	%55
PMOS	$35 \mu m \times 0.5 \mu m$	$-2.78 mA$	$-3.63 mA$	$-0.85 mA$	%30
RF NMOS	$35 \mu m \times 0.18 \mu m$	20.28 mA	26.92 mA	6.64 mA	%33
Low $V_{TH}$ NMOS	$35 \mu m \times 0.5 \mu m$	16.92 mA	25.31 mA	8.39 mA	%50

mobility increase. In the measurement results,  $V_{dsat}$  decreased by 0.05 V to 0.15 V when the maximum gate-source bias is applied.

### 3.2.1 Measurements at various intermediate temperatures

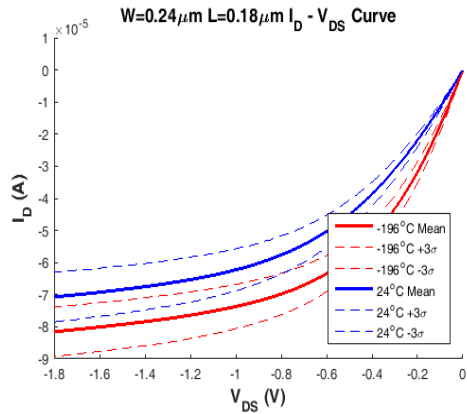
In addition to transistor measurements at  $-196^\circ C$ ,  $I-V$  curves were extracted at various intermediate temperatures between  $-196^\circ C$  and  $-40^\circ C$ . Extraction temperatures of these curves can vary by  $\pm 2^\circ C$  around the reported extraction temperature. It is observed that the drain current of each transistor increases monotonically as temperatures go down. For the 180 nm device technology and the corresponding



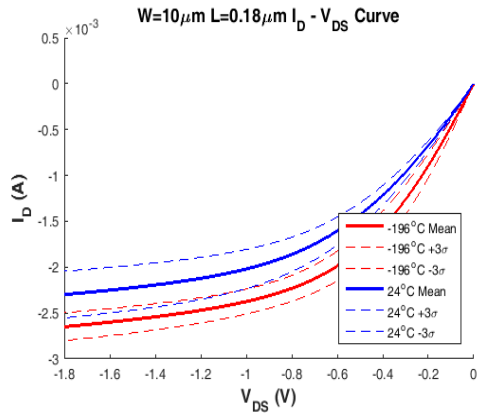


**Figure 3.7** : The mean result and variations of NMOS measurements at  $24^\circ\text{C}$  and  $-196^\circ\text{C}$

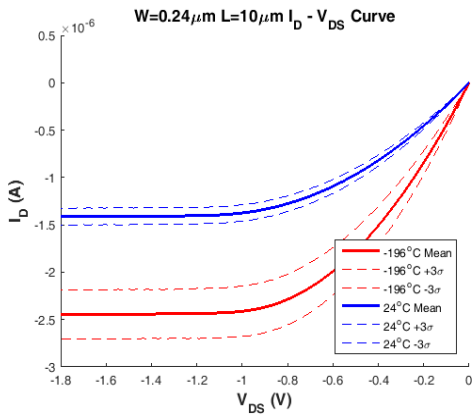
doping concentration amounts, freeze-out effects have not been come across within this temperature range. In Figs.3.10a to 3.11c, it can be seen that the mobility increases steadily from  $-40^\circ\text{C}$  to  $-196^\circ\text{C}$  for various sizes of NMOS and PMOS devices respectively.



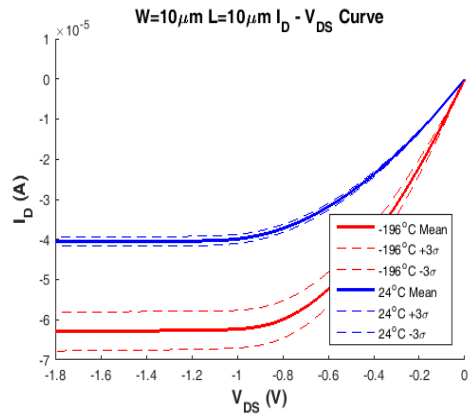
(a)  $W = 0.24 \mu m, L = 0.18 \mu m$



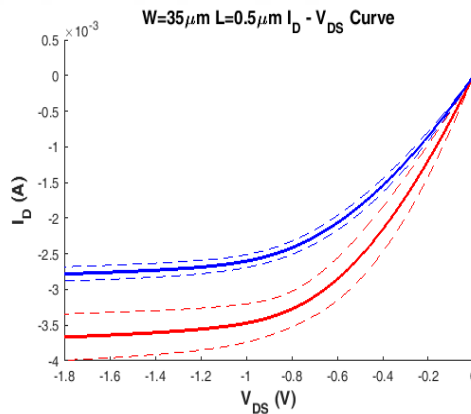
(b)  $W = 10 \mu m, L = 0.18 \mu m$



(c)  $W = 0.24 \mu m, L = 10 \mu m$



(d)  $W = 10 \mu m, L = 10 \mu m$



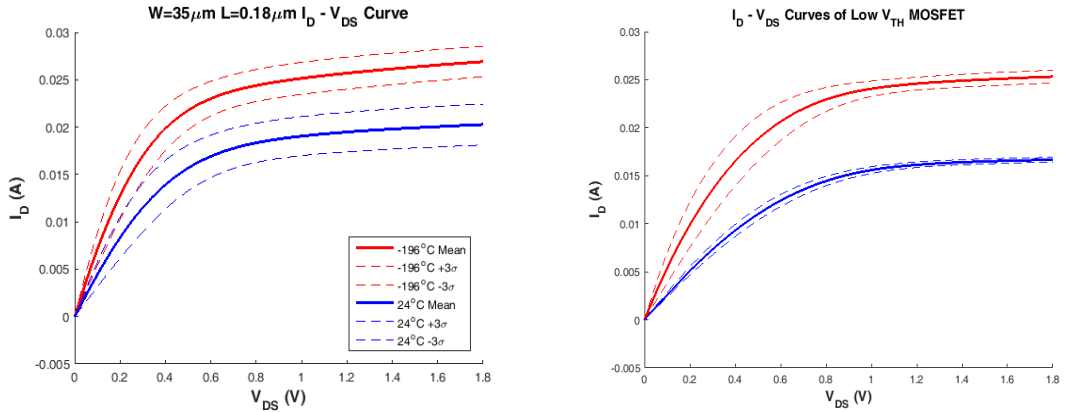
(e)  $W = 35 \mu m, L = 0.5 \mu m$

**Figure 3.8** : The mean result and variations of PMOS measurements at  $24^{\circ}C$  and  $-196^{\circ}C$

### 3.2.2 Extracted model parameters

#### 3.2.2.1 Model usage in simulation

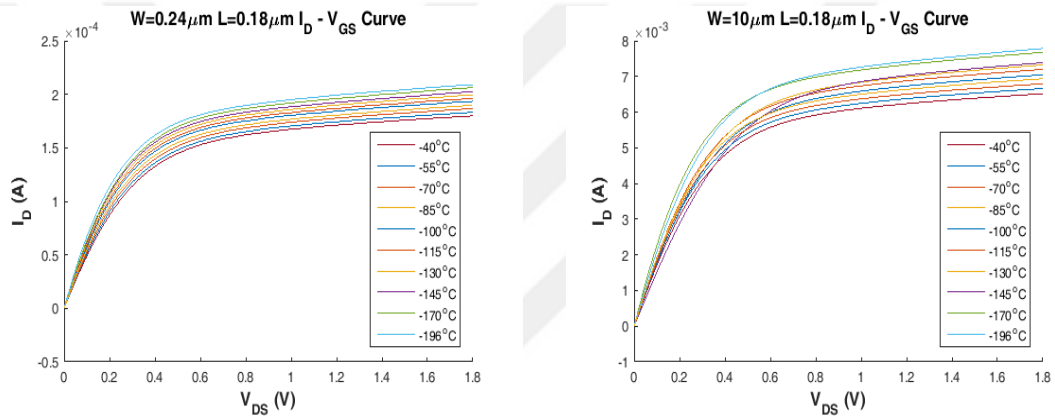
BSIM3 is one the most commonly used model standard in the industry, it is developed by University of California, Berkeley. However, BSIM models provided



(a) RF-NMOS  $W = 35 \mu m, L = 0.18 \mu m$

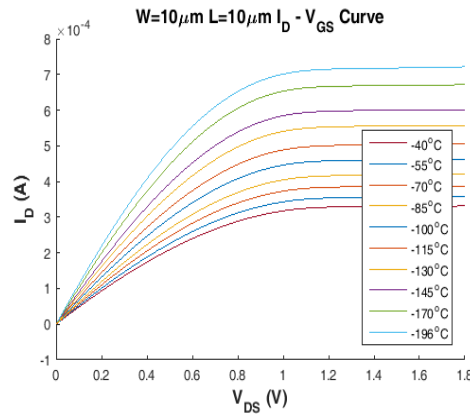
(b) Low  $V_{TH}$  NMOS  $W = 35 \mu m, L = 0.5 \mu m$

**Figure 3.9** : The mean result and variations of RF and Low  $V_{TH}$  NMOS measurements at  $24^\circ C$  and  $-196^\circ C$



(a)  $W = 0.24 \mu m, L = 0.18 \mu m$

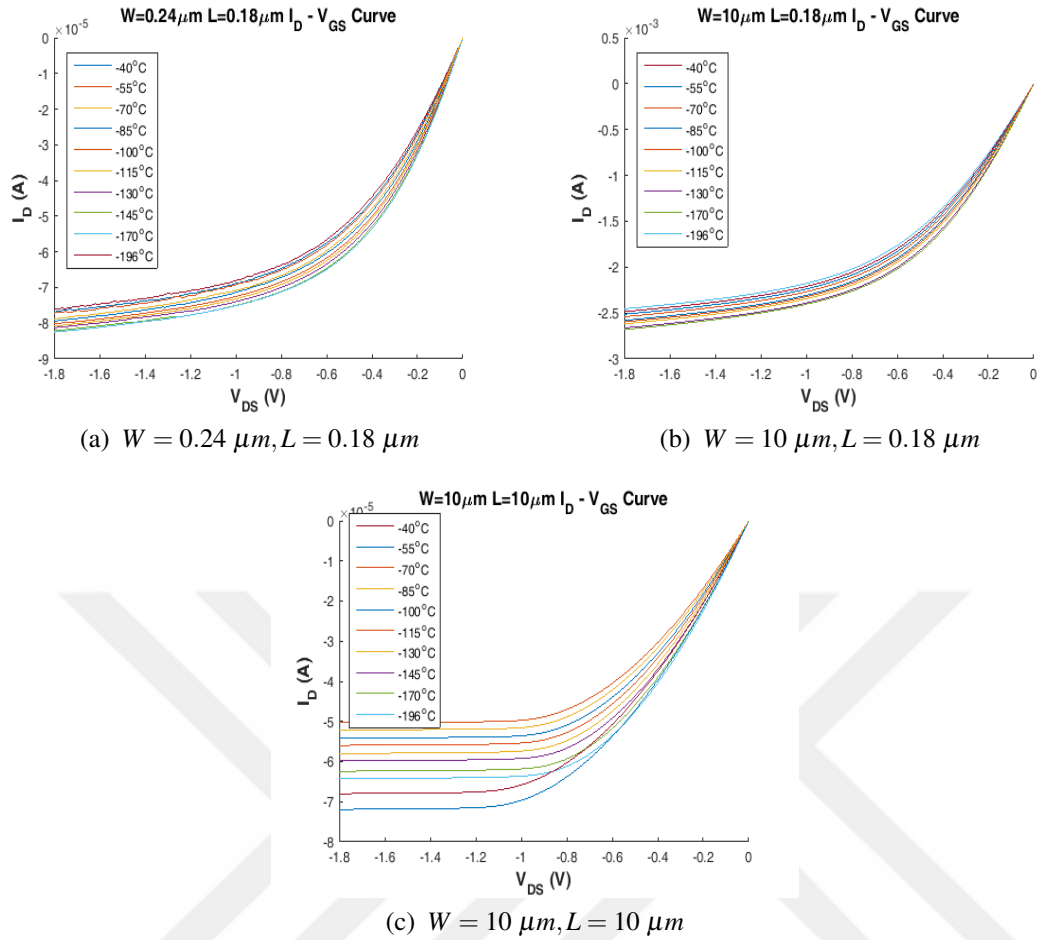
(b)  $W = 10 \mu m, L = 0.18 \mu m$



(c)  $W = 10 \mu m, L = 10 \mu m$

**Figure 3.10** :  $I_D - V_{DS}$  measurements of NMOS devices from  $-40^\circ C$  to  $-196^\circ C$

by manufacturers can not fit the experimental results at cryogenic conditions, because the model standard uses different equations for sub-threshold, linear and saturation regimes and it has fitting parameters extracted from measurements to fit simulation results to measured curves and these fitting parameters are products of temperature as



**Figure 3.11** :  $I_D - V_{DS}$  measurements of PMOS device from  $-40^{\circ}C$  to  $-196^{\circ}C$

shown in 1.2 and gives the best result only in room temperature. When the working conditions are far away from room temperature, the model cannot converge to real values with default parameters. Furthermore, BSIM3 has a deficiency in modeling the channel length dependency of mobility. Different size transistors have distinct mobility increase amounts at low temperatures. Therefore, if a designer wants to obtain less error between simulations and measurements, different parameter sets for short and long channel devices should be used to adjust the model at low temperatures. Simulation programs allow designers to use multiple model files in the same design so different parameter sets can be used for different size transistors if lower errors are desired.

In the algorithm, mobility phenomena does not have length and temperature dependency together but threshold voltage has a parameter for model this dependency. The KT1L parameter specifies threshold voltage length dependency and KT1L extraction step in the proposed methodology can be used to get a single parameter set

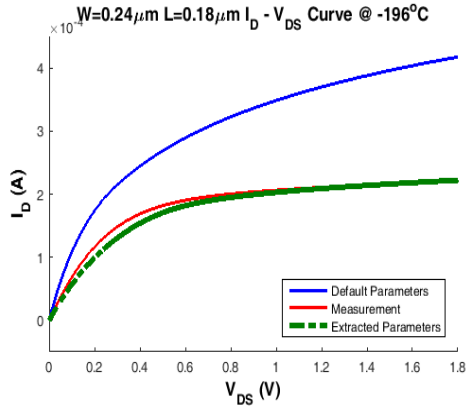
to model the threshold voltage for various size transistors at cryogenic temperatures; otherwise, this step can be disabled and the user can create new model files considering different measurements of various size transistors. The extracted new model files should be included within the simulation model file directory; after that, the designer can make simulations on any simulator that supports BSIM.

### **3.2.2.2 Comparison of default and extracted model**

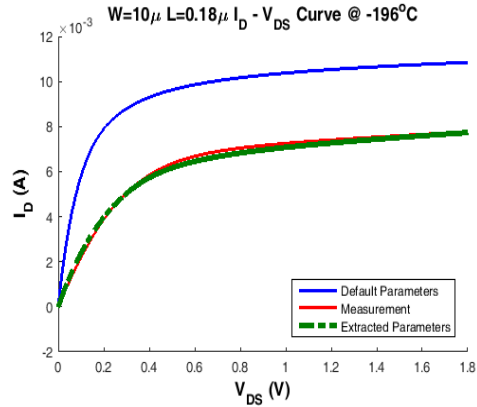
Without generating any new model card, designers can only use the default model file provided by the manufacturer. This model file cannot be used below  $-55^{\circ}C$  and the error margin of the model increases dramatically in cryogenic conditions as shown in Figs. 3.12-3.14. The algorithm can produce a new model parameter set for specific temperatures so the error rate can be minimized at that temperature as default parameters give the best result only at room temperature and error rates of parameter sets increase when moving away from the extraction temperature.

The comparison of measurements with simulation results using the extracted parameters are shown in Figs.3.12a–3.17b. Here, the error rate is scaled below %5 for different parameter sets extracted per each transistor type. The error rates for different gate bias and temperature conditions are given in Table 3.4 and 3.5 and these error rates have similar values with body effect presence because the temperature dependency parameter of the body bias is also modified at cryogenic conditions as discussed previously. The model accuracy reduces for very long channel devices but the model performs with high accuracy in 180 nm and 500 nm devices which are commonly used in analog applications. Furthermore, these transistors produce accurate simulation results with the revised model file in a larger temperature range in comparison to long channel devices. Although default parameters are valid at  $-55^{\circ}C$ , the new parameter set has a smaller error at this specific temperature for the above mentioned devices.

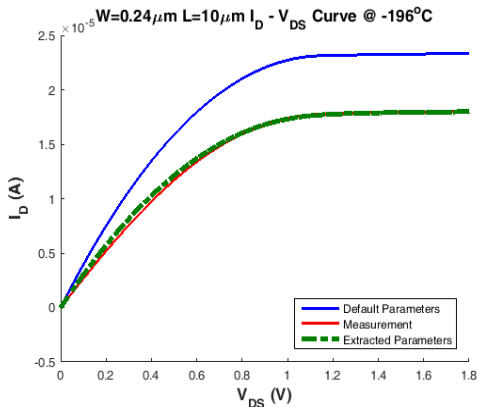
The extracted models performance in cryogenic conditions are not related with default model success. As shown in Table 3.4 the number 1 NMOS that has the smallest device size has %74.1 error with default model and it is decreased to %4.0 with extracted model. Although the device 4 has similar error rates with default model, it can be



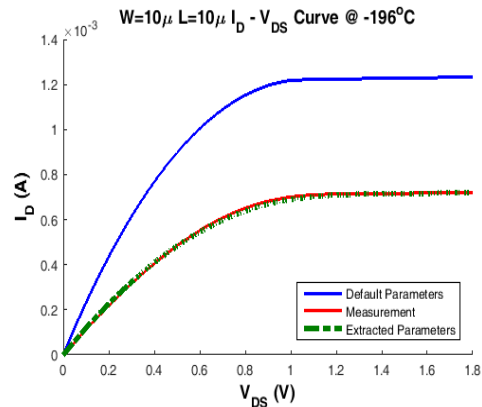
(a)  $W = 0.24 \mu m, L = 0.18 \mu m$



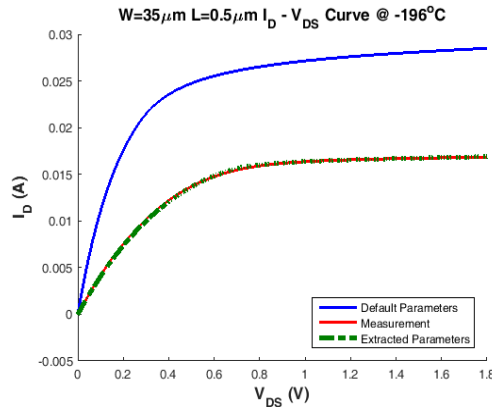
(b)  $W = 10 \mu m, L = 0.18 \mu m$



(c)  $W = 0.24 \mu m, L = 10 \mu m$



(d)  $W = 10 \mu m, L = 10 \mu m$

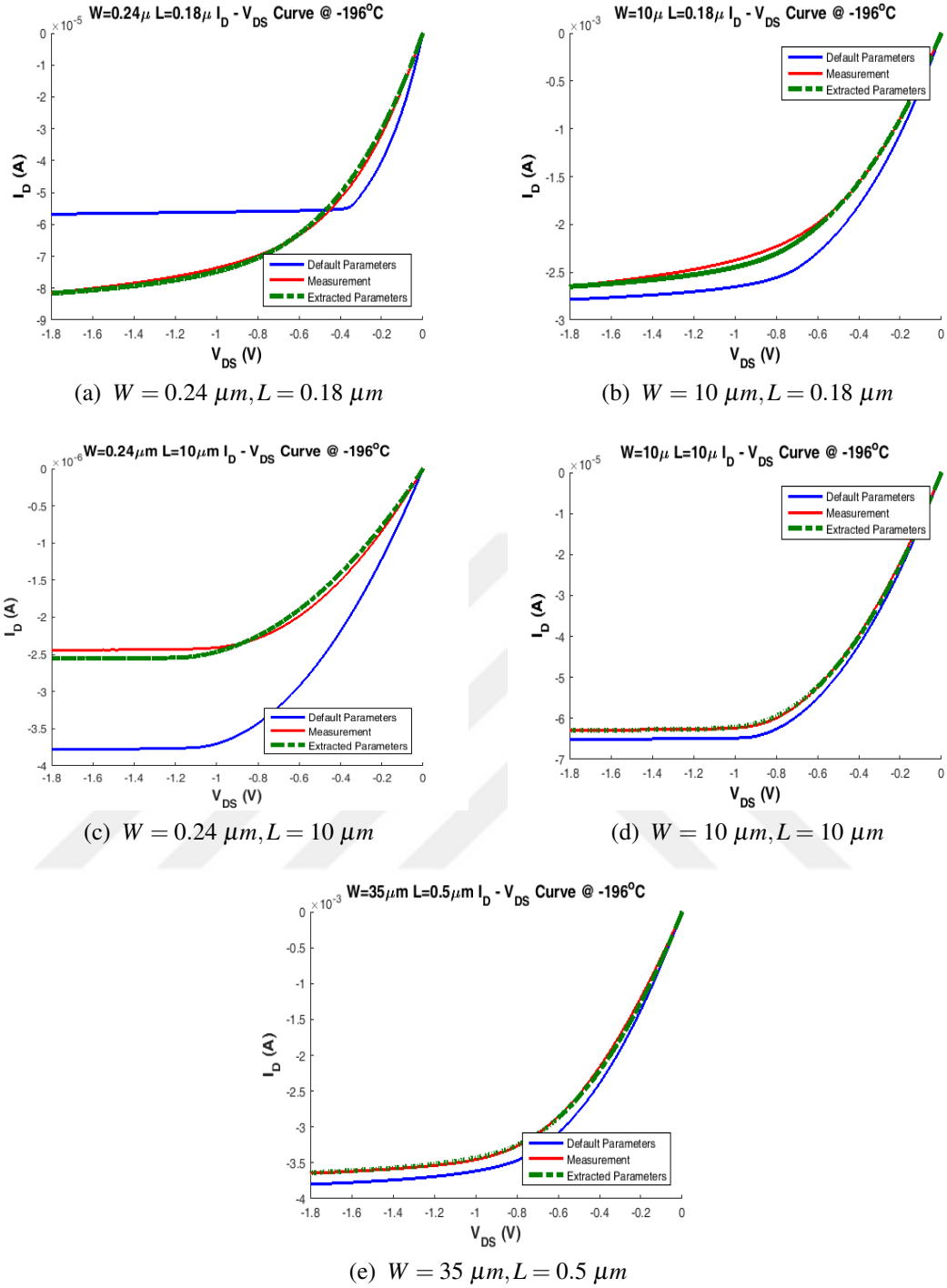


(e)  $W = 35 \mu m, L = 0.5 \mu m$

**Figure 3.12** : Comparison of the default model and extracted models of NMOS with measurement results at  $-196^{\circ}C$

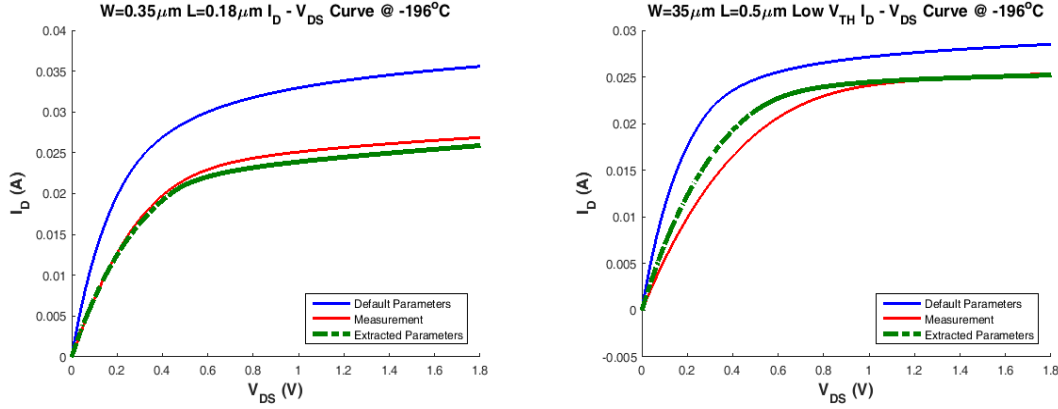
decreased to %1.1. The device 3 has similar error rates with device 1 when extracted model used but its initial error is smaller than the half of the error of device 1.

Although current increase by temperature lowering depends on length size, we cannot observe any relation between length size and default model mismatch to measurements when Figs. 3.12 and 3.13 are considered. However, the default model shows better



**Figure 3.13** : Comparison of the default model and extracted models of PMOS with measurement results at  $-196^\circ\text{C}$

performance on PMOS devices comparing the performance on NMOS device because holes have less mobility that involves less current increase; therefore, default model errors do not increase as much as NMOS devices. Hence, the proposed model is independent of the initial error rates of the default model and the size of devices because the methodology uses BSIM equations with measurements and it solves



(a) RF NMOS  $W = 35 \mu m, L = 0.18 \mu m$

(b) Low  $V_{TH}$  NMOS  $W = 35 \mu m, L = 0.5 \mu m$

**Figure 3.14** : Comparison of the default model and extracted models of PMOS with measurement results at  $-196^{\circ}C$

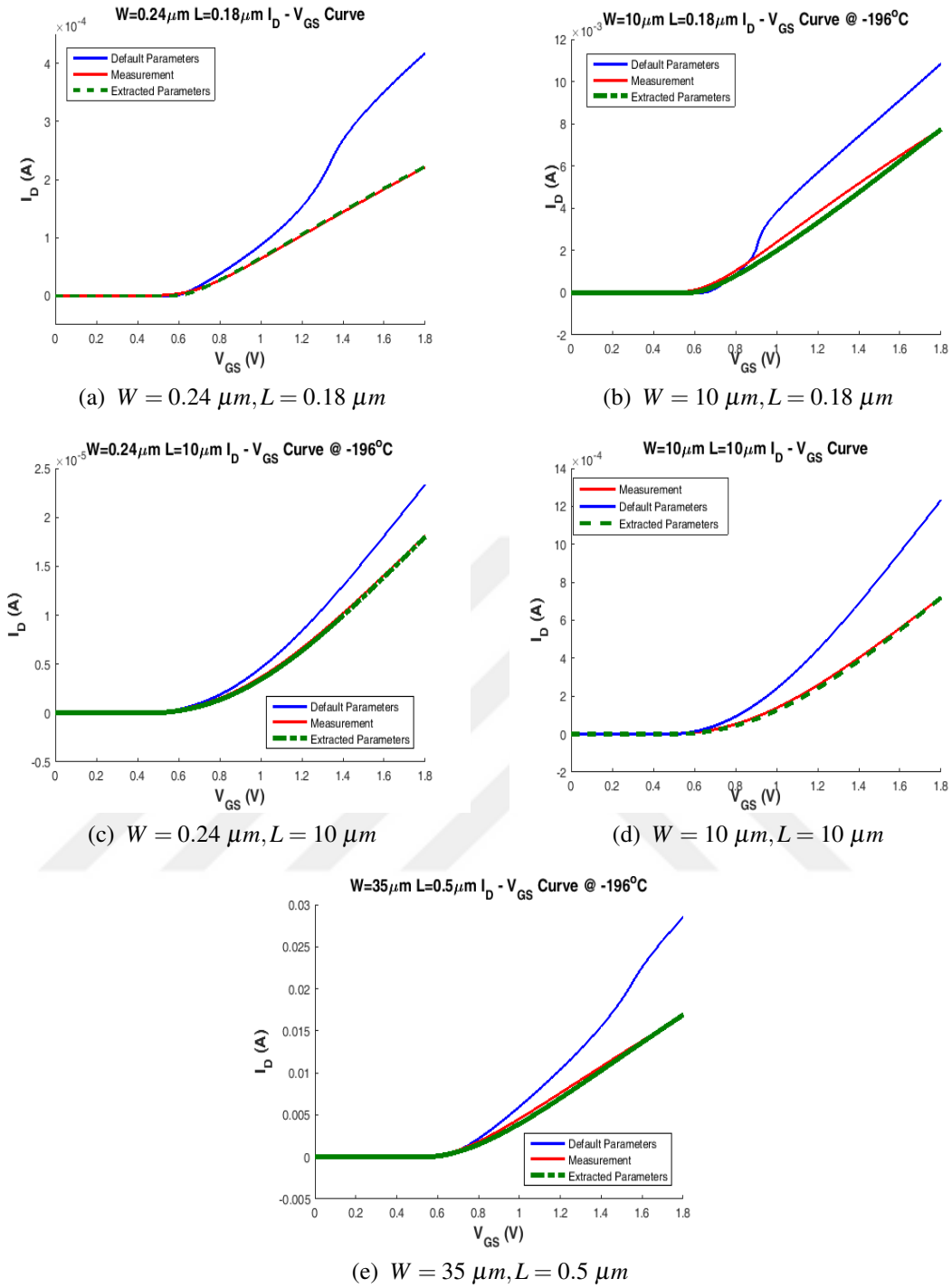
equations considering device size and the simulation software results that works in parallel with the model algorithm.

The curves obtained from simulations with default parameters in cryogenic conditions have insufficiency on both  $I_D - V_{DS}$  and  $I_D - V_{GS}$ . In addition to current mismatch, the shapes of the curves are also incompatible with reality. The shape of the  $I_D - V_{DS}$  curves vary on  $V_{DSAT}$ . Especially in the  $I_D - V_{GS}$  simulations, curves can become distorted in active region when default parameters are used at low temperatures. The Figs. 3.15a and 3.15b have such cases and their shapes are not related with device physics. These distortions are treated separately in the algorithm and the UB1 parameter that specify second order mobility degradation is optimized to restore proper  $I_D - V_{GS}$  curve shape as discussed in section PROPOSED MODEL.

**Table 3.4** : Error rates of  $I_D - V_{DS}$  curves @  $|V_{GS}| = 1.8V$  with extracted model files at  $-196^{\circ}C$  for transistors of every size and the model performance at different temperatures

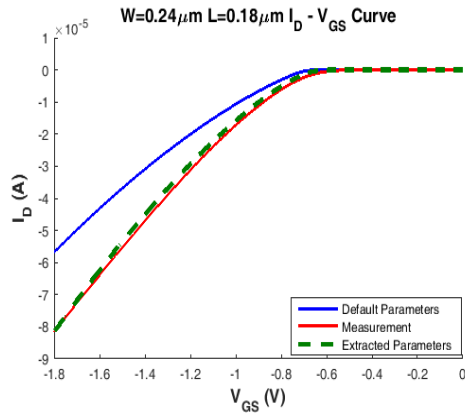
Type	Size(WxL)	$-196^{\circ}C$		$-170^{\circ}C$		$-145^{\circ}C$	
		Def.(%)	Model(%)	Def.(%)	Model(%)	Def.(%)	Model(%)
NMOS	$0.24 \mu m \times 0.18 \mu m$	71.1	4.0	42.0	5.7	26.3	8.4
NMOS	$10 \mu m \times 0.18 \mu m$	48.7	1.8	49.8	5.6	57.0	5.7
NMOS	$0.24 \mu m \times 10 \mu m$	31.4	3.9	-	-	-	-
NMOS	$10 \mu m \times 10 \mu m$	75.0	1.1	34.5	15.2	16.4	19.9
NMOS	$35 \mu m \times 0.5 \mu m$	99.7	0.6	-	-	-	-
PMOS	$0.24 \mu m \times 0.18 \mu m$	39.5	1.6	25.4	8.9	24.8	13.2
PMOS	$10 \mu m \times 0.18 \mu m$	11.0	2.0	12.1	4.7	11.4	5.3
PMOS	$0.24 \mu m \times 10 \mu m$	13.6	4.3	-	-	-	-
PMOS	$10 \mu m \times 10 \mu m$	4.3	0.6	7.1	10.2	11.4	13.8
PMOS	$35 \mu m \times 0.5 \mu m$	5.9	1.1	-	-	-	-
RF_N	$35 \mu m \times 0.18 \mu m$	33.2	1.3	31.3	5.3	32.3	3.4



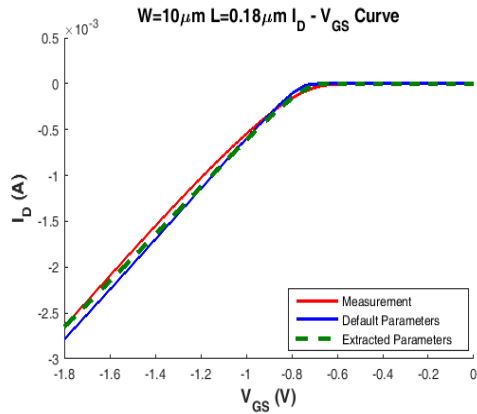


**Figure 3.15** : Comparison of the default model and extracted model of NMOS with measurement results at  $-196^{\circ}\text{C}$

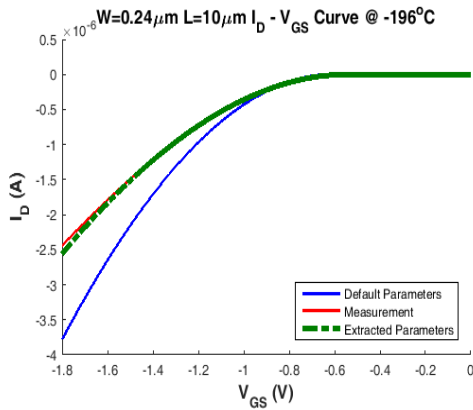
In addition to the extraction of different parameter sets for each transistor, a single parameter set can be obtained by only considering transistors 1, 2 and 5. This is especially useful and critical for analog and mixed-signal circuits where transistors of multiple channel lengths used together in a circuit topology. Transistors 1,2 and 5 can be counted as the most common devices observed in typical analog circuit blocks.



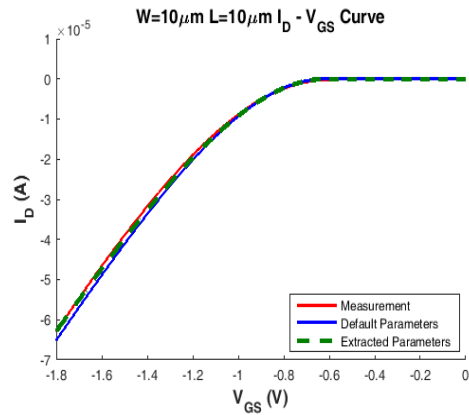
(a)  $W = 0.24 \mu m, L = 0.18 \mu m$



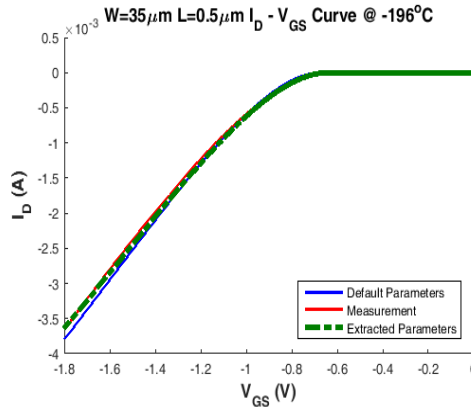
(b)  $W = 10 \mu m, L = 0.18 \mu m$



(c)  $W = 0.24 \mu m, L = 10 \mu m$



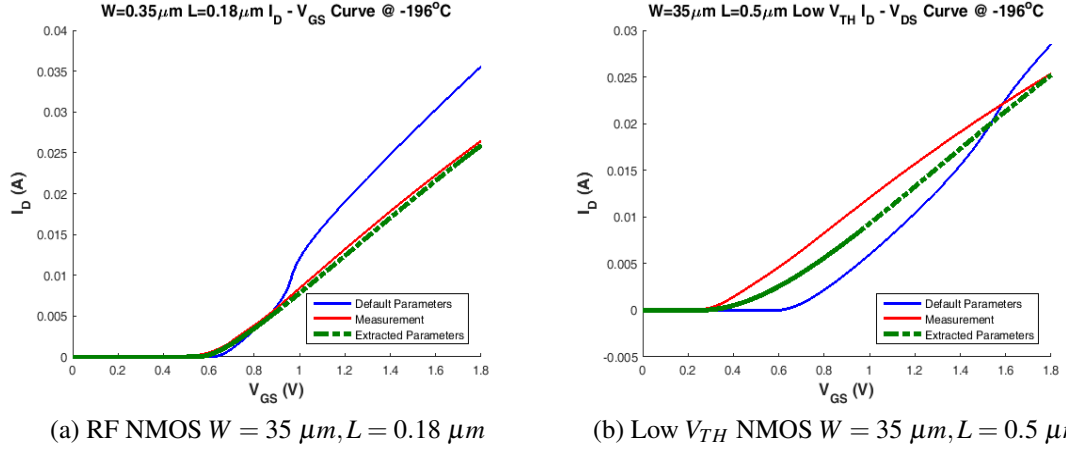
(d)  $W = 10 \mu m, L = 10 \mu m$



(e)  $W = 35 \mu m, L = 0.5 \mu m$

**Figure 3.16** : Comparison of the default model and extracted model of PMOS with measurement results at  $-196^{\circ}C$

Even though the error rates rise when only one parameter set is extracted, they are still significantly lower in regard to the default model. When  $I_D - V_{DS}$  measurements are compared with simulations using the extracted model file, for transistors 1, 2 and 5, error rates of %14.21, %12.34 and %1.25 are acquired, respectively. Conversely, the default model can only yield error rates of %71.1, %48.7 and %99.7 which clearly



(a) RF NMOS  $W = 35 \mu\text{m}, L = 0.18 \mu\text{m}$  (b) Low  $V_{TH}$  NMOS  $W = 35 \mu\text{m}, L = 0.5 \mu\text{m}$   
**Figure 3.17** : Comparison of the default model and extracted model of RF NMOS and Low  $V_{TH}$  NMOS with measurement results at  $-196^\circ\text{C}$

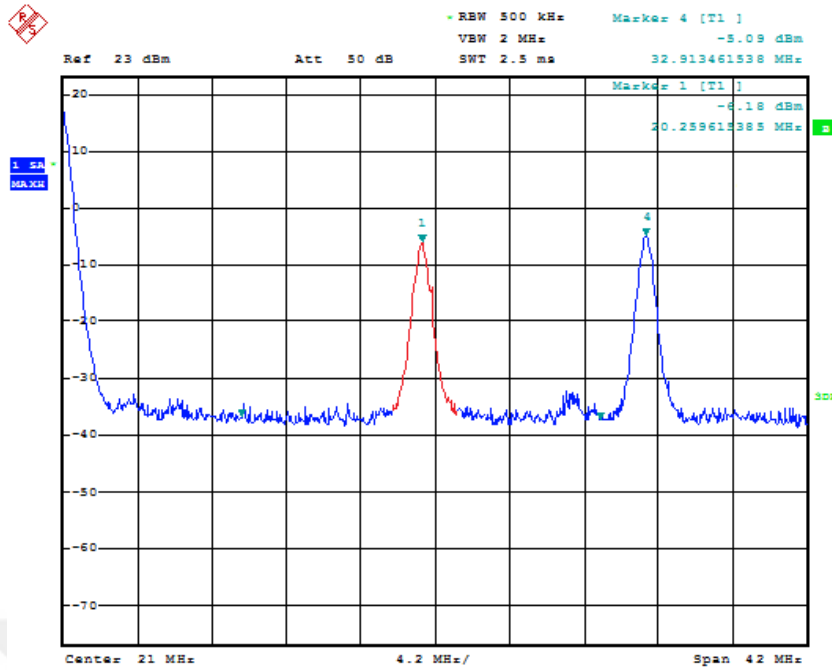
**Table 3.5** : Error rates of  $I_D - V_{DS}$  curves of different parameter sets for each transistor with lower gate biasing at  $-196^\circ\text{C}$

Type	Size(WxL)	$-196^\circ\text{C} @  V_{GS}  = 1.2\text{V}$	
		Def.(%)	Model(%)
NMOS	$0.24 \mu\text{m} \times 0.18 \mu\text{m}$	44.2	1.1
NMOS	$10 \mu\text{m} \times 0.18 \mu\text{m}$	53.8	11.6
NMOS	$0.24 \mu\text{m} \times 10 \mu\text{m}$	29.0	3.2
NMOS	$10 \mu\text{m} \times 10 \mu\text{m}$	74.7	5.9
NMOS	$35 \mu\text{m} \times 0.5 \mu\text{m}$	43.5	8.3
PMOS	$0.24 \mu\text{m} \times 0.18 \mu\text{m}$	30.5	6.5
PMOS	$10 \mu\text{m} \times 0.18 \mu\text{m}$	17.2	12.2
PMOS	$0.24 \mu\text{m} \times 10 \mu\text{m}$	33.3	2.3
PMOS	$10 \mu\text{m} \times 10 \mu\text{m}$	7.4	3.9
PMOS	$35 \mu\text{m} \times 0.5 \mu\text{m}$	8.0	6.2
RF_N	$35 \mu\text{m} \times 0.5 \mu\text{m}$	42.4	1.5

identifies the improvement achieved by the extracted model. Various temperatures, body and gate biases are taken into account and the algorithm with its outputs are proved for its accuracy measurements under LN2(liquid nitrogen).

### 3.2.2.3 Circuit measurements

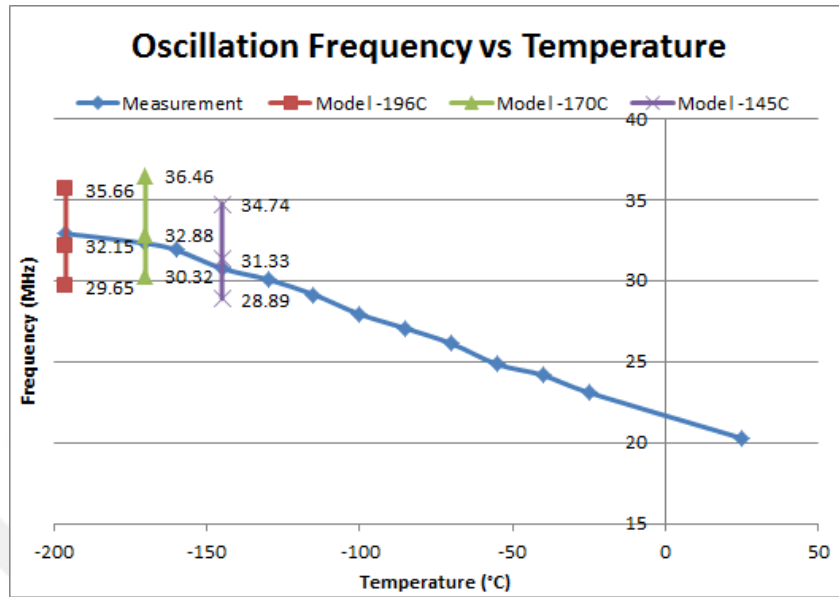
A ring oscillator is considered to demonstrate the model in a typical circuit example and Rohde&Schwarz FSU 20Hz – 26.5GHz spectrum analyzer is used. Measurements have been performed on four different dies at both room temperature and cryogenic conditions. The measured oscillation spectrum of acquired from one of the ring oscillators at  $-196^\circ\text{C}$  is shown in Fig.3.18. The mean of measured oscillation



**Figure 3.18** : Measured spectrum of the ring oscillator at  $-196^{\circ}\text{C}$  (blue) and  $24^{\circ}\text{C}$  (red)

frequencies are 20.67 MHz and 32.65 MHz for  $25^{\circ}\text{C}$  and  $-196^{\circ}\text{C}$  respectively. Simulation and measurement results of 4 different dies are compared in Table 3.6. While the default model results in 38.43% error in simulation-measurement comparison, a single model extracted for all sizes by the proposed methodology can accurately match the measurement results and the error is decreased down to 1.53% as shown in Table 3.6.

Additionally, a single ring oscillator was measured at various temperature from  $24^{\circ}\text{C}$  to  $-196^{\circ}\text{C}$ . All measured oscillation frequencies with temperature sweep are given in Fig. 3.19. The oscillation frequency shows similar result with current change and it is increased linearly with temperature decrease as expected. The standard deviation values at  $-196^{\circ}\text{C}$ ,  $-170^{\circ}\text{C}$  and  $-145^{\circ}\text{C}$  are also given that is calculated considering the measurement variation. The extracted model is verified with a circuit application and the validation of the model is proved at different temperatures and the statistical analysis are given for cryogenic conditions.



**Figure 3.19** : Measured oscillation frequencies of the ring oscillator from  $-196^{\circ}\text{C}$  to  $24^{\circ}\text{C}$  and proposed model results at  $-196^{\circ}\text{C}$ ,  $-170^{\circ}\text{C}$  and  $-145^{\circ}\text{C}$  with  $\pm 3\sigma$  values

**Table 3.6** : Comparison of oscillation frequency for the ring oscillator at nominal and liquid nitrogen temperatures

Results	$25^{\circ}\text{C}$	$-196^{\circ}\text{C}$
Post Layout Sim. (Default)	19.1 MHz	45.2 MHz
Post Layout Sim. (Modeled)	19.1 MHz	32.15 MHz
Measurement (Chip 1)	20.73 MHz	31.9 MHz
Measurement (Chip 2)	21.26 MHz	33.31 MHz
Measurement (Chip 3)	20.46 MHz	32.51 MHz
Measurement (Chip 4)	20.26 MHz	32.91 MHz



#### 4. CONCLUSION

In this thesis, a method has been presented to calibrate the BSIM3 temperature dependency parameters for cryogenic temperatures at which BSIM parameters cannot match the measurement outcomes. Although the algorithm was demonstrated for using 180 nm technology with measurements under liquid nitrogen, it can also be implemented in different device technologies because the method is independent of process parameters. The algorithm developed in this project is based on BSIM3 model and it only needs the target data with the default model file to yield the experimental results using BSIM equations and analytical solution methods. The extracted model parameter set can be called for simulations from any CAD program which supports BSIM3. This methodology can be used in BSIM4 as well because it has same modeling approach. The only need is adapting new equations and parameters to the developed methodology flow. This experimentally verified model on analog circuit design in the sense that it correctly reflects the device characteristics changes in transistors of various sizes. The model has a statistical approach and it includes the impact of process variation at cryogenic conditions. Finally, intermediate temperatures between the  $-196^{\circ}C$  and room temperature has also been considered and a specific model, calibrated at these temperatures are developed. The accuracy of the model derived from single-transistor experiments has been verified using a ring oscillator as well, which confirms its suitability for use in more complex circuit design.





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## **APPENDICES**

### **APPENDIX A.1 : Source Code of Main Function**





## APPENDIX A.1 - Source Code of Main Function

```

1  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% INPUTS %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
2      transistor_no = 2;
3      % No - W(um), L(um) , type
4      % 1 - 0.24 , 0.18 , n
5      % 2 - 10 , 0.18 , n
6      % 3 - 0.24 , 10 , n
7      % 4 - 10 , 10 , n
8      % 5 - 35 , 0.5 , n
9      % 9 - 0.24 , 0.18 , p
10     % 10 - 10 , 0.18 , p
11     % 11 - 0.24 , 10 , p
12     % 12 - 10 , 10 , p
13     % 13 - 35 , 0.5 , p
14     % 15 - 35 , 0.18 , rf-n
15     temp = -196; % measurement temperature
16
17     Wdrawn=10e-06; % transistor width
18     Ldrawn=0.18e-06; % transistor length
19
20     short_ch = 0; % KTIL activation
21     Ldrawn_s = 0.18e-06; % short channel transistor length
22
23     transistor_name = 'n_18'; % name in the model file
24     type = 'n'; % n / p type
25
26     vds_second_bias = 8; % Id-Vds, VGS 8 9 10 11 12 (VGS = 1.8 1.5...
27     % 1.2 0.9 0.6)
28
29     step = 10; % delta iteration
30     maksimum_simulasyon_sayisi = 10; % simulation_limit
31     target_min_error = 0.5;
32
33     % maximum biases
34     if type == 'n'
35         vd = 1.8;
36         vg = 1.8;
37         vs = 0;
38         vb = 0;
39     elseif type == 'p'
40         vd = 0;
41         vg = 0;
42         vs = 1.8;
43         vb = 1.8;
44     end
45 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
46 % ocean file path for each sweep
47     [~,transistor_size] = size(transistor_name);
48     if transistor_size == 4 & (transistor_name == 'n_18' | ...
49         transistor_name == 'p_18')
50         %----- N_18, P_18 -----%
51         ocean_address_n_vds = './ocean_files/ocean_n_vds.ocn';
52         ocean_address_n_vgs = './ocean_files/ocean_n_vgs.ocn';
53         ocean_address_n_vgs_low_vds = ...
54             './ocean_files/ocean_n...vgs_low_vds.ocn';
55         ocean_address_p_vds = './ocean_files/ocean_p_vds.ocn';
56         ocean_address_p_vgs = './ocean_files/ocean_p_vgs.ocn';
57         ocean_address_p_vgs_low_vds = ...
58             './ocean_files/ocean_p_vgs_low_vds.ocn';
59         model_address = '/vlsi/projects/mm180_reg18_v124.mdl.scs';
60
61         file = fopen(model_address);
62         formatSpec = '%s';
63         C = textscan(file, formatSpec);
64         [boyut, ~] = size(C{:});

```

```

65
66 % model parameter location in model file
67 for i=1:boyut
68     k=strfind(C{1}{i}, 'type=');
69     if k==1
70         model_mosfet_type = textscan(C{1}{i}, 'type=%s');
71         model_mosfet_type = model_mosfet_type{1}{1};
72         if type == 'n'
73             if model_mosfet_type=='n'
74                 baslangic = i; %nmos
75             elseif model_mosfet_type=='p'
76                 son = i; %pmos
77             end
78         end
79
80         if type == 'p'
81             if model_mosfet_type=='p'
82                 baslangic = i; %pmos
83                 son = boyut;
84             end
85         end
86     end
87 end
88 fclose(file);
89
90 else % for rf transistor
91     %----- RF -----%
92     ocean_address_n_vds = './ocean_files/ocean_n_vds_rf.ocn';
93     ocean_address_n_vgs = './ocean_files/ocean_n_vgs_rf.ocn';
94     ocean_address_n_vgs_low_vds = ...
95         './ocean_files/ocean_n_vgs_low_vds_rf.ocn';
96     ocean_address_p_vds = './ocean_files/ocean_p_vds_rf.ocn';
97     ocean_address_p_vgs = './ocean_files/ocean_p_vgs_rf.ocn';
98     ocean_address_p_vgs_low_vds = ...
99         './ocean_files/ocean_p_vgs_low_vds_rf.ocn';
100     model_address = './vlsi/projects/mm180_reg18_v124.mdl.scs';
101
102     file = fopen(model_address);
103     formatSpec = '%s';
104     C = textscan(file, formatSpec);
105     [boyut, ~] = size(C{:});
106
107     % RF Transistor model dosyasi
108     n = 1;
109     for i=1:boyut
110         k = strfind(C{1}{i}, transistor_name);
111         if k==1
112             if n==1
113                 baslangic = i;
114                 n = 2;
115             elseif n == 2
116                 son = i;
117             end
118         end
119     end
120 end
121
122 % simulation results of cadence
123 result_address_vgs = './sonuclar/n_vgs.dat';
124 result_address_vgs_low_vds = './sonuclar/n_vgs_low_vds.dat';
125 result_address_vds = './sonuclar/n_vds.dat';
126
127 % iteration parameters
128 ub1_n_max=-10.6730e-18;
129 delta_n_max = 0.2;
130
131 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
132
133 command = 'sed -i -e 's/''%s''/'/%s''/g'' %s';
134 if type == 'n'
135     ocean_address_vds = ocean_address_n_vds;

```



```

136     ocean_address_vgs = ocean_address_n_vgs;
137     ocean_address_low_vds = ocean_address_n_vgs_low_vds;
138
139     elseif type == 'p'
140         ocean_address_vds = ocean_address_p_vds;
141         ocean_address_vgs = ocean_address_p_vgs;
142         ocean_address_low_vds = ocean_address_p_vgs_low_vds;
143     end
144
145     %%%%%%%%%% Algorithm starts here %%%%%%%%%%
146     simulasyon_sayisi=1;
147     level = 1;
148     % level 1 - vbs=0
149     % level 2 - bulk effect
150     % level 3 - vdsat, delta
151     while level <= 3
152         if level == 2
153             if type == 'n'
154                 vb = -0.4; % bulk effect (vbs = -0.4)
155             elseif type == 'p'
156                 vb = 2.2; % bulk effect (vbs = 0.4)
157             end
158         elseif level == 3
159             if type == 'n'
160                 vb = 0;
161             elseif type == 'p'
162                 vb = 1.8;
163             end
164         end
165
166         %%%%%%%%%% Measurement Data Import %%%%%%%%%%
167         if type == 'n'
168             V = 0:0.01:1.8;
169             if (level == 1 || level == 3)
170                 [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] = ...
171                     target_meas_data( transistor_no, 'VGS', 2, 8 );
172                 V_aim_low_vds = V;
173                 I_aim_low_vds = Id_mean_ln2;
174
175                 [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] = ...
176                     target_meas_data( transistor_no, 'VGS', 1, 8 );
177                 V_aim = V;
178                 I_aim = Id_mean_ln2;
179
180                 [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] = ...
181                     target_meas_data( transistor_no, 'VDS', 0, vds_second_bias );
182                 Vds_aim = V;
183                 Ids_aim = Id_mean_ln2;
184             elseif level == 2
185                 [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] = ...
186                     target_meas_data( transistor_no, 'VGS', 2, 12 );
187                 V_aim_low_vds = V;
188                 I_aim_low_vds = Id_mean_ln2;
189                 I_aim_low_vds_vbs = I_aim_low_vds;
190                 % FF = importdata(Id_Vg_Vdmax1_path);
191                 V_aim = FF(:,1);
192                 I_aim = FF(:,2);
193                 [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] = ...
194                     target_meas_data( transistor_no, 'VDS', 4, vds_second_bias );
195                 Vds_aim = V;
196                 Ids_aim = Id_mean_ln2;
197                 Ids_aim_vbs = Ids_aim;
198             end
199         elseif type == 'p'
200             V = 1.8:-0.01:0;
201             if (level == 1 || level == 3)
202                 [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] = ...
203                     target_meas_data( transistor_no, 'VGS', 2, 8 );
204                 V_aim_low_vds = V;
205                 I_aim_low_vds = Id_mean_ln2*-1;
206

```

```

207     [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] =...
208         target_meas_data( transistor_no, 'VGS', 1, 8 );
209     V_aim = V;
210     I_aim = Id_mean_ln2*-1;
211
212     [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] =...
213     target_meas_data( transistor_no, 'VDS', 0, vds_second_bias );
214     Vds_aim = V;
215     Ids_aim = Id_mean_ln2*-1;
216     elseif level == 2
217         [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] =...
218             target_meas_data( transistor_no, 'VGS', 2, 12 );
219         V_aim_low_vds = V;
220         I_aim_low_vds = Id_mean_ln2*-1;
221         I_aim_low_vds_vbs = I_aim_low_vds;
222         % FF = importdata( Id_Vg_Vdmax1_path );
223         % V_aim = FF(:,1) + 1.8;
224         % I_aim = FF(:,2)*-1;
225         [ Id_mean_ln2, Id_3sigma, Id_e3sigma ] =...
226         target_meas_data( transistor_no, 'VDS', 4, vds_second_bias );
227         Vds_aim = V;
228         Ids_aim = Id_mean_ln2*-1;
229         Ids_aim_vbs = Ids_aim;
230     end
231 end
232
233 if level == 1 %% measurement graphs
234     subplot(2,2,1)
235     ax1_I_aim = plot(V_aim,I_aim,'linewidth',2,'color','r');
236
237     subplot(2,2,3)
238     ax2_I_aim = plot(V_aim_low_vds,I_aim_low_vds, ...
239         'linewidth',2,'color','r');
240
241     subplot(2,2,2)
242     ax3_I_aim = plot(Vds_aim,Ids_aim,'linewidth',2, ...
243         'color','r');
244
245     elseif level == 2
246         subplot(2,2,4)
247         ax4_I_aim = plot(Vds_aim,Ids_aim_vbs,'linewidth',2,...
248             'color','r');
249     end
250 drawnow
251 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
252
253
254 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% Input Import / Ocean File %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
255 ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
256     ocean_address_vds);
257 ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
258     ocean_address_vgs);
259 if type == 'n'
260     vd = 0.05;
261     ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
262         ocean_address_low_vds);
263     vd = 1.8;
264 elseif type == 'p'
265     vd = 1.75;
266     ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
267         ocean_address_low_vds);
268     vd = 0;
269 end
270 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% default degerlerde analiz %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
271
272 drawnow
273
274 [ Vds, Ids ] = simulation( ocean_address_vds, result_address_vds );
275 [ V, I ] = simulation( ocean_address_vgs, result_address_vgs );
276 [ V_low_vds, I_low_vds ] = simulation( ocean_address_low_vds,...
277     result_address_vgs_low_vds ); % (ID-VGS @ low VDS)

```

```

278 vth = importdata('./sonuclar/vth.dat');
279 vdsat = importdata('./sonuclar/vdsat.dat');
280 if level ==1
281     Ids_cad_ln2 = Ids;
282     I_cad_ln2 = I;
283
284     plot(V, Ids)
285     plot(V, Ids_aim)
286
287     subplot(2,2,1)
288     ax1_I_cad_ln2 = plot(V, I_cad_ln2, '-');
289
290     subplot(2,2,2)
291     ax3_I_cad_ln2 = plot(Vds, Ids_cad_ln2, '-');
292
293     drawnow
294 end
295
296
297 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% VTH Extraction %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
298 I_aim_low_vds = smooth(I_aim_low_vds);
299
300 if type == 'n'
301     [~, loc]=max(diff(I_aim_low_vds));
302 elseif type == 'p'
303     [~, loc]=max(abs(diff(I_aim_low_vds)));
304 end
305
306 if loc >=3
307     m= (I_aim_low_vds(loc)-I_aim_low_vds(loc-2))/...
308         (V_aim_low_vds(loc)-V_aim_low_vds(loc-2));
309 else
310     m= (I_aim_low_vds(loc)-I_aim_low_vds(loc+2))/...
311         (V_aim_low_vds(loc)-V_aim_low_vds(loc+2));
312 end
313 b = I_aim_low_vds(loc) - m*V_aim_low_vds(loc);
314
315 vth_graph = -b/m; % linear method
316
317 if ~manual_input
318     [~, loc]=max(smooth(transpose(V_aim_low_vds(1:...
319         1:size(V_aim_low_vds,2)-2)), diff(I_aim_low_vds,2)));
320 else
321     [~, loc]=max(smooth(transpose(V_aim_low_vds(1:...
322         size(V_aim_low_vds,1)-2)), diff(I_aim_low_vds,2)));
323 end
324
325 vth_sd = V_aim_low_vds(loc); % second derivative method
326 if type == 'p'
327     vth_sd = 1.8-vth_sd;
328     vth_graph = 1.8-vth_graph;
329 end
330
331 vth_app = vth_sd;
332 if abs(abs(vth_graph)-abs(vth_sd))>0.2
333     vth_app = vth_graph;
334 end
335 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
336 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
337 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
338 error_vds=100;
339 [Ids_boyut, ~] = size(Ids);
340
341 while error_vds>target_min_error || (Ids_aim(Ids_boyut,1)...
342     -Ids(Ids_boyut,1))/Ids(Ids_boyut,1)>0.01
343     %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% VDSAT %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
344
345     [ vdsat_difference ] = vdsat_finding( Vds, Ids, Vds,...
346         Ids_aim );
347
348     %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% Calculations %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

```

349 % Parameters are extracted at this stage
350 if type == 'n'
351     [level, hata, Ids_app] = parametric_calculations_n(...
352 temp, vg, vd, vs, vb, vth, vth_app, Wdrawn, Ldrawn, model_address, ...
353 command, Ids_aim, Ids, I, I_aim, vdsat, vdsat_difference, ...
354 ocean_address_vgs, ocean_address_low_vds, ocean_address_vds, ...
355 result_address_vgs, result_address_vgs_low_vds, result_address_vds, ...
356 ubl_n_max, step, level, baslangic, son, short_ch, type);
357
358 elseif type == 'p'
359     [level, hata, Ids_app] = parametric_calculations_p(...
360 temp, vg, vd, vs, vb, vth, vth_app, Wdrawn, Ldrawn, model_address, ...
361 command, Ids_aim, Ids, I, I_aim, vdsat, vdsat_difference, ...
362 ocean_address_vgs, ocean_address_low_vds, ocean_address_vds, ...
363 result_address_vgs, result_address_vgs_low_vds, result_address_vds, ...
364 ubl_n_max, step, level, baslangic, son, short_ch, type);
365 end
366
367 if hata == 1
368     if level == 1
369         hata_ute = 1;
370     end
371 end
372
373 if short_ch == 1 && level == 1 && simulasyon_sayisi > 2
374     level = 4;
375
376     if type == 'n'
377         FF = importdata(Id_Vg_Vdmin_s_path);
378         V_aim_low_vds_s = FF(:,1);
379         I_aim_low_vds_s = FF(:,2);
380
381     elseif type == 'p'
382         FF = importdata(Id_Vg_Vdmin_s_path);
383         V_aim_low_vds_s = FF(:,1)+1.8;
384         I_aim_low_vds_s = FF(:,2)*-1;
385     end
386
387 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% VTH %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
388 I_aim_low_vds_s = smooth(I_aim_low_vds_s);
389
390 if type == 'n'
391     [~, loc]=max(diff(I_aim_low_vds_s));
392 elseif type == 'p'
393     [~, loc]=max(abs(diff(I_aim_low_vds_s)));
394 end
395
396 if loc >= 3
397     m = (I_aim_low_vds_s(loc)-I_aim_low_vds_s(loc-2))/...
398         (V_aim_low_vds_s(loc)-V_aim_low_vds_s(loc-2));
399 else
400     m = (I_aim_low_vds_s(loc)-I_aim_low_vds_s(loc+2))/...
401         (V_aim_low_vds_s(loc)-V_aim_low_vds_s(loc+2));
402 end
403 b = I_aim_low_vds_s(loc) - m*V_aim_low_vds_s(loc);
404
405 vth_graph = -b/m;
406
407 [~, loc]=max(smooth(V_aim_low_vds_s(1:...
408     size(V_aim_low_vds_s)-2,1), diff(I_aim_low_vds_s,2)));
409 vth_sd = V_aim_low_vds_s(loc);
410 if type == 'p'
411     vth_sd = 1.8-vth_sd;
412     vth_graph = 1.8-vth_graph;
413 end
414
415 vth_app = vth_sd;
416 if abs(abs(vth_graph)-abs(vth_sd))>0.2
417     vth_app = vth_graph;
418 end
419

```

```

420         Ldrawn_old = Ldrawn;
421         Ldrawn = Ldrawn_s;
422
423         %%%%%%%%%%% Input Import / Ocean File %%%%%%%%%%%
424         ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
425             ocean_address_vgs);
426         if type == 'n'
427             vd = 0.05;
428             ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
429                 ocean_address_low_vds);
430             vd = 1.8;
431         elseif type == 'p'
432             vd = 1.75;
433             ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
434                 ocean_address_low_vds);
435             vd = 0;
436         end
437
438         %%%%%%%%%%% Simulations %%%%%%%%%%%
439         [ V_low_vds, I_low_vds ] = simulation( ...
440             ocean_address_low_vds, result_address_vgs_low_vds );
441         [ V, I ] = simulation( ocean_address_vgs, ...
442             result_address_vgs );
443         A = importdata('./sonuclar/vth.dat');
444         vth = A;
445
446
447         %%%%%%%%%%% Calculations %%%%%%%%%%%
448         if type == 'n'
449             [level, hata, Ids_app] = parametric_calculations_n(...
450 temp, vg, vd, vs, vb, vth, vth_app, Wdrawn, Ldrawn, model_address,...
451 command, Ids_aim, Ids, I, I_aim, vdsat, vdsat_difference,...
452 ocean_address_vgs, ocean_address_low_vds, ocean_address_vds,...
453 result_address_vgs, result_address_vgs_low_vds, result_address_vds,...
454 ub1_n_max, step, level, baslangic, son, short_ch, type );
455
456         elseif type == 'p'
457             [level, hata, Ids_app] = parametric_calculations_p(...
458 temp, vg, vd, vs, vb, vth, vth_app, Wdrawn, Ldrawn, model_address,...
459 command, Ids_aim, Ids, I, I_aim, vdsat, vdsat_difference,...
460 ocean_address_vgs, ocean_address_low_vds, ocean_address_vds,...
461 result_address_vgs, result_address_vgs_low_vds, result_address_vds,...
462 ub1_n_max, step, level, baslangic, son, short_ch, type );
463         end
464
465         Ldrawn = Ldrawn_old;
466         level = 1;
467     end
468
469
470     %%%%%%%%%%% Simulations with new parameters %%%%%%%%%%%
471     [ Vds, Ids ] = simulation( ocean_address_vds, ...
472         result_address_vds );
473     [ V_low_vds, I_low_vds ] = simulation( ...
474         ocean_address_low_vds, result_address_vgs_low_vds );
475     [ V, I ] = simulation(ocean_address_vgs, result_address_vgs);
476     A = importdata('./sonuclar/vth.dat');
477     vth = A;
478     A = importdata('./sonuclar/vdsat.dat');
479     vdsat = A;
480     if level == 2
481         Ids_vbs = Ids;
482         I_low_vds_vbs = I_low_vds;
483         I_vbs = I;
484     end
485     %%%%%%%%%%% ERROR %%%%%%%%%%%
486     %%%%%%%%%%% ERROR %%%%%%%%%%%
487     error=0;
488     for i=1:size(I)
489         error = abs(I_aim_low_vds(i)-I_low_vds(i))+error;
490     end

```

```

491         toplam=0;
492         for i=1:size(I)
493             toplam = abs(I_aim_low_vds(i))+toplam;
494         end
495         error_vgs = error/toplam*100 % maksimum error
496
497         error=0;
498         for i=1:size(Ids)
499             error = abs(Ids_aim(i)-Ids(i))+error;
500         end
501         toplam=0;
502         for i=1:size(Ids)
503             toplam = abs(Ids_aim(i))+toplam;
504         end
505         error_vds_new = error/toplam*100 % maksimum error
506
507         if abs(error_vds_new-error_vds) < 0.1
508             break
509         else
510             error_vds = error_vds_new
511         end
512         %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
513
514         simulasyon_sayisi=simulasyon_sayisi+1
515         if level == 1 && simulasyon_sayisi==...
516             maksimum_simulasyon_sayisi
517             break
518         end
519
520         if level == 2 && simulasyon_sayisi==2*...
521             maksimum_simulasyon_sayisi
522             break
523         end
524
525         if level == 3 && simulasyon_sayisi==2*...
526             maksimum_simulasyon_sayisi + 2
527             break
528         end
529         if hata == 3
530             break
531         end
532     end
533
534     %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% Iterations for DELTA %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
535     if level == 3
536         [ delta_n, Vds, Ids ] = delta_iteration(...
537 model_address, baslangic, son, command, step, Ids, Vds, Ids_aim,...
538 Vds_aim, ocean_address_vds, result_address_vds, delta_n_max, ...
539 error_vds, vdsat_difference );
540     end
541
542     level = level + 1
543 end
544 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% Algorithm ends here %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
545
546 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%% Input Import / Ocean File %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
547 ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
548 ocean_address_vds);
549 ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
550 ocean_address_vgs);
551 if type == 'n'
552     vd = 0.05;
553     ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
554 ocean_address_low_vds);
555     vd = 1.8;
556 elseif type == 'p'
557     vd = 1.75;
558     ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn,...
559 ocean_address_low_vds);
560     vd = 0;
561 end

```

```

562
563 %%%%%%%%%%% Last Simulations %%%%%%%%%%%
564 [ Vds, Ids ] = simulation( ocean_address_vds , result_address_vds );
565 [ V_low_vds, I_low_vds ] = simulation( ocean_address_low_vds , ...
566     result_address_vgs_low_vds );
567 [ V, I ] = simulation( ocean_address_vgs , result_address_vgs );
568 A = importdata( './sonuclar/vth.dat' );
569 vth = A;
570
571 if type == 'n'
572     vb = -0.4;
573 elseif type == 'p'
574     vb = 2.2;
575 end
576 ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn, ...
577     ocean_address_vds);
578 ocean_file_edit(temp, vg, vd, vs, vb, Wdrawn, Ldrawn, ...
579     ocean_address_vgs);
580 [ Vds, Ids_vbs ] = simulation( ocean_address_vds , ...
581     result_address_vds );
582 [ V, I_vbs ] = simulation( ocean_address_vgs , ...
583     result_address_vgs );
584 %%%%%%%%%%%

```





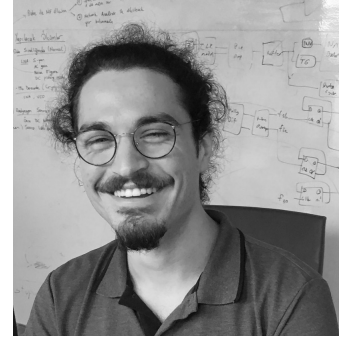


## CURRICULUM VITAE

**Name Surname: Aykut Kabaoğlu**

**Place and Date of Birth: 13.08.1993**

**E-Mail: kabaoglua@itu.edu.tr**



### EDUCATION:

- **B.Sc.:** 2016, Istanbul Technical University, Electrical and Electronics Faculty, Electronics and Communication Engineering
- **M.Sc.:** 2019, Istanbul Technical University, Graduate School of Science Engineering and Technology, Electronics Engineering

### PROFESSIONAL EXPERIENCE AND REWARDS:

- 2018- Co-Founder of Ravinspect Technology.
- 2016-2019 Research Student in VLSI Duran Leblebici Laboratory, Istanbul Technical University
- 2014-2016 Intern in RF Laboratory, Istanbul Technical University

### PUBLICATIONS, PRESENTATIONS AND PATENTS ON THE THESIS:

- Kabaoğlu, A., & Yelten, M. B. (2017, June). A cryogenic modeling methodology of MOSFET IV characteristics in BSIM3. *In 2017 14th International Conference on Synthesis, Modeling, Analysis and Simulation Methods and Applications to Circuit Design (SMACD)* (pp. 1-4). IEEE.
- Kabaoğlu, A., Solmaz, N. Ş., İlik, S., Uzun, Y., & Yelten, M. B. (2019). Statistical MOSFET Modeling Methodology for Cryogenic Conditions. *IEEE Transactions on Electron Devices*, 66(1), 66-72.