

DOKUZ EYLÜL UNIVERSITY
GRADUATE SCHOOL OF NATURAL AND APPLIED
SCIENCES

WATER QUALITY AND WATER BUDGET
ANALYSES IN EYMİR-MOGAN LAKES BASIN

by
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July, 2005
İZMİR

**WATER QUALITY AND WATER BUDGET
ANALYSES IN EYMIR-MOGAN LAKES BASIN**

**A Thesis Submitted to the Graduate School of Natural and Applied Sciences of
Dokuz Eylül University In Partial Fulfillment of the Requirements for the
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Water Resources Program**

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Serkan ÖZEN**

**July, 2005
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M.Sc THESIS EXAMINATION RESULT FORM

We have read the thesis entitled “WATER QUALITY AND WATER BUDGET ANALYSES IN EYMIR-MOGAN LAKES BASIN”, completed by Serkan ÖZEN under supervision of Prof. Dr. Nilgün HARMANCIOĞLU we certify that, in our opinion, it is fully adequate, in scope and in quality, as a thesis for the degree of Master of Science

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There are many complex physical, chemical, and biological interactions within a reservoir. Reservoir or lake models help us understand these interactions. Many models are available for use. In this study, Mogan and Eymir Lakes are modelled by DYRESM-CAEDYM. Water quality and budget for these two lakes are examined, and the results are discussed.

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Serkan ÖZEN
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WATER QUALITY AND WATER BUDGET ANALYSES IN EYMir- MOGAN LAKES BASIN

ABSTRACT

In recent years, water quality and water budget modelling in lakes has become an important element of surface water management. To this end, numerous computer models have been developed. The coupled lake model DYRESM-CAEDYM is one of these models and has hydrodynamic and ecologic components. Provision of accurate predictions without calibration is the most important feature of this model. In this study, Mogan and Eymir Lakes, which are located in Ankara, are simulated over a period of 210 days with DYRESM-CAEDYM. Water quality parameters PO₄ (phosphorus), NO₃ (nitrate), NH₄ (ammonium), and DO (dissolved oxygen), which provide information about the lake ecosystems are simulated. In addition, temperature and salinity variations in both lakes are modelled and compared with observed values.

Keywords : DYRESM-CAEDYM, water quality, computer models, Mogan and Eymir

EYMİR-MOGAN GÖLLER HAVZASINDA SU BÜTÇESİ VE KALİTESİ ANALİZİ

ÖZ

Son yıllarda göllerde su kalitesi ve su bütçesinin modellenmesi, yüzeysel suların yönetiminde önemli bir konu olmuştur. Doğru tahminler elde edebilmek için birçok bilgisayar modeli geliştirilmiştir. Bu modellerden biri olan DYRESM-CAEDYM bileşik göl modeli ekolojik ve hidrodinamik bileşenlere sahiptir. Bu modelin en önemli özelliği kalibrasyon olmadan da isabetli sonuçlar vermesidir. Bu çalışmada, Ankara'da yeralan Mogan ve Eymir gölleri, 210 günlük bir süre boyunca modellenmiştir. Simülasyon için göl ekosistemi hakkında yeterli bilgi sağlayacak olan su kalite parametreleri PO_4 (fosfor), NO_3 (nitrat), NH_4 (amonyum) ve DO (çözünmüş oksijen) seçilmiştir. Bunlara ek olarak sıcaklık ve tuzluluğun değişimlerinde modellenmiş ve gözlenmiş değerlerle karşılaştırılmıştır.

Anahtar Sözcükler : DYRESM-CAEDYM, su kalitesi, bilgisayar modelleri, eymir ve mogan

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CHAPTER ONE

INTRODUCTION

Modern society is contributing, through its industrial, agricultural activities, not only to present global climate trends, but also, more directly, to local environmental degradation. Water resource management is a universal problem that particularly affects populations living in areas where intense industrial and agricultural activities take place, as this can affect the characteristics of surface/subsurface waters in terms of quality and quantity.

Among surface water resources, shallow lakes are important waterbodies throughout the world. Although they contain only a small part of the world's water reserves, they are of paramount importance for biodiversity. Moreover, they provide a number of important functions, such as water supply for drinking, nature, recreation, and fisheries, etc. On the other hand, these systems are highly sensitive to pressures by man: wastewater discharges, overexploitation of fish, eutrophication, and water level regulation. For these reasons, both the ecological conditions and the management of these ecosystems received substantial attention during the last decades. Shallow lakes symposia have been held in Silkeborg, Mikolajki, Berlin and Balatonfüred. The 5th Conference Shallow Lakes 2005 conference will be held from 5 - 9 June , 2005 in Dalfsen, the Netherlands. (Boers, 2005)

For effective water resources management, as well as that for management of shallow lakes, Decision Support Systems-DSS should be developed and executed properly to achieve reliable and confident decisions. DSS comprises the integration of databases, models and Geographical Information Systems (GIS) and is applicable in several developed countries, especially for rivers and lakes to produce more reliable information about water resources.

This study focuses on application of one element of DSS, namely computer-based simulation models, to assess the water quality characteristics of Eymir-Mogan Lakes. Eymir and Mogan lakes are shallow lakes which are under the increasing threat of

domestic, industrial and agricultural pollutants and, hence, of serious eutrophication. The lakes region receives potential impacts from extensive agriculture, recreation, incomplete infrastructure and other anthropogenic activities. The basin, together with the creeks that contribute to Eymir and Mogan Lakes, was declared as a “Special Environmental Protection Zone” in 1990. Since then, several studies have been carried out in the basin to improve its environmental conditions and to develop better management practices for the area. The presented study is different from the previous investigations in the sense that it applies, for the first time, a computer-based simulation model to assess water quality conditions in the lakes. With such a model, distribution of variables such as temperature, salinity and density in lakes can be predicted. When the model is coupled with a water quality component, water quality variables can also be predicted. The model used in this study is called DYRESM-CAEDYM, which permits the prediction of longterm changes of various physiochemical indices.

DYRESM-CAEDYM is a coupled, one dimensional model to predict vertical distributions of variables. DYRESM is the hydrodynamic part, and CAEDYM is biochemical part of the model. DYRESM (Dynamic Reservoir Simulation Model) is a process-oriented model, which means that the model is based on well-defined physical relationships rather than the empirical relationships. Therefore, calibration is not generally required. CAEDYM (the Computational Aquatic Ecosystem Dynamics Model) is an ecological model that represents the biology and chemistry of aquatic ecosystem.

In chapter II, literature survey is provided on both the Eymir-Mogan Lake studies and the applications of the DYRESM-CAEDYM model together with other models used for lake studies. Chapter III discusses the basic characteristics of the simulation model used. Chapter IV presents the case study area and the model application procedures. Chapter V provides the results of the modelling study and Chapter VI discusses the basic conclusion derived.

CHAPTER TWO

LITERATURE SURVEY

2.1. Previous Studies on Eymir-Mogan Lakes Basin

A comprehensive study on Eymir-Mogan Lakes Basin was carried out by Altınbilek (1995), called “Project on Water Resources and Environmental Management Plan for the Gölbaşı Eymir-Mogan Lakes”. The aim of this study was to develop a master plan for Eymir and Mogan Lakes and for the “Special Protection Zone”, and to improve water resources and environmental management in the area. For this, meteorological, hydrological, geological, hydrogeological, bathymetrical, and recreational properties of study site were examined; and solutions and suggestions were provided about supply of drinking water, drainage, pollution prevention, groundwater usage, and flood control.

Karakoç, Erkoç and Katircioğlu (2003) conducted a study about water quality of Lake Eymir and Lake Mogan. In this study, potential impacts from extensive agriculture, recreation, incomplete infrastructure and other human activities were investigated. It was found that the most polluted creeks were Yavrucak, Gölcük and Mogan Canal. In the summer months, there were heavier pollution loads due to lower flow rates and heavier land use, human activities and agricultural activities. It was observed that Eymir Lake had heavy pollution originating from Mogan Lake. It was also found that the pollution loads did not worsen after the study in 1995.

Another study was realized between 17.12.2003 and 28.10.2004 by “Ministry of Environmental and Forestry” and “Environmental Protection Agency” in Mogan Lake. The project was named as “Determination of Pollutants in Creeks Feeding the Mogan Lake and Their Treatment via Natural Treatment Methods”. The aim of the project was the restoration of water quality of the Mogan Lake. At the locations where the main streams enter the lake decontamination zones were built as a result of this project.

Other studies in study site are; “Hydrometeorological characteristics of Eymir-Mogan Lakes Basin” by EIE (2001), “Lymnological Analysis of the Mogan Lake” by DSI(1993), “The role of water level fluctuations and nutrient concentration in determining the macrophyte-dominated clear water stage of Lake Mogan, Turkey” by Beklioglu&Tan (2003), “Macrophyte-dominated clearwater state of Lake Mogan” by Burnak & Beklioglu(2000).

2.2. Lake and Reservoir Models

There are many complex physical, chemical, and biological interactions within a reservoir. To help understand these interactions and better manage a reservoir, simulation models can be used. Computer models can help unravel the complex interactions that occur in lakes between weather, temperature stratification, hydrodynamics, water quality, nutrient cycling and algal growth. Their use can vary from predicting the impact of reducing the water level in a lake to predicting how land-use change or even climate change could influence lake ecology in the long term (NIWA, 2001).

There are many lake and reservoir models developed. Although some of them do not have widespread usage, others have many users around the world. Some of the most familiar one dimensional lake models are DYRESM, BIOLA, MINLAKE, LIMNMOD, GIRL, SALMO, and PROTECH model. There is also a two-dimensional model CE-QUAL-W2, and even a three dimensional model ELCOM. Brief information about these is given below.

BIOLA (Biogeochemical Lake Model), was developed at SMHI for eutrophication studies in Sweden. The model is a one-dimensional (vertical) model that simulates temperature stratification and water quality influenced by weather, inflow and biogeochemical processes in the lake and in the sediments. The model is a biogeochemical lake module coupled to a one-dimensional hydrodynamic model. The model simulates the continuous change of lake stratification and water quality due to weather, inflow, outflow and biogeochemical processes in the lake and in the sediments. ELCOM (Estuary and Lake Computer Model) is a three-dimensional hydrodynamic model, used for predicting the velocity, temperature and salinity

distribution in natural water bodies subjected to external environmental forcing such as wind stress, surface heating or cooling. ELCOM is suited for comparative studies of the summer and winter circulation patterns, spring versus neap tidal cycles, or dispersal conditions under different flow regimes. ELCOM can be run either in isolation for hydrodynamic studies, or coupled with CAEDYM for simulation of biological and chemical processes. PROTECH (Phytoplankton Responses to Environmental Change) simulates the dynamic responses of up to eight species of phytoplankton to environmental variables in lakes and reservoirs. The crude hydrodynamic model in PROTECH is created by using a layer thickness of 10 cm, temperature, wind speed, maximal solar radiation at a particular latitude on a given day of the year, cloud cover, and light extinction. The thermal stratification, mixed layer depth and movement of phytoplankton are defined for each layer for every daily time step (Reynolds et al., 2001). The dynamic ecological model SALMO (Simulation of an Analytical Lake Model) simulates the most important planktic food-web compartments of lakes and reservoirs. The model can be used within scenario analysis applications for decision making and as a research tool (Petzoldt, T 2003).

DYRESM-CAEDYM, is a coupled of a hydrodynamic driver DYRESM (Dynamic Reservoir Simulation Model) with an ecological model CAEDYM (Computational Aquatic Ecosystem Dynamic Model). DYRESM predicts the variation of temperature and salinity with depth and time. CAEDYM can be coupled with DYRESM as the basis for considering water movement and simulating temperature (Antenucci & Imerito, 2002, Herzfeld & Hamilton, 2000).

DYRESM-CAEDYM has some users in Turkey but there are no published articles. Known users are Ali Erturk (ITU), Atilla Akkoyunlu (Bogazici University), Yasar Avsar (Yildiz Technical University). Although there is not many users in Turkey, DYRESM has been used in predicting water quality in many lakes and reservoirs throughout the world. In the U.S., it has recently been applied to San Vicente Reservoir (City of San Diego), Los Vaqueros Reservoir (Contra Costa Water District), and Lake Youngs (Seattle Water Department) (FSI, 2003). Other countries where DYRESM-CAEDYM is used are; Algeria, Argentina, Australia, Bangladesh,

Bermuda, Bolivia, Brazil, Canada, Chile, China, Colombia, Denmark, Egypt, Faroe Island, Finland, France, Germany, Greece, Hong Kong, Hungary, India, Indonesia, Iran, Ireland, Israel, Italy, Japan, Jordan, Kyrgyzstan, Lithuania, Malaysia, Mexico, Nepal, Netherlands, New Zealand, Nigeria, Norway, Poland, Portugal, Russia, Saudi Arabia, Singapore, South Africa, South Korea, Spain , Sri Lanka, Sweden, Switzerland, Taiwan, Tanzania, Thailand, Turkey, Uganda, United Kingdom, United States, Uzbekistan, Venezuela, and Vietnam(CWR, 2005).

DYRESM-CAEDYM was also used for an application in Australia where two inter-connected lakes like Eymir and Mogan were modelled in Australia by Romero et al.(2002) at the Centre of Water Research University of Western Australia.

CHAPTER THREE

DYRESM-CAEDYM MODEL

3.1. General

Experiments and field measurements have long shown that the horizontal temperature variation in reservoirs is almost non-existent. This fact allows a reservoir to be efficiently modeled in a one-dimensional fashion (in the vertical direction). By considering the appropriate physical processes and including a biochemical model, water quality in lakes and reservoirs can be accurately predicted. The computer program, DYRESM-WQ (Dynamic Reservoir Model - Water Quality), is a one-dimensional model that predicts temperature, salinity and water quality in a reservoir by integrating a process-based physical model with a biochemical model. It is owned by the Center for Water Research (FSI, 2003). The Centre for Water Research (CWR) is based at the University of Western Australia in Perth. Its Research Partners include research institutes and universities from around the world that use and develop the Centre's computer models in their efforts to better understand the thermal regimes and ecosystems of lakes (NIWA, 2001).

DYRESM (Dynamic Reservoir Simulation Model) is a one-dimensional hydrodynamics model which can estimate the temperature, salinity and densities vertical distribution in lakes and reservoirs. However the lake or reservoir must satisfy the one-dimensional approximation which will be explained in further sections of this chapter.

DYRESM can be run only for hydrodynamic studies or run coupled with CAEDYM (Computational Aquatic Ecosystem Dynamics Model) which can model chemical and biological processes.

In this model, there is a layer construction. The reservoir can be represented as series of these horizontal layers, which involve no lateral variations (Antenucci & Imerito 2000).

3.2 Model Structure

3.2.1 The Layer Structure

A Lagrangian layer scheme is used in DYRESM. This means that the lake is modelled by a series of horizontal layers of uniform property except the variable thickness. Under the effect of inflow, outflow, rainfall, and evaporation, the stored volume either increase or decreases. As this happens, layer positions change vertically in order to accommodate volume changes.

For given layer thicknesses, the layer volumes and surface areas or for given volumes, the layer thicknesses and surface areas can be found. It is important that layers must be counted from bottom to top (Figure 3.1).

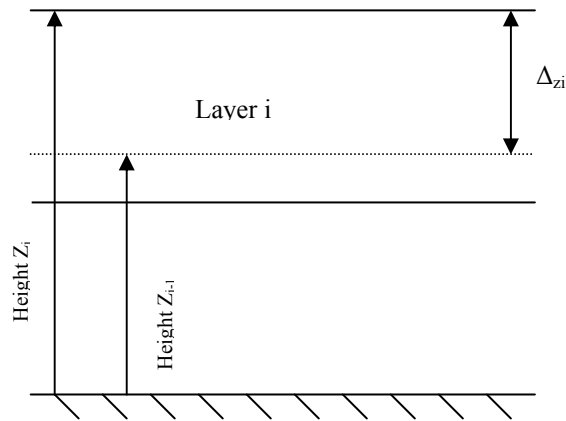


Figure 3.1 Definition of the height and thickness of a layer in DYRESM, defines the height of a layer is defined from the bottom to the top of the reservoir.

The layer structure is based on layers having curved sides. Volumes are calculated cumulatively from the base upwards, with:

$$V(z) = v_{k-1} \left(\frac{z}{z_{k-1}} \right)^{a_k} ; \quad 0 < z_{k-1} < z \leq z_k \quad \forall k \in \{2, 3, \dots, N_S\} \quad (3.1)$$

and

$$A(z) = A_{k-1} \left(\frac{z}{z_{k-1}} \right)^{b_k} ; \quad 0 < z_{k-1} < z \leq z_k \quad \forall k \in \{2,3,\dots,N_S\} \quad (3.2)$$

where

$$a_k = \log \left(\frac{V_k}{V_{k-1}} \right) / \log \left(\frac{z_k}{z_{k-1}} \right) ; \quad \forall k \in \{2,3,\dots,N_S\} \quad (3.3)$$

and

$$b_k = \log \left(\frac{A_k}{A_{k-1}} \right) / \log \left(\frac{z_k}{z_{k-1}} \right) ; \quad \forall k \in \{2,3,\dots,N_S\} \quad (3.4)$$

For the bottom layer, a conical section is used such that

$$A(z) = A_1 \left(\frac{z}{z_1} \right)^2 ; \quad 0 \leq z \leq z_1 \quad (3.5)$$

and hence

$$V(z) = V_1 \left(\frac{z}{z_1} \right)^3 ; \quad 0 \leq z \leq z_1 \quad (3.6)$$

To avoid excessive number of layers, the upper and lower limits must be set on the layer thicknesses and volumes. But, it is important that the lower limit is selected properly so that numerical diffusion problems do not arise through an excessive number of layer amalgamations. If one layer has volume greater than the maximum limit, then this layer is split into parts to create new layers. After that, the layers are

renumbered, and the surface areas are determined. If one layer has a volume smaller than the minimum limit then, this layer is amalgamated with the neighbouring layer of the smallest volume; and then, the layers are renumbered, and the surface areas are determined.

Generally, the density of a solution decreases when temperature increases or the salinity decreases. At 20 °C, freshwater and seawater have densities of 998 kg/m³ and 1030 kg/m³, respectively.

The density of the water (in kgm⁻³) in a layer, given its temperature (°C), salinity (psu), and pressure (in bars) is given by the UNESCO (1981) as an equation of the state for the density of salt water:

$$\rho(T, S, P) = \frac{\rho(T, S, 0)}{\left(1 - \frac{P}{K(T, S, P)}\right)} \quad (3.7)$$

where

$$\rho(T, S, 0) = A + BS + CS^{3/2} + DS^2 \quad (3.8)$$

	A	B	C	D
T ⁰	+999,8425	+8,245*10 ⁻¹	-5,725*10 ⁻³	+4,831*10 ⁻⁴
T ¹	+6,794*10 ⁻²	-4,089*10 ⁻³	+1,022*10 ⁻⁴	
T ²	-9,095*10 ⁻³	7,643*10 ⁻⁵	-1,654*10 ⁻⁶	
T ³	+1,022*10 ⁻⁴	-8,246*10 ⁻⁷		
T ⁴	-1,12*10 ⁻⁶	+5,387*10 ⁻⁹		
T ⁵	+6,536*10 ⁻⁹			

and

$$K(T, S, P) = A + BP + CP^2 \quad (3.9)$$

	<i>A</i>	<i>B</i>	<i>C</i>
T ⁰	19652,21+54675S+7,944* 10 ⁻² S ^{3/2}	3,240+2,284*10 ⁻³ S +1,91075*10 ⁻⁴ S ^{3/2}	8,510*10 ⁻⁵ - 9,935*10 ⁻⁷ S
T ¹	148,421-0,604S + 1,648 * 10 ⁻² S ^{3/2}	1,437*10 ⁻³ - 1,098*10 ⁻⁵ S	-6,123*10 ⁻⁶ + 2,081*10 ⁻⁸ S
T ²	-2,327+1,1*10 ⁻² S - 5,301*10 ⁻⁴ S ^{3/2}	1,161*10 ⁻⁴ - 1,608*10 ⁻⁶ S	5,279*10 ⁻⁸ + 9,710*10 ⁻¹⁰ S
T ³	1,360*10 ⁻² - 6,167*10 ⁻⁵ S	-5,779*10 ⁻⁷	
T ⁴	-5,155*10 ⁻⁵		

Layer stability is checked by comparing the densities of layers. This process starts with the surface layer and continues with the layers below. At this process, the density of current layer is compared with that of the layer below and it is ensured that the density profile is always stable. If the density of current layer is greater than the density of the layer below it, the layers are combined. The properties of the two layers are conserved according to the equations governing constituent conservation, and the new density is determined from the new temperature and salinity. Then, the density of the new layer is compared to the next layer below and the process is continued until the lowest layer is reached.

If two layers are combined, the conservation laws for temperature, salt, energy and momentum can be generalised as

$$C_i^* = \frac{C_i \Delta M_i + C_{i+1} \Delta M_{i+1}}{\Delta M_i + \Delta M_{i+1}} \quad (3.10)$$

where the subscripts refer to layer indices, and *C* is the property being conserved (θ_i , S_i or U_i). For conservation of temperature, the above assumes the specific heat to be constant

3.2.2 Surface Heat, Mass and Momentum Exchange

The surface heat, mass and momentum exchange comprise the primary driving mechanisms for DYRESM. The surface exchanges include heating due to short wave radiation penetration into the lake and the fluxes at the surface due to evaporation, long wave radiation and, wind stress.

Daily or sub-daily meteorological data can be used. Except for shortwave radiation and wind speed, all data are assumed to be uniformly distributed during the day for daily data entrance. The shortwave energy distribution is found by the lake latitude and the time of the year. The wind speed can be either uniformly distributed, or a simple "wind hump" distribution applied. If sub-daily data are entered, all data are uniformly distributed within the input timestep. The sub-daily timestep must be greater than (or equal to) 10 minutes, and less than (or equal to) 3 hours.

Short wave radiation (280nm to 2800nm) is usually measured directly. Long wave radiation (greater than 2800nm) emitted from clouds and atmospheric water vapour can be measured directly or calculated from cloud cover, air temperature and humidity. The reflection coefficient of short wave radiation varies from lake to lake and depends on the angle of the sun, the lake colour and the surface wave state. The data required is shown Table 3.1.

Table 3.1. The data required for determination of the reflection coefficient of shortwave radiation.

Attribute	Type	Unit
Short Wave Radiation	Timestep Average	Wm^{-2}
Long Wave Radiation	Timestep Average	Wm^{-2}
Vapour Pressure of Air	Timestep Average	HPa
Wind Speed	Timestep Average	ms^{-1}
Air Temperature	Timestep Average	$^{\circ}\text{C}$
Rainfall	Timestep Total	M

The approach used in DYRESM is to first calculate the surface energy fluxes; the surface mass fluxes then derived from these energy fluxes.

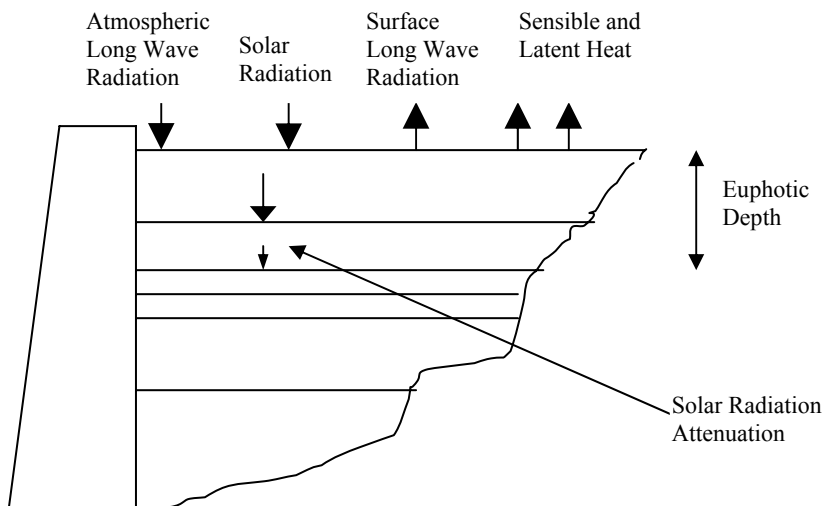


Figure 3.2 Surface energy flux exchanges.

Determination of the solar (shortwave) radiation flux : There are two types of shortwave radiation with respect to wavelength: penetrative (radiation shorter than 700 nm (Photosynthetically Active Radiation, or PAR) , meaning that energy is not only in the surface layer but is also deposited in all layers in the water column) and non-penetrative (all other fluxes).

It is found that 45% of the incoming solar radiation is penetrative (Gates 1966, Jellison and Melack 1993). So, DYRESM takes 55% of the incoming solar radiation as non-penetrative, and the remaining 45% as being distributed throughout the water column. Solar (shortwave) radiation is assumed to have a sinusoidal distribution, centered about midday. If a daily timestep is used, the total energy per unit area for a 24 hour period, $Q_{sw(total)}$, is calculated as 45% of the daily average, and is passed to the thermodynamics routine as:

$$Q_{sw(total)} = \int_{tsr}^{tss} A \sin(\omega t - \beta) dt \quad (3.11)$$

where;

$$w = \frac{\pi}{N_d \gamma} \quad (3.12)$$

where N_d is the duration of a day, t_{SR} is the time of sunrise, t_{SS} is the time of sunset (all in seconds), γ is the day photo fraction (fraction of day with sunlight)

$$\gamma = \frac{t_{ss} - t_{sr}}{N_d} \quad ; \quad 0 \leq t_{sr} < t_{ss} \leq N_d \quad (3.13)$$

and

$$A = \frac{w Q_{sw(\text{toplam})}}{2} \quad (3.14)$$

The day photo fraction is computed, based on the lake latitude and the time of the year. The sunset hour angle is first computed as (Henderson-Sellers, 1986)

$$\cos(h_{ss}) = -\tan \theta \tan \delta \quad (3.15)$$

where θ is the lake latitude, δ is the declination of the sun and computed as (TVA 1972):

$$\delta = 23.45 \left(\frac{\pi}{180} \right) \cos \left[\frac{2\pi}{365} (172 - D) \right] \quad (3.16)$$

with D the day of the year. The day photofraction γ is then calculated (TVA 1972)

$$\gamma = h_{ss} / \pi \quad (3.17)$$

and t_{SR} and t_{SS} are determined by assuming the day is symmetric about midday.

The constraints on t_{SR} and t_{SS} mean that this model is applicable for sub-polar latitudes only. Furthermore, the solar altitude at sunrise and sunset is assumed to be zero. The term β (radians) is a phase shift to ensure the shortwave radiation curve is symmetrical about midday:

$$\beta = \frac{1}{2} \left(\frac{1}{\gamma} - 1 \right) \pi \quad (3.18)$$

Hence the energy deposited per unit area between the times of t_1 and t_2 ($t_{sr} \leq t_1 < t_2 \leq t_{ss}$) is given by:

$$Q_{sw(toplam)}(t_1, t_2) = A \int_{t_1}^{t_2} \sin(\omega t - \beta) dt \quad (3.19)$$

and finally by;

$$Q_{sw(toplam)}(t_1, t_2) = \frac{1}{2} Q_{sw(toplam)}(\cos(\omega t_1 - \beta) - \cos(\omega t_2 - \beta)) \quad (3.20)$$

For sub-daily meteorological input data, the value of shortwave radiation for a timestep is simply taken from the input data file. Once again, 55% is absorbed in the surface layer, with 45% being distributed according to the Beer-Lambert law.

Now, we consider the effect of the albedo of the water surface on the penetration of short-wave radiation. We define

$$Q_{sw}(t_1, t_2) = (1 - r_a^{sw}) Q_{sw(toplam)}(t_1, t_2) \quad (3.21)$$

where

$$r_a^{(sw)} = \bar{R}_a^{(sw)} + a^{(sw)} \sin\left(\frac{2\pi d}{D} - \frac{D}{2}\right); \quad \text{South Hemisphere} \quad (3.22)$$

$$r_a^{(sw)} = \bar{R}_a^{(sw)} \quad ; \quad \text{Equator} \quad (3.23)$$

$$r_a^{(sw)} = \bar{R}_a^{(sw)} + a^{(sw)} \sin\left(\frac{2\pi d}{D} + \frac{D}{2}\right); \quad \text{North Hemisphere} \quad (3.24)$$

with $\bar{R}_a^{(sw)} = 0.08$, $a^{(sw)} = 0.02$, D the standard number of days in a year (365) and d is the day number in the year; (1, 2, ...,D)

Short-wave radiation penetrates according to the Beer-Lambert law, such that:

$$Q(x) = Q_{sw}(t_1, t_2) e^{-\eta_A x} \quad (3.25)$$

where x is the depth below the water surface (measured down from the surface of the reservoir) and η_A the attenuation coefficient.

Thus, the shortwave energy per unit area entering layer j through its upper face is

$$\Delta Q_j = Q_j - Q_{j-1} \quad (3.26)$$

or

$$\Delta Q_j = Q_j (1 - e^{-\eta_{A_j} \Delta z_j}) \quad (3.27)$$

where η_{A_j} is the attenuation coefficient for the j_{th} layer, of thickness Δz_j , and

$$\Delta z_j = z_j - z_{j-1}; \quad (z_0=0, z_N=H).$$

For heating purposes, it is assumed that all of the ΔQ_j 's are converted to heat. If $\Delta Q_j > 0$, heat is deposited, and if $\Delta Q_j < 0$, heat is removed from layer j .

Determination of long wave energy flux : There are three methods to calculate long wave radiation and one of them is chosen according to the available data. These three methods are:

1. Incident long wave radiation

For daily data, the incident long wave radiation over a timestep is:

$$Q_{lw(incident)} = \dot{Q}_{lw(incident)} \Delta t \quad (3.28)$$

where $\dot{Q}_{lw(incident)}$ is the average long wave radiative power density for the day. For sub-daily data, the incident longwave radiation over a timestep equals that in the inputfile. The long wave radiation penetrating the water surface is then

$$Q_{lw} = (1 - r_a^{lw}) Q_{lw(incident)} \quad (3.29)$$

where $r_a^{(lw)}$ is the albedo for long wave radiation, which is taken as a constant = 0.03 (Henderson-Sellers 1986)

Long wave radiation emitted from the water surface is given by (TVA 1972)

$$Q_{lw(emitted)} = \varepsilon_w \sigma T_w^4 \quad (3.30)$$

where ε_w is the emissivity of the water surface (=0.96), σ is the Stefan-Boltzmann constant ($\sigma = 5.6697 \times 10^{-8} \text{ Wm}^{-2}\text{K}^{-4}$), and T_w is the absolute temperature of the water surface.

The nett longwave radiation energy density deposited into the surface layer for the period Δt is therefore:

$$Q_{lw} = (1 - r_a^{lw}) Q_{lw(incident)} - \varepsilon_w \sigma T_u^4 \quad (3.31)$$

2. Nett long wave radiation

For daily data, the incident long wave radiation over a timestep is

$$Q_{lw(net)} = \dot{Q}_{lw(net)} \Delta t \quad (3.32)$$

For sub-daily data, the incident long wave radiation over a timestep equals that in the input file. The long wave radiation energy density deposited into the surface layer for the period Δt is therefore:

$$Q_{lw} = (1 - r_a^{lw}) Q_{lw(net)} \quad (3.33)$$

3. Cloud cover

Long wave radiation can also be estimated from atmospheric conditions, using cloud cover fraction.

The Nett long wave radiation energy density incident on the water surface can be estimated as:

$$Q_{lw(rad)} = (1 - r_a^{lw}) Q_{lw(air)} \quad (3.34)$$

where (TVA 1972, Fischer et al.1979)

$$Q_{lw(air)} = (1 + 0.17C^2) \varepsilon_a (T_a) \sigma T_a^4 \quad (3.35)$$

with the subscript a referring to properties of the air. Swinbank (1963) showed that

$$\varepsilon_a(T_a) = C_E T_a^2 \quad (3.36)$$

where $C_E = 9.37 \times 10^{-6} K^{-2}$. As previously, the long wave emitted is

$$Q_{lw(emitted)} = \varepsilon_w \sigma T_w^4 \quad (3.37)$$

The nett long wave radiation is therefore

$$Q_{lw} = (1 - r_a^{(lw)})(1 + 0.17C^2)\varepsilon_a(T_a)\sigma T_a^4 - \varepsilon_w \sigma T_w^4 \quad (3.38)$$

For the period Δt , the sensible heat loss from the surface can be written as (Fischer et al. 1979):

$$Q_{sh} = C_s \rho_A C_P U_a (T_a - T) \Delta t \quad (3.39)$$

where C_S is the sensible heat transfer coefficient for wind speed at 10 m reference height above the water surface ($= 1.3 \times 10^{-3}$), ρ_A the density of air (kg m^{-3}), C_P the specific heat of air at constant pressure ($= 1003 \text{ J kg}^{-1} \text{K}^{-1}$), U_a is the wind speed at the 'standard' reference height 10 m (m s^{-1}) and temperatures either both in Celsius or both in Kelvin.

The evaporative heat flux is given by (Fischer et al. 1979) as:

$$Q_{th} = \min \left[0, \frac{0.622}{P} C_l \rho_a L_E U_a (e_a - e_s(T_s)) \Delta t \right] \quad (3.40)$$

where P is the atmospheric pressure in hectopascals, C_L is the latent heat transfer coefficient ($= 1.3 \times 10^{-3}$) for wind speed at the reference height of 10 m, ρ_A the density of air in kg m^{-3} , L_E the latent heat of evaporation of water ($= 2.453 \times 10^6 \text{ J kg}^{-1}$), U_a is the wind speed (ms^{-1}) at the reference height of 10 m, e_a the vapour pressure

of the air, and e_s the saturation vapour pressure at the water surface temperature T_s ; both vapour pressures are measured in hectopascals. The condition $Q_{lh} < 0$ is so that no condensation effects are considered.

The saturated vapour pressure e_s is calculated via the *Magnus-Tetens* formula (TVA 1972):

$$e_s(T_s) = \exp \left[2.3026 \left(\frac{7.5T_s}{T_s + 237.3} + 0.7858 \right) \right] \quad (3.41)$$

where T_s is in degrees Celsius and e_s is in hectopascals.

Thus, the total non-penetrative energy density deposited in the surface layer during the period Δt is given by:

$$Q_{non-pen} = Q_{lw} + Q_{sh} + Q_{lh} \quad (3.42)$$

The change in mass in the surface layer (layer number N) due to latent heat flux is calculated as:

$$\Delta M_N^{(lh)} = -\frac{Q_{lh} A_N}{L_V} \quad (3.43)$$

where A_N is the surface area of the surface layer and L_V is the latent heat of vaporisation for water.

It is assumed that the properties of the rain are the same as that of the surface layer. For daily data, the rainfall input for each timestep is:

$$r_h = R_h \frac{\Delta t}{N_d} \quad (3.44)$$

where R_h is the daily total rainfall height. For sub-daily data, the rainfall over a timestep equals that in the input file. The change in surface layer mass is:

$$\Delta M_N^{(rain)} = \rho_N A_N r_h \quad (3.45)$$

The total mass change of the surface layer for the period Δt is

$$\Delta M_N = \Delta M_N^{(lh)} + \Delta M_N^{(rain)} \quad (3.46)$$

In the current model, the change is due to evaporation and precipitation of pure water.

For daily meteorological data, the wind input into DYRESM is a daily average of the wind speed; and for sub-daily data, the wind speed for the timestep equals that in the input file.

A critical wind speed U_{crit} is used in the model, above which the wind is considered to drive motion in the surface layer. This value is set to 3 ms⁻¹ in DYRESM.

When the wind speed exceeds the critical value ($U_a > U_{crit}$), then the momentum exchange begins. Before this, the velocities in the layers *are* set to zero for all layers. After the start of the wind, the velocity in the surface layer U_N is calculated as (Fischer et al., 1979):

$$U_N = \frac{u_*^2}{\Delta z_N} \Delta t \quad (3.47)$$

The shear velocity u_* is calculated from the wind speed by (Fischer et al., 1979)

$$u_* = \left(\frac{C_D \rho_A}{\rho_N} \right)^{1/2} U_a \quad (3.48)$$

where $C_D = 1.3 \cdot 10^{-3}$, ρ_N is the density of the surface layer, A_N the area of the surface layer, $\rho_a = 1.2 \text{ kg m}^{-3}$ (the density of air) and U_a is the wind velocity at a reference height of 10 metres.

For subsequent times, the velocity in the surface layer is:

$$U_N(1 + \Delta t) = U_N(t) + \frac{u_*}{\Delta z_N} \Delta t \quad (3.49)$$

This continues until T_{sp} after the wind has increased above the critical value. If the time T_{sp} is reached and the wind speed is still above the critical value, the layer speeds are set to zero, and the algorithm starts as if for a new wind event. If the wind speed drops below the critical value before the shear period is over, the layer speeds continue to build up above until T_{sp} is reached. It is possible for the input wind speed U_a to be above the critical value. In this case, the wind will always put momentum into the surface layer.

The upper bound on the shear period is:

$$T_{\max(sp)} = \min(T_{\text{limit}}, T_{\text{cor}}) \quad (3.50)$$

where T_{cor} is the period based on the Coriolis effect:

$$T_{\text{cor}} = \frac{N_d}{\sin|\theta|} \quad (3.51)$$

where θ is the latitude, N_d the number of seconds in a day, and T_{limit} the maximum allowable limit for the shear period in the model, which is currently set to seven days.

The shear period used in the model is defined as:

$$T_{sp} = \min\left(\frac{T_i}{4}, T_{\max,sp}\right) \quad (3.52)$$

where T_i is the internal seiche period and can be found as:

$$T_i = \frac{L_N}{2c} \quad (3.53)$$

where L_N is the basin length scale ($\equiv A_N^{1/2}$), and c is the phase speed of the uninodal seiche (Fischer et al. 1979):

$$c = \left[\frac{g}{\rho_{hypo}} (\rho_{hypo} - \rho_{epi}) \left(\frac{\Delta z_{epi} \Delta z_{hypo}}{\Delta z_{epi} + \Delta z_{hypo}} \right) \right]^{1/2} \quad (3.54)$$

where g is the gravitational constant, *epi* refers to the epilimnion, *hypo* to the hypolimnion, ρ is the volume-averaged layer density, and Δz is the layer thickness.

Sometimes when modelling deep lakes, in order not to have too many layers, the user may be forced to set the maximum layer size to a large allowable thickness. The surface layer may then be too thick to allow accurate thermodynamic calculations to be made for the surface waters.

To ensure accurate surface layer thermodynamics with large maximum layer thicknesses, DYRESM re-grids the top part of the water body to ensure that this part of the water column has a high enough resolution to enable 'good' thermodynamic calculations to be made. This re-gridding of surface layers takes place before the distribution of energy into the water body occurs.

One factor known to cause variability in the heat and momentum transfer described above is air column stability and water roughness (Imberger and Patterson 1990). This has the effect of altering the exchange coefficients C_S , C_L and C_D .

If the meteorological sensors are located within the internal boundary layer over the surface of the lake, and data are collected at sub-daily intervals, it is appropriate to consider the effect of air column stability on surface exchange. DYRESM uses the iterative procedure of Hicks (1975) to compute these values, as described in Imberger and Patterson (1990).

3.2.3. *The Surface Mixing Model*

Three mechanisms are available

1. stirring : where energy from the wind stress is applied to the surface layer;
2. convective overturn : where energy is released from the decrease in potential energy resulting from dense water falling to a lower level; and
3. shear : where kinetic energy is transferred from upper to the lower layers in the water column.

The surface mixed layer model uses simple energy arguments to mix the water column based on the kinetic and potential energy available. Mixing is done by conserving mass and momentum on a layer-by-layer basis, starting from the free surface. The method is to compute the energy available for mixing two layers with the energy required to mix the two layers. If there is sufficient energy, the layers are mixed. Any excess energy is then available for mixing subsequent deeper layers. When there is not enough energy available to mix further layers, mixing stops. Any remaining mixing energy is carried over for mixing in the next time step.

The sign convention for the model is such that if $E_i^{(req)} < 0$ (that is the energy required to mix layer i and layer $i-1$ is negative); then, energy is released during the mixing. If $E_i^{(req)} > 0$ energy is required for the mixing. At all times, the energy available to mix, $E^{(avail)}$, must be non-negative.

The change in the potential and kinetic energy for a pair of layers mixing is:

$$\Delta P_i = g \left[(M_1 + M_2) \zeta_{i-1}^* - (M_i \zeta_i + M_{i-1} \zeta_{i-1}) \right] \quad (3.55)$$

$$\Delta K_i = -\frac{1}{2} \frac{M_i M_{i-1}}{M_i + M_{i-1}} (U_i - U_{i-1})^2 \quad (3.56)$$

where $\Delta X \equiv X_{final} - X_{initial}$ for some parameter X, and N indexes the surface layer. M_i as the mass of layer i , U_i the characteristic layer speed, ΔP_i the potential energy change, ΔK_i the kinetic energy change and z_i the height of the centre of mass of layer i . The superscript $*$ indicates the attribute measured after a layer pair have been (notionally) mixed. Also, layers are not re-indexed after mixing in the formalism used here. Also note that $\Delta K_i \leq 0$.

Thus, the energy required to mix the two layers is

$$E_i^{(req)} = g \left[(M_1 + M_2) \zeta_{i-1}^* - (M_i \zeta_i + M_{i-1} \zeta_{i-1}) \right] - \frac{1}{2} \frac{M_i M_{i-1}}{M_{i-1}^*} (U_i - U_{i-1})^2 \quad (3.57)$$

where

$$M_{i-1}^* = M_i + M_{i-1} \quad (3.58)$$

is the mass of the new layer after mixing the two previous layers.

In the surface layer, the energy available to mix is $E^{(stir)}$, that is the stirring energy due to the wind, which is introduced only into the surface layer, and is given for a time step Δt by (Imberger and Patterson, 1981)

$$E^{(stir)} = \eta_s \rho_N A_N u_*^3 \Delta t \quad (3.59)$$

If $\Delta K_i \leq 0$, energy is released (or at least not required for kinetic energy change) for mixing. An efficiency factor η_K must be incorporated. Similarly, if $\Delta P_i < 0$, an efficiency factor η_P must be incorporated. If $\Delta P_i \geq 0$, then energy is required to mix; in this case, the efficiency factor is unity as all of the energy required to mix must be input. Hence,

$$E_i^{(req)} = \begin{cases} \eta_K \Delta K_i + \eta_P \Delta P_i, & \Delta P_i < 0 \\ \eta_K \Delta K_i + \Delta P_i, & \Delta P_i \geq 0 \end{cases} \quad (3.60)$$

For each time step, $E^{(stir)}$ is calculated and added to any energy carried over from the previous time step to give $E^{(avail)}$. If:

$$E_N^{(avail)} \geq E_N^{(req)} \quad (3.61)$$

then layer N and layer $N-1$ mix, and mixing is terminated. Any energy left over from this mixing event stays with $E^{(avail)}$, and is compared with $\Delta E_{N-1}^{(req)}$ to determine whether to mix layers $N-1$ and $N-2$. This continues until $E_i^{(avail)} < E_i^{(req)}$, at which point mixing ceases for this time step. Any energy in is carried over into the next time step.

After mixing has taken place, epilimnion and hypolimnion heights and densities are stored for possible use in the next time step, for use in the calculation of the shear period. The epilimnion height and density values are those of the newly mixed and deepened surface layer. The hypolimnion height and density values are taken to be those of the layer immediately below the newly mixed surface layer.

If water quality is to be simulated using CAEDYM, bottom stress magnitudes need to be calculated and then passed to the CAEDYM algorithms for resuspension. This requires that epilimnion and hypolimnion water speeds be determined, U_E and

U_H respectively. From the mixing just completed, a value for U_E is available and is equal to U_N , which is the velocity of the surface layer.

The velocity in the hypolimnion is calculated by

$$U_H = \begin{cases} \frac{U_E h_E}{h_H}, & h_E < h_H \\ U_E, & h_E \geq h_H \end{cases} \quad (3.62)$$

where h_H and h_E are the thicknesses of the hypolimnion and epilimnion, respectively. The first condition is obtained from the conservation of volume in a rectangular basin, with the second condition taken so as to avoid high unrealistic values for U_H when the mixed layer is the dominant fraction of the water column.

The magnitudes of the bottom stress for the epilimnion and hypolimnion can now be directly calculated:

$$\tau_E = C_{D,dip} \rho_E U_E^2 \quad (3.63)$$

$$\tau_H = C_{D,dip} \rho_H U_H^2 \quad (3.64)$$

where $C_{D,bottom}$ is the bottom drag coefficient.

3.2.4 Inflow Dynamics

Surface flows due to stream flows and subsurface flows due to groundwater are available in DYRESM. Subsurface inflows can be buoyant or dense from the ambient water so that there are different algorithms for these situations. Surface inflow algorithm and the case of dense algorithm are the same.

3.2.4.1 Surface Inflow

The surface inflow process may be divided into three stages. As a stream enters the lake, it will push the stagnant water ahead of itself until buoyancy forces, due to the density differences which may be present, have become sufficient to arrest the flow. At this point, the flow either floats over the reservoir surface if the inflow is lighter than the lake water, or it plunges beneath the reservoir water if it is heavier. If the entrance point to the reservoir is a well defined drowned river valley, then the side of the valley will confine the flow, and a plunge line will be visible across the reservoir at which point the river water submerges uniformly and travels down the channel in a one dimensional fashion (Figure 3.3).

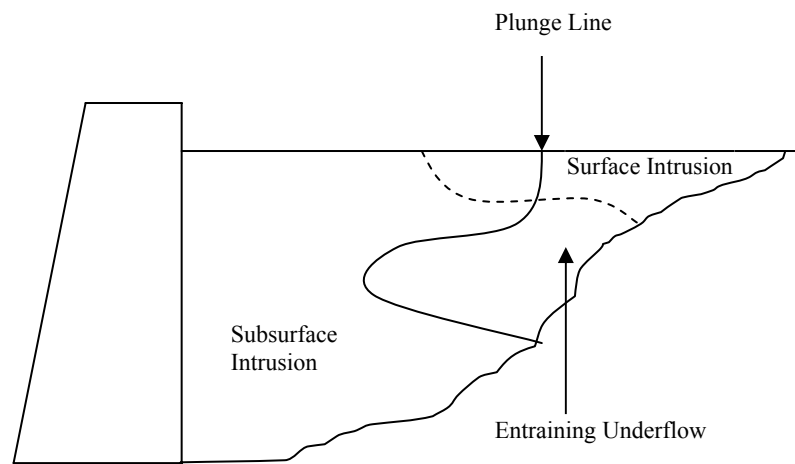


Figure 3.3 Possible river inflow patterns.

For all inflows, the values of the drag coefficient of the river bed C_D , the slope angle of the inflow ϕ , the stream half angle α and the entrainment coefficient constant ε are read in. The entrainment coefficient is given by (Dallimore et al. 2001)

$$E = \frac{C_K C_D^{3/2} + C_S}{R_{in} + 10(C_K C_D^{3/2} + C_S)} \quad (3.65)$$

where C_D is the drag coefficient, C_K and C_S are shape parameters and are fixed at 2,2 and 0,0001 respectively, R_{in} is the bulk Richardson number of the inflow, and is given by (Fischer et al. 1979)

$$R_{in} = \frac{4E + 5C_D / \sin \alpha}{5 \tan \varphi - \frac{8}{3} E} \quad (3.66)$$

Equations above are solved once simultaneously for each inflow at the start of the simulation to give the parameters E and R_{in} for the remainder of the simulation.

Once the inflowing river has negotiated the plunge line, it will continue to flow down the river channel, entraining reservoir water as it moves towards the dam wall. The downflow time may be several days and is further complicated by the entrainment of lake water into the inflowing volume during this downflow process.

At the start of the plunge into the lake, the initial thickness of the inflow, h_0 , is given by:

$$h_0 = \left[\frac{2\dot{Q}_{alq}^2 R_{in}}{g' \tan^2 \alpha} \right]^{1/5} \quad (3.67)$$

where

$$g' = \frac{\rho_{inf low} - \rho_{surface}}{\rho_{inf low}} g \quad (3.68)$$

is the reduced gravity, \dot{Q}_{alq} is the volume flow rate of inflow for the day (m^3s^{-1}) and alq denotes the inflow aliquot for the day.

As the aliquot downflows, it entrains water from each layer it passes through, thus changing the aliquot's properties. The amount of water entrained from a layer into the

downflowing aliquot is determined by the aliquot's frontal thickness and current volume. The increase ΔQ_{alq} in the underflow aliquot volume Q_{alq} is given by the conservation of volume (Imberger and Patterson 1981):

$$\Delta Q_{alq} = Q_{alq} \left[\left(\frac{h}{h_{prev}} \right)^{5/3} - 1 \right] \quad (3.69)$$

where h_{prev} is the frontal thickness for the previous layer, and h the frontal thickness for the current layer after entrainment. The height after entrainment h is given by (assuming a triangular cross section where $a = h_2 \tan \alpha$) (Fischer et al. 1979)

$$h = 1.2E_s + h_0 \quad (3.70)$$

where s is the slope distance from the surface (Figure 3.4).

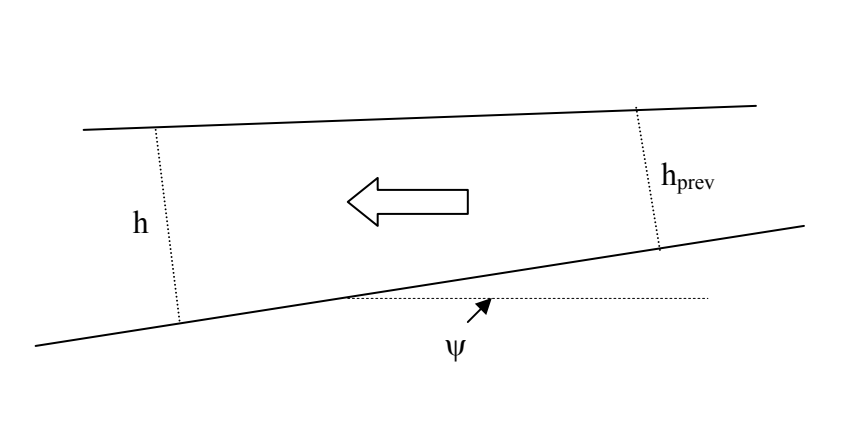


Figure 3.4 Schematic diagram of downflow aliquot

The process of entrainment is repeated for each layer until the aliquot reaches a position in the water body of neutral buoyancy (or the lake bottom), at which point a layer is created in the water body and filled with the aliquot.

The entrance of the river inflow into the reservoir is modeled by the insertion of a volume into a number of existing layers at the appropriate height. If the layer

volumes become excessive, new layers are formed. The increased volume of these layers causes those above to move upwards, decreasing their thickness in accordance with the given volume-depth relationship, to accommodate the volume increase.

The inflow properties of volume Q , temperature T , salinity S , and density ρ are initialised to the corresponding river values. The inflow density ρ is then computed using the UNESCO equation of state as defined before. The inflow density is then compared with the density of the surface layer.

If $\rho_{inflow} \leq \rho_{surface}$, then the total volume is added to the top layer, a new surface level and properties are computed, and the control is returned to the main program.

If $\rho_{inflow} > \rho_{surface}$, then underflow occurs and entrainment calculations are necessary.

The next step is to calculate ΔQ for each inflow. The entrainment from the layers adjacent to the underflow is computed, and this quantity of water is added to the inflow volume Q . The properties are adjusted, and the density compared with the next lowest layer. If the inflow density is smaller, a new layer is created and filled with the inflow aliquot. If not, the process is repeated until the particular inflow has reached its neutrally buoyant level or the bottom is reached. Each inflow is routed to its neutrally buoyant level instantaneously.

And finally insertion comes. If an inflow has reached its level of neutral buoyancy, it is inserted instantaneously as a new layer at that height. The layer structure is then checked for layer amalgamation, based on layer limits set for the simulation.

3.2.4.2 Subsurface inflow

As explained before, subsurface inflows can be buoyant or dense compared to the ambient water. If it is dense than the surface inflow the model is applicable. For a buoyant subsurface inflow, the flow is modelled as a simple, single-phase plume with circular cross-section. When the upwards buoyancy flux due to the density becomes zero due to the entrained ambient water, the plume inserts.

The plume is initialised by first computing the upwards buoyancy flux due to the density difference between the inflowing aliquot and the ambient fluid at the height of the inflow, as (Fischer et al. 1979) described:

$$B_i = g \left(\frac{\rho_i - \rho_{inf}}{\rho_i} \right) Q_{inf} \quad (3.71)$$

where Q_{inf} is the inflow flow rate (m^3s^{-1}), ρ_{inf} is the density of the inflowing water and ρ_i is the ambient density of layer i , at the height of the inflow.

The flow rate of the plume (inflow plus entrained water) is computed as (Fischer et al. 1979):

$$Q_p = \alpha \frac{6\pi}{5} b_1 L_R B^{1/3} (z_i - z_{inf})^{5/3} + Q_{inf} \quad (3.72)$$

where B is the buoyancy flux (m^4s^{-3}), z_i is the layer height, z_{inf} is the height of the inflow, b_1 is a constant ($=4.7$) (Fischer et al. 1979), L_R is the plume aspect ratio (plume radius to plume length, assumed to be a constant of 0.1), and α is an entrainment coefficient. This value has been found experimentally to be 0.083.

The flow rate of the entrained volume in layer i is calculated as:

$$Q_p = \alpha \frac{6\pi}{5} b_1 L_R B^{1/3} (z_i - z_{i-1})^{5/3} + Q_{p-1} \quad (3.73)$$

where the buoyancy flux now accounts for the entrained water:

$$B_i = g \left(\frac{\rho_i - \rho_p}{\rho_i} \right) Q_p \quad (3.74)$$

When the buoyancy flux B becomes zero or negative, or the plume reaches the water surface, the entrained water is entrained instantaneously into the current layer. For the case of the plume reaching the surface, a new layer is created on the surface of the reservoir containing only the plume water.

3.2.5 Outflow Dynamics

The term 'outflow' refers to the combination of withdrawals and overflow. For each outlet, the following algorithm is executed.

1. The level of the outlet is determined and the required quantity Q is extracted from the layer adjacent to this outlet.
2. If Q exceeds the volume of this layer, then water is taken from successive layers above the outlet until the required volume Q is removed from the water column
3. The layer structure is re-determined after each layer has been altered.

All water above the crest height is removed from the top of the water body. If there is initially more than one layer above the crest height, then all layers above crest height are removed and a proportion of the remaining layer is removed such that the surface height of the resulting water body is equal to the crest height.

The water properties (*e.g.*, temperature, DO, FE) which are selected by the user to be output during the simulation, are output not only for the water column but also for each withdrawal and overflow 'device' (*i.e.*, an aliquot of water for each time step

and for each device). For each outflow aliquot, the volume is written to the program output as well as the selected water properties. If water from more than one layer is required for an aliquot, then the resulting aliquot properties are the averaged values for each property.

3.2.6 Hypolimnion Mixing

The mixed layer algorithm allows the depth of the thermocline to be calculated. Below the thermocline are the waters that comprise the hypolimnion. The density gradient in the hypolimnion, although weak, has a stabilising effect, and as a result, the vertical mixing in the hypolimnion is small.

The mixing mechanisms that occur in the hypolimnion of lakes can be categorised into three broad groups (Imberger and Patterson 1981). Firstly, internal wave interactions lead, under the right conditions, to a growth of one wavelength at the expense of others until breaking occurs. Secondly, the local shear may be raised, by combining of long and short internal waves, to such a level that Kelvin-Helmholtz billowing can take place. Thirdly, gravitational overturning can be induced by absorption of wave energy at critical layers.

A model that would attempt to describe these processes would be very complex and difficult to verify due to the nature of internal wave dynamics. To avoid these complexities, DYRESM takes a parameterisation approach to modelling the mixing processes in the hypolimnion of lakes.

In DYRESM, hypolimnetic mixing is separated into two parts: 1) internal mixing and 2) (benthic) boundary layer mixing. Both of these mechanisms are invoked in DYRESM only once per day (at midnight at the start of each day):

1. For benthic boundary layer mixing the user specifies a boundary layer thickness. A volume of water can thus be determined for each hypolimnetic layer. Aliquots of water are removed from the corresponding layers and then mixed into the

thermocline region. This simulates the action of the benthic boundary layer (Lemckert *et al.* 2000).

2. 'Internal mixing' encompasses the effects of two mixing mechanisms together: molecular diffusion and shear mixing. For each layer a calculated proportion of the volume is removed and transferred into the layer immediately above it. Similarly, the same volume is mixed from the upper layer into the current layer of interest. This process continues from bottom to top through the water column.

Benthic boundary layer pumping and internal mixing are done once per day and at the start of each day. The benthic boundary layer mixing is calculated first followed by diffusion. These two mechanisms are not invoked whenever the water column is fully mixed at the start of the day.

A volume for each hypolimnetic layer is calculated. An aliquot of appropriate volume is then removed from each layer of the hypolimnion and mixed into the lowest epilimnion layer. The volume for the i^{th} layer is taken to be

$$v_{BBL,i} = (A_i - A_{i-1})h \quad (3.75)$$

where h is the boundary layer thickness provided by the user.

DYRESM uses the Lake Number (L_N) (Imberger and Patterson, 1990) and buoyancy frequencies (N^2) of the water column to determine the amount of water to mix from one layer to another. The Lake Number is calculated once per day by using day-averaged values of its parameters; N^2 is calculated at all the layer boundaries of the water column.

The volume of water transferred from layer i to $i+1$ and, simultaneously, from layer $i+1$ to i is given by

$$v_{IM,i} = f v_i \quad (3.76)$$

The mixing fraction, f , is determined using the parameterisation:

$$f = \frac{200N_i^2 K_M \Delta t}{L_N N_{\max}^2 \left[\frac{\delta_i + \delta_{i+1}}{2} \right]^2} \quad (3.77)$$

where Δt is the model time step, K_M is the molecular diffusivity of heat and δ_i and δ_{i+1} are the thicknesses of layers i and $i+1$ respectively. The purpose of normalising with respect to the maximum buoyancy frequency (N_{MAX}^2) is to ensure that internal mixing in the water column is maximized at the seasonal thermocline. The coefficient of 200 has been determined by fitting a relationship between field estimates of eddy diffusivity and Lake Number in a range of lakes (Yeates and Imberger 2003).

The mixing process starts at the bottom layer and continues up to the immediate sub-surface layer (Figure 3.5) (Antenucci&Imerito, 2000).

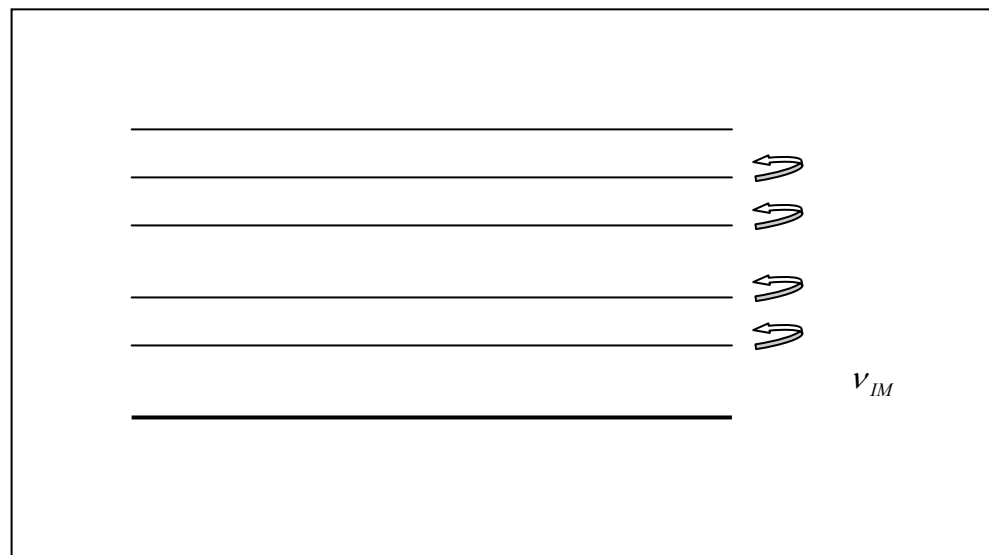


Figure 3.5 The Mixing Process

3.3 Model Applicability

The model DYRESM is based on an assumption of one dimensionality. One-dimensionality means that variations of vertical direction are more important than variations of the horizontal direction.

The one dimensional assumption can be tested by two criteria. The first one is the Lake Number L_N (Imberger and Patterson, 1990). The Lake Number is defined in terms of stability of the stratification and the disturbing influence of wind. L_N can be found as;

$$L_N = \frac{(z_g - z_0)Mg\beta}{\int_{A(z_h)} \rho_0 u_*^2 dA (z - z_g)} \quad (3.78)$$

where z_H is the height of the water column, M is the total mass of water, β is the angle subtended to the vertical by the line segment connecting the center of mass to the center of volume, z_g is height of center of volume, u_* is surface friction velocity, z_0 is the center of gravity as;

$$z_0 = \frac{\int_0^{z_h} \rho(z)zA(z)dz}{\int_0^{z_h} \rho(z)A(z)dz} \quad (3.79)$$

If wind stress is constant over the surface, then L_N reduces to;

$$L_N = \frac{(z_g - z_0)Mg(1 - \frac{z_T}{z})}{A^{1/2}(1 - \frac{z_g}{z}) \int_{A(z_h)} \rho_0 u_*^2 dA} \quad (3.80)$$

If $L_N \gg 1$ then the density structure is approximately horizontal and the one dimensional assumption is valid. So the first criterion is that $L_N \gg 1$.

The second criterion is about the earth's rotation (Patterson&Hamblin&Imberger, 1984). The ratio given below is used to check the effects of the earth's rotation.

$$R = R_I / B \quad (3.81)$$

where R_I is internal Rossby radius of deformation and B is the maximum width of the lake. Internal Rossby radius is defined as;

$$R = \frac{\sqrt{g'h}}{f} \quad (3.82)$$

where g' is the effective reduced gravity over the surface layer depth h , and f is the coriolis parameter. For one-dimensionality, R must be greater than 1. So the second criterion is $R > 1$.

3.4 Model Input Files

The DYRESM-CAEDYM needs some text files to be used as inputs. The files can be grouped as "DYRESM Files" and "CAEDYM Files". These files are;

- 1- DYRESM Conf. File
- 2- Morphometry File
- 3- Initial Profile File
- 4- Meteorologic Data File
- 5- Inflow File
- 6- Withdrawals File
- 7- Parameter File
- 8- Artificial Mixing File
- 9- Field Data File

- 10- CAEDYM Config. File
- 11- CAEDYM Initialisation File
- 12- CAEDYM Water Quality Constants

All of these files must be present in order to run the model. If even one of them is unavailable, the model does not work and gives an error message. The preparation of these files and their contents are given below.

3.4.1 *DYRESM Configuration File*

This text file which must have “.cfg” extension contains the configuration information for a particular simulation. The data that must be in this file are as follows.

Simulation start day; Number of days of simulation; CAEDYM switch (whether run CAEDYM or not keywords are .TRUE. or .FALSE. respectively); Output interval in days; Light extinction coefficient (m^{-1}); Benthic boundary thickness (m); Minimum layer thickness (m); Maximum layer thickness (m); Time step (s); Number of output selections; List of output selections; Artificial mixing switch (.TRUE. or .FALSE.) and operation period indicator (keywords : DAYTIME_OP, NIGHTTIME_OP or CONTINUOUS_OP) ; Non-neutral atmospheric stability correction switch (.TRUE. or .FALSE.)

3.4.2 *Physical Data and Lake Morphometry File*

This text file, which must have the “.stg” extension is about the description of the morphometric characteristics of the water body. Required data for this file are;

Text Header; Latitude : This value is positive for the Northern Hemisphere and negative for Southern Hemisphere; ***Vertical distance*** : of crest of the lake above Mean Sea Level (MSL) in metres; ***Number of inflows*** : Number of streams which are connected to lake or reservoir; ***Inflow type*** : ‘SURF’ keyword for a surface inflow or the ‘height’ of a submerged inflow above the base of the lake; ***Streambed half angle*** : for each inflow, it is given by the value of A (in the figure

3.6); **Streambed slope** : this is given by the value of B (in the figure 3.7), and represents the average stream gradient prior to entering the water body; **Streambed drag coefficient** : typically assumes $C_D = 0.015$; **Name of river** : the name of river; **Zero height Elevation** : the elevation of the reservoir bottom above some arbitrary datum. The datum is irrelevant as long as consistency is maintained throughout the file; **Crest Elevation** : in the case of a dam, this is the elevation of the level of the spillway above the reference datum. The datum used for this elevation must be consistent with the datum used for the zero height elevation. ; **Number of outlets** : this is simply the number of outlets from the water body (excluding the overflow/spill). This value must match with the value in withdrawal file; **Outlet elevations** : the elevations of the individual outlets with respect to the datum; **Lake morphometry** : this consists of a matrix of height-area values which describe the hypsographic curves of the water body. That is, a storage table of elevations (above the datum) versus (horizontal) cross-sectional surface areas at those elevations.

In DYRESM, the first line of the file must be “text header”, and the last line must be “the lake morphometry”. Units used in DYRESM are given in Table 3.2 and a drawing to explain the values used in morphometry file are given Figure 3.8.

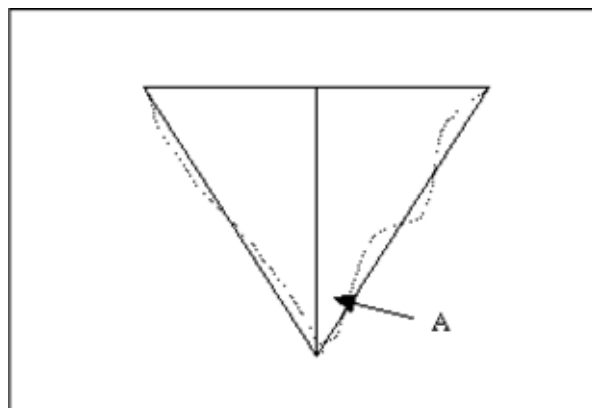


Figure 3.6 : Streambed Half Angle

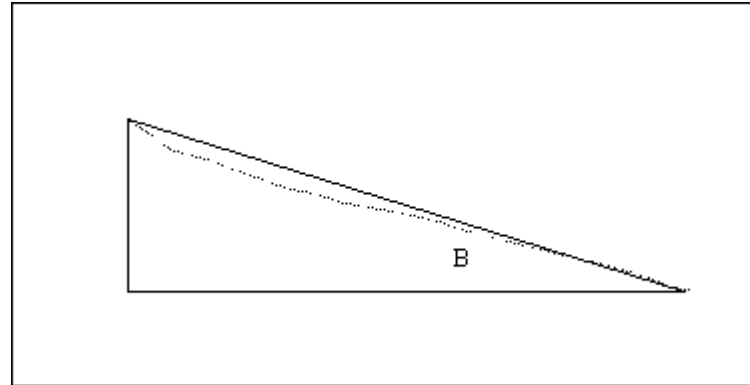


Figure 3.7 : Streambed Slope

Table 3.2 Morphometry Units Used

Attributes	Units
$\frac{1}{2}$ angle	Degrees
Slope	Degrees
drag coefficient	Dimensionless
Elevation	m
Area	m ²

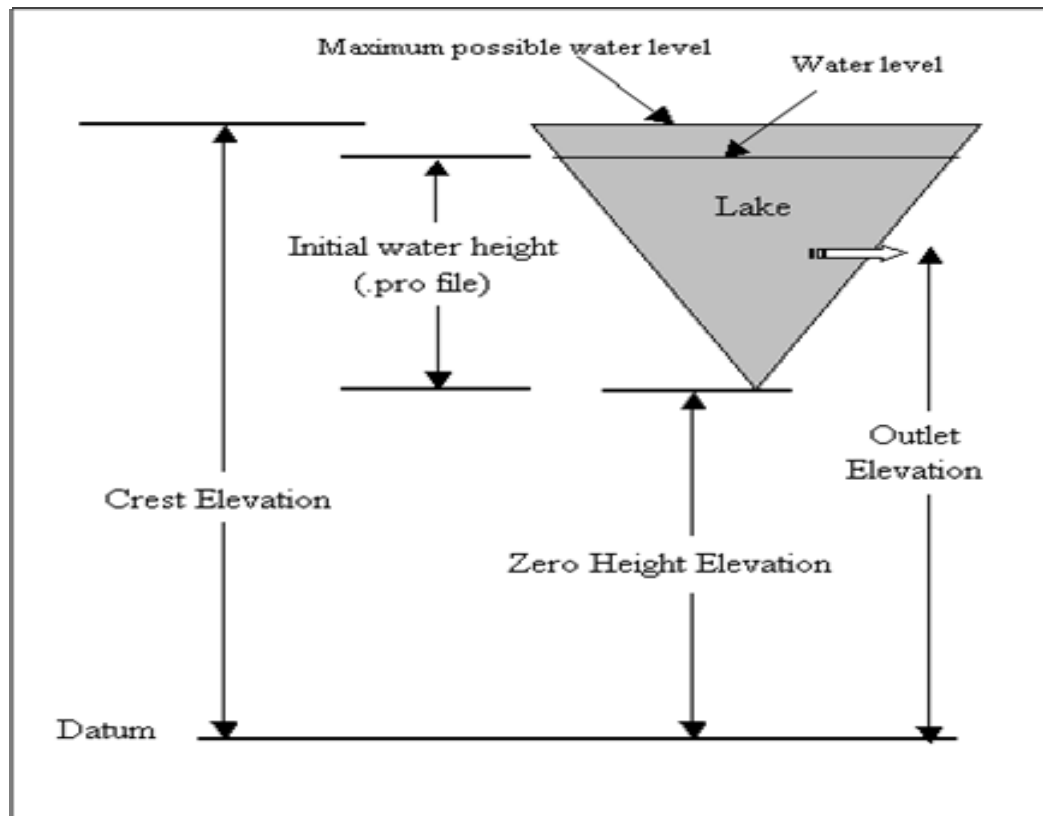


Figure 3.8

3.4.3 Initial Profile File

The initial vertical profile of the water temperature and salinity are given via this file. Extension of this file is “.pro”. The initial profile must be specified at the deepest point in the water body and should be at the start of the first simulation day.

The initial profile consists of a table where there are different columns for each state variable and different rows for the different heights in the reservoir. The height of each layer in the initial profile is specified by its height above the reservoir zero height elevation. The final height listed represents the initial height of the water surface.

3.4.4. Meteorological Data File

This text file contains meteorological data which can be either daily or sub-daily values to cover the simulation period. The file extension must be “.met”.

The header of the file must contain the timestep of the input data in units of seconds. When using the sub-daily meteorological forcing, the input file timestep **MUST MATCH** the simulation timestep. Sub-daily meteorological forcing timesteps must be in the range [10, 180] minutes.

The meteorological file must contain $(86400/\text{timestep})$ data points per day. That is, if a 3 hour (10800 sec) timestep is used, each day of the data file must have $86400/10800 = 8$ data points.

This file must also be contained in the header of the file with a keyword describing the type of longwave radiation data provided. These keywords are **INCIDENT_LW**(long wave incident), **NETT_LW**(long wave), **CLOUD_COVER** (cloud cover fraction (valid range is [0,1])).

The last line of the file header contains information as to whether the sensor is at a fixed height (**FIXED_HT** – with respect to the bottom of the water body) or floating on the water surface (**FLOATING** – *i.e.*, a constant fixed height above the water surface). For a fixed height sensor, the height of the sensor above the lake bottom (*i.e.*, where $z = 0$) must be given. For a floating sensor, the height of the sensor above the water surface must be provided. This information is only used if the non-neutral atmospheric stability correction is invoked

The meteorological data include short wave and longwave radiation (or cloud cover), air temperature, vapour pressure, wind speed and rainfall. The seven columns of the met file are given below.

Ordinal Date : For example, 2002001 refers to 01 January 2002; **Short Wave Radiation** : the short wave radiation power flux density averaged over the input timestep; **Long Wave Radiation** : It can be either the long wave radiation power flux density averaged over the input timestep or as a decimal fraction of cloud

cover according to available data. If cloud cover is entered, the model estimates long wave radiation based on this. If there is no longwave radiation or cloud cover data, cloud cover fraction can be estimated approximately with formula (3.83):

$$C_k = \left(\frac{RH_k - RH_c}{1 - RH_c} \right) \quad (3.83)$$

where C_k : Cloud cover (%), RH_k relative humidity, and RH_c critical cloud cover fraction (%); **Air Temperature** : this is the average temperature over the input timestep; **Average Water Vapour Pressure** : this is the average over the input timestep. This value can be found in two ways: first, from average wet and dry bulb temperatures and second, from average relative humidity and average air temperature. Required formulas and constants are given in figure 3.9 and figure 3.10 ; **Average Wind Speed** : this is the average wind speed over the time step. Wind data are assumed to be collected from the height of the wind speed sensor; **Rainfall** : total rainfall measured over the timestep.

And it is important that these values are written in correct units. The units used in the meteorological file are given in Table 3.3.

$$e_a = e_{as} - 0.00066 * (1 + 0.00115 * q_w) * P * (q_D - q_w)$$

where

e_a = vapour pressure (mb) , e_{as} = saturation vapour pressure (mb),

q_w = wet bulb air temperature (degrees C), q_D = dry bulb air temperature (degrees C) , P = atmospheric pressure (mb)

$e_{as} = \exp[2.303 ((a * q_D / (a * q_D + b)) + c)]$ (*Magnus-Tetens formula*)

$a = 7.5$, $b = 237.3$, $c = 0.7858$

Figure 3.9 : Vapour Pressure Based on Wet and Dry Bulb Temperatures

$$e_a = (h/100) * \exp[2.303 ((a * q_D / (q_D + b)) + c)]$$

where

e_a = vapour pressure (mb), h = relative humidity of air (%), q_D = dry bulb air temperature (degrees C), $a = 7.5$, $b = 237.3$, $c = 0.7858$

Figure 3.10 : Vapour Pressure Based on Relative Humidity and Air Temperature

Table 3.3 : Meteorology Units Used

Attributes	Units
short wave	$W m^{-2}$
Long wave	$W m^{-2}$ or dimensionless for cloud cover
air temp	$^{\circ}C$
vapour pressure	H Pa
Wind speed	ms^{-1}
Rainfall	M

3.4.5 Stream Inflow File

Daily average inflow data during the simulation period such as volume, temperature, salinity (and water quality data if required), are contained by this file. The file must have the “.inf” extension. The contents of this file are as follows:

Ordinal Date : 2002001 represents 01 January 2002; **Inflow Number** : this is a sequence number for each inflow and must be consistent with the information provided for the morphometry (.stg) file; **Volume** : this is the inflow volume; **Temperature** : There are three methods to obtain inflow temperatures: continuous measurements, periodic measurements or estimates from average air temperatures. Linear interpolation is often used between periodically measured temperatures. If no inflow temperature measurements are available, it may be possible to use an average air temperature for a period of about 4 days prior to the date of the inflow entering the water body as an estimate of the inflow temperature; **Salinity** : The salinity of stream/river. In cases where reservoir density stratification is influenced solely by temperature, salinity is not considered important and is commonly as a constant value.

The data units used in inflow file is given in Table 3.4.

Table 3.4 : Inflow Data Units in the stream inflow file

Attributes	Units
daily volume	M ³
Temperature	°C
Salinity	Practical Salinity Scale
WQ parameters	As required by water quality module CAEDYM

The first 5 columns (ordinal date to salinity) must always be present in the correct order. If there are any water quality columns, these are identified by their header labels.

3.4.6 *Withdrawals File*

The text file must have the extension "wdr". Withdrawal data during the simulation period is contained by this file. The withdrawal file consists of a table of daily volumes of outflow from the lake or reservoir. The outflows must be in the order that they were specified in the morphometry file.

The units used in this file are m³ of daily withdrawal volume.

3.4.7 *Parameter File*

This file, which must have “.par” extension, contains 'parameters' of the simulation. The lines of this file must all be present and be in the specified order. The user must be careful if it is decided to change the values in this file.

3.4.8 *Artificial Mixing File*

The DYRESM artificial mixing file specifies the operational set-up of an artificial destratification system, if there is one operating. Currently two destratification devices are possible: DIFFUSER, a bubble plume diffuser, and/or IMPELLER, a surface mounted mechanical mixer with a draft tube. Contents of this file are;

Text Header; Number of Destratification Devices : the number of destratification devices operating in the reservoir; ***Device Type, Draft Tube Length or Diffuser Height, Draft Tube Diameter or Number of Diffuser Ports*** : All dimensions are in metres, with height of the diffuser referring to distance of the bubbler tube above the base of the reservoir. (A height of 0 m indicates that it is lying on the bottom of the water body bed.); ***Volume Flow Rates*** : Indicates the volume flow rate of air (for bubblers) or water (for impellers). Unit is m³s⁻¹.

3.4.9 Field Data File

This file is not used for simulation; it is only used to compare the field data with model results. The extension of this file is “.fld”.

The field data file contains a series of data blocks, one for each measurement period. Data are organised in vertical columns for measured variables.

The order of variables must not change from one measurement period to the next. This means that all measured variables must be present in each data block. If no data are recorded, a no data flag value such as -999 is used. The file must end with the end-of-file keyword **EOF**

3.4.10 CAEDYM Configuration File

This section provides an overview on how to configure a CAEDYM simulation. File extension must be “.con”.

3.4.11 CAEDYM Initialisation File

Initialisation of all the compulsory and configured state variables is performed via the initialisation file named in the I/O section of the con file. The file extension must be “.int”. The file must end with “EOF” keyword.

There are some initialisation methods. These methods and required keywords are given in Table 3.6

Table 3.6 Initialisation Methods in CAEDYM

CODE	DESCRIPTION	CODE	DESCRIPTION
CO_I	Constant Value	FI_I	File Input
LI_I	Linear Distribution	D2_I	Two Dim. Initialisation
EX_I	Exponential Distribution	RI_I	Along-River initialization
IN_I	Piecewise Linear		

3.4.12 CAEDYM Water Quality Constants and Parameters File

The various water quality modules contained in CAEDYM require physiological constants for each of the processes. For example, the parameter file includes growth rates for the various phytoplankton groups, half-saturation rates for many processes, as well as many other parameters.

Specification of physiological constants used by CAEDYM are input via a text file that can be adjusted using the graphical user interface and are saved to the simulation file (Hipsey et al, 2003).

CHAPTER FOUR

APPLICATION

4.1 Project Area

4.1.1 Eymir and Mogan Lakes Basin

The DYRESM-CAEDYM Model described in Chapter III is applied to the case of Eymir and Mogan Lake Basin. This basin is located in Middle Anatolia to the south of Ankara, between 39,28 and 39,53 north latitudes and 32,30 and 33,00 east longitudes. The total area of the basin is approximately 971,4 km². 245 km² of total drainage area was declared in 1990 as “Special Environment Protect Zone” by decision of the Cabinet. The basin has a rectangular shape with 50 km length and 19 km width. The maximum elevation in the basin is 1650 m and the minimum elevation in the basin is 950 m. Figure 4.1 and 4.2 show the location of the lakes basin. The latter figure also indicates the borders of the “Special Environmental Zone”.

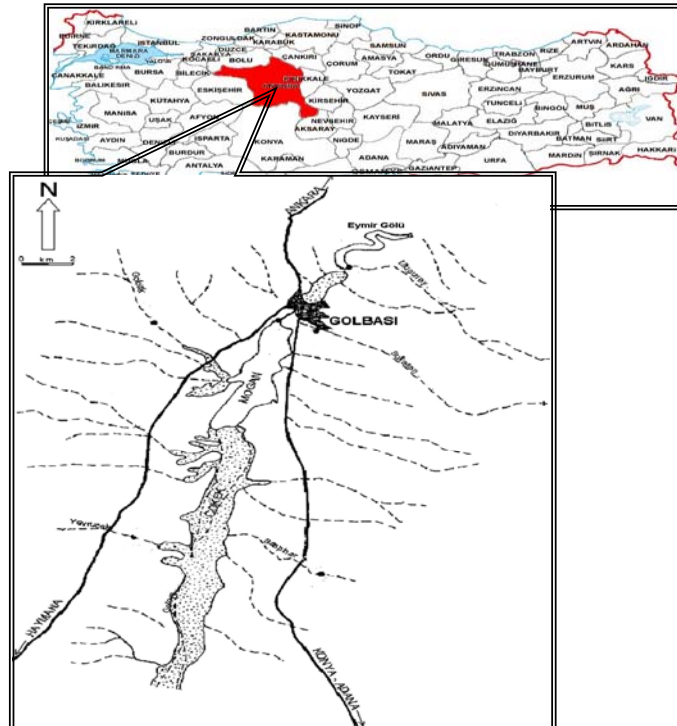


Figure 4.1 Location of the Eymir-Mogan Lakes Basin in Central Anatolia

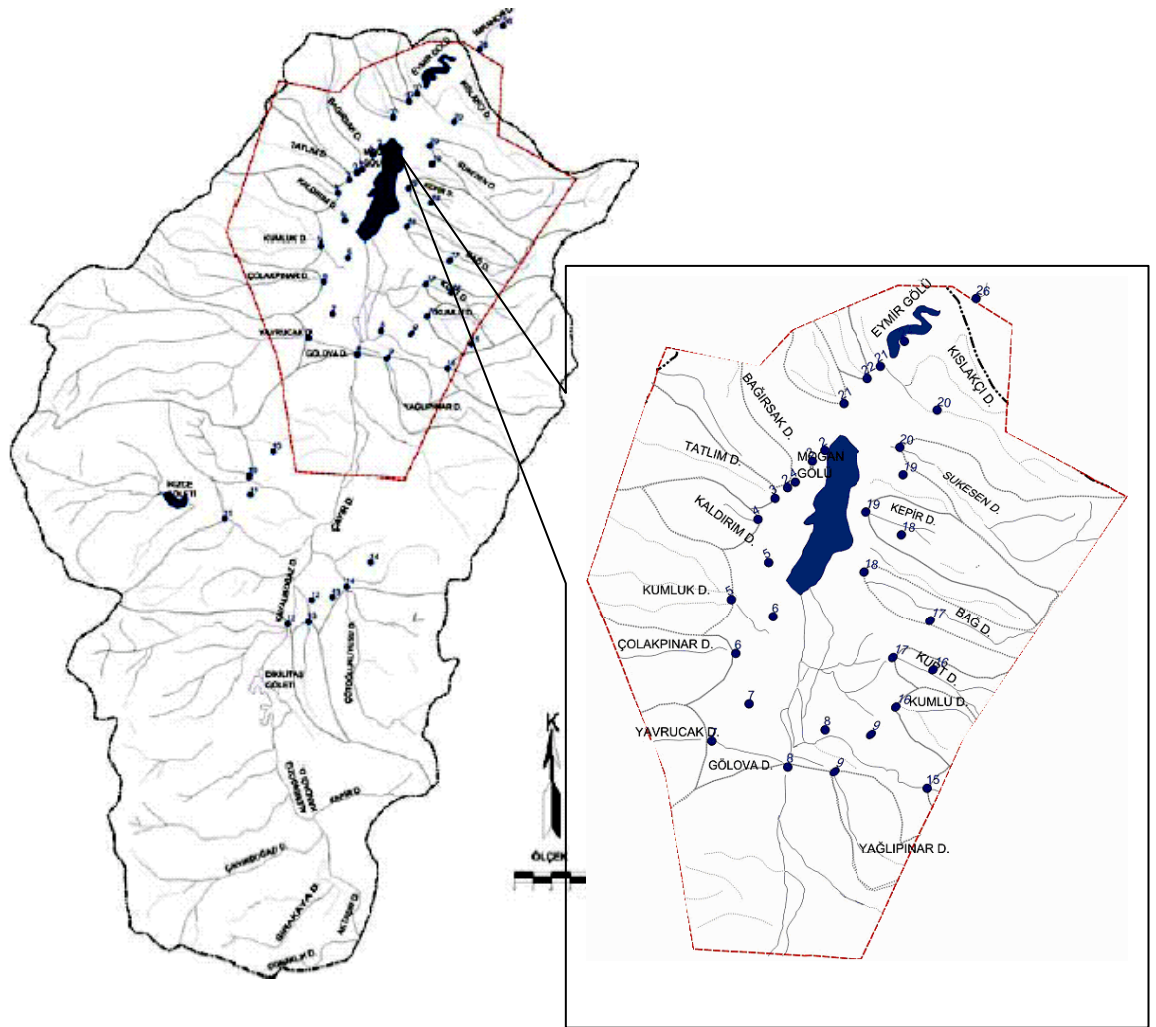


Figure 4.2 The drainage area and the Special Environmental Protection Zone in the Eymir-Mogan Lakes basin

Gölbaşı, located at the north shore of Mogan Lake is the denser residential area in the project site. There are also 10 villages in the basin. Total population of villages and Gölbaşı are respectively 3699 and 25123. Gölbaşı is at a distance of 35-40 km to Ankara and can be reached in about 45 minutes. Due to the easy transportation, rapid

population growth and urbanization has been observed extensively in the basin (Altınbilek, 1995).

4.1.2 Water Resources of the Lakes Basin

Mogan and Eymir Lakes are two shallow lakes, interconnected hydrologically in the close vicinity of Ankara. In addition to Eymir and Mogan lakes, there are İkizce and Dikilitaş artificial lakes in the basin. In the basin, Mogan and Eymir's surface areas, lengths, and widths differ from season to season because of water level changes. Mogan Lake has an area of about 6 km². The length of the lake is about 6000 m and width is about 1000 m. The shores of the lake extend approximately to 14 km. Eymir is smaller than Mogan and has an area of 1,22 km². Its length and width are respectively 4000 m and 300 m. The elevation of Eymir is 3 m lower than Mogan's elevation and so that water flows from Mogan to Eymir.

Çölova Stream is the main stream of basin. Other streams which discharge to Mogan are Yavrucak, Başpınar, Yağlıpınar, Kurt, Kumluk, Çolakpınar, Tatlım, Gölcük, Kaldırım, and Sukesen streams. Mogan Regulator represents the only outgoing flow which discharges to Eymir and its main stream. Kışlakçı stream is the another entered stream that contributes to Eymir.

Streams which flow every season except for the driest seasons are Sukesen, Başpınar, Yavrucak, and Çölova. These streams are shown on Fig. 4.3.

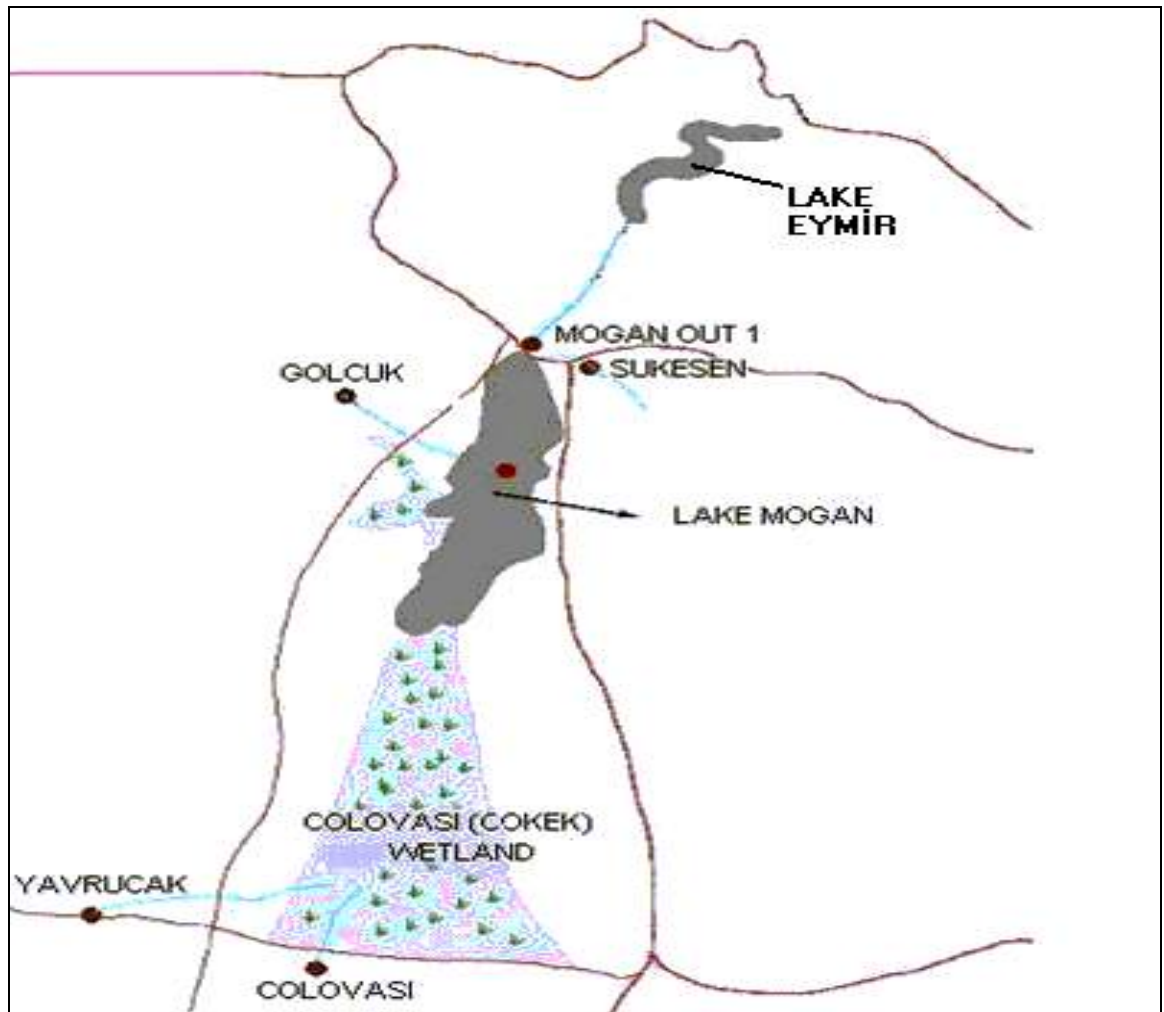


Figure 4.3 Mogan and Eymir Lakes with contributing streams (Burmak & Beklioğlu 2000)

4.1.3 General Characteristics of the Project Area

Mogan and Eymir lakes were designed by DSI for flood control. They protect Ankara from the floods of the Imrahor Stream.

Although many properties of the two lakes change from season to season, some of their characteristics can be given as minimum, normal, and maximum values. Water levels, volume, area, drainage area, and elevations of the deepest points are summarized in Table 4.1.

Table 4.1 General Characteristics of Eymir and Mogan lakes

Lakes	MOGAN			EYMİR		
Water Levels (m)	Minimum 971	Normal 972	Maximum 973,25	Minimum 967	Normal 968,50	Maximum 969,50
Volume (10 ⁶ m ³)	6,20	11,63	20,24	3,88	3,68	4,8
Area(km ²)	4,77	5,43	7,72	1,05	1,25	1,34
Watershed Area(km ²)	925			971		
Elevation of the Deepest Point (m)	968,00			963,90		
Latitude	39°53'			39°28' N		
Longitude	33°00' E			32°30' E		

4.2 Data Used in Model Applications

DYRESM-CAEDYM model application requires particular daily observed data along with information on streams and lakes. The compulsory daily data required by DYRESM-CAEDYM are:

1. Stream Volumes
2. Rain (depth)
3. Wind Speed
4. Cloud Cover
5. Long Wave Radiation (or Cloud Cover)
6. Shortwave Radiation
7. Air Temperature
8. Stream Temperature

Several water quality variables can be modelled by DYRESM-CAEDYM. However, due to lack of proper data, only the following variables are modified in this study:

1. PO₄
2. NO₃
3. NH₄
4. PH
5. DO
6. Salinity

Some other values describing the characteristics of the streams and lakes are also required. These values are light extinction coefficient, benthic boundary thickness, streambed half angle, streambed slope, streambed drag coefficient, initial temperature and salinity values, latitude of lake, and elevation-surface area matrix of lake.

Data which are required to run the DYRESM-CAEDYM model are obtained from different sources. The meteorological data are taken from the Culuk Meteorology Station (12-M04) operated by EIE. Characteristic values of the streams are taken from some flow gauging stations operated by DSI, and water quality data of streams and lakes are obtained from the Ministry of Environment and Forestry.

4.3 Model Runs

It was determined in the presented study that the period between 1 March 2002 and 30 September 2002 was the most appropriate timeline for model simulations because all the required data (meteorology, stream and water quality) to run DYRESM were available for this period. Phosphate (PO₄), nitrate (NO₃), ammonium (NH₄) and dissolved oxygen (DO) were chosen as the water quality parameters to be modelled. In addition to these, temperature and salinity variations were also modelled. The parameters such as silica (SiO₂), chyllorophil-a, dissolved inorganic

carbon (DIC), dissolved organic carbon (DOCL), dissolved organic nitrogen (DONL), particulate organic nitrogen (PONL), particulate organic carbon (POCL), particulate organic phosphorus (POPL), dissolved organic phosphorus (DOPL) were not included the study because they were not gauged at the project site.

The model application involves three steps as:

- 1- Estimation of daily water quality values
- 2- Preparation of model input files
- 3- Running the model

4.3.1 Estimation of Daily Water Quality values

The DYRESM-CAEDYM model needs daily water quality data for the simulations. However, water quality data in the streams connected to Eymir or Mogan Lakes are gauged monthly instead of daily. In order to run the model, linear interpolation was applied between consecutive months to estimate daily values.

4.3.2 Preparation of Model Input Files

The preparation of input files is explained earlier in Chapter 3. The most important issue here is that all of the data must be defined in correct units. In addition, all the heights and depths must be given relative to a common datum. Otherwise, the model gives unlogical results.

In DYRESM configuration file, an average value for light extinction coefficient is used. In the physical data and lake morphometry file, streambed half angles are given as approximate values because stream profiles are not available.

As is the case in general, model application in the presented study has suffered from lack of proper data. The model needs daily water quality values which were not available for the study so that linear interpolation is used between the monthly

quality data to obtain daily values. These estimated values may not represent the real occurrences but there is no other way of estimating daily values. For the meteorological file, cloud cover and vapour pressure values did not exist. Thus, these values were obtained by formulas explained in section 3.3.4 of Chapter 3. Some screenshots of Mogan and Eymir configuration files and input files are given in Figure 4.3, Figure 4.4, Figure 4.5 , Figure 4.6, Figure 4.7, Figure 4.8, Figure 4.9, Figure 4.10.

```

<#4>
DYRESM configuration file for mogan
2002060          # Başlangıç günü
210             # çalıştırılma süresi
.TRUE.         # CAEDYM çalıştırılacak mı?
1              # çıktı zaman aralığı
0.4            # Işık geçirgenlik katsayısı (m-1)
0.50          # Bentik tabaka kalınlığı (m)
0.20          # Min tabaka kal. (m)
0.50          # Max tabaka kal. (m)
3600          # zaman adımı (s)
7              # çıktı tercihlerinin sayısı
SALINITY TEMPTURE PO4 NO3 NH4 PH DO # çıktı tercihlerinin listesi|
.FALSE.       # Activate bubbler (.TRUE. or .FALSE.)
.FALSE.       # Activate non-neutral atmospheric stability (.TRUE. or .FALSE.)

```

Figure 4.3 Mogan Configuration File

```

<#4>
DYRESM configuration file for eymir
2002060          # Simulation start day
210             # Simulation length (in days)
.TRUE.         # Run CAEDYM (.TRUE. or .FALSE.)
1              # Output Interval (in days, -9999 for every time step)
0.4            # Light extinction coefficient (m-1)
0.0            # Benthic Boundary Thickness (m)
0.20          # Min layer thickness (m)
0.50          # Max layer thickness (m)
3600          # Time Step (s)
7              # Number of Output Selections
SALINITY TEMPTURE PO4 NO3 NH4 PH DO # List of Output Selections
.FALSE.       # Activate bubbler (.TRUE. or .FALSE.)
.FALSE.       # Activate non-neutral atmospheric stability (.TRUE. or .FALSE.)

```

Figure 4.4 Eymir Configuration File

```

mogan
39 #Enlem (kuzey yarım küre +, Güney yarım küre - )
971.53 #Su seviyesinden yükseklik (m)
7 #Giren akım sayısı. Aşağıda özellikleri (.inf de aynı sayı
SURF 70 0.02 0.015 yavrucak #height, 1/2-angle, slope, drag coeff
SURF 70 0.01 0.015 colova #height, 1/2-angle, slope, drag coeff
SURF 70 0.025 0.015 baspinar #height, 1/2-angle, slope, drag coeff
SURF 70 0.04 0.015 sukesen #height, 1/2-angle, slope, drag coeff
SURF 70 0.02 0.015 golcuk #height, 1/2-angle, slope, drag coeff
SURF 70 0.02 0.015 tatlim #height, 1/2-angle, slope, drag coeff
SURF 70 0.02 0.015 colakpinar #height, 1/2-angle, slope, drag coeff
0 # zero-ht elevation
2.47
1 # Çıkan akım sayısı
0.5 # çıkan akım yüksekliği
6 # kaç satır yükseklik-alan var
Elev_[m] SurfArea_[m^2]
0.47 6192982
0.97 6781581
1.47 7564834
1.86 7841400
1.97 8052174
2.47 8669274

```

Figure 4.5 Mogan Morphometry File

```

<#3>
eymir
39 #enlem (kuzey yarım küre +, Güney yarım küre - )
966.42 #taban kotu
2 #Giren akım sayısı. Aşağıda özellikleri (.inf de aynı sa
SURF 70 0.01 0.015 kanal #height, 1/2-angle, slope, drag co
SURF 70 0.02 0.015 kislakci #height, 1/2-angle, slope, drag co
0 # zero-ht elevation
3.58 # toplam yükseklik tabandan [m]
1 # Çıkan akım sayısı (.wdr'de o kadar çıktı)
1 # outlet heights(eğer n tane çıkan varsa yanyana bir boşlu
8 # number of stg survey points after header line
Elev_[m] SurfArea_[m^2]
0.08 976060
0.58 1043158
1.08 1102786
1.58 1182000
2.08 1257007
2.58 1313730
3.08 1368694
3.58 1415113

```

Figure 4.6 Eymir Morphometry File

Mogan									
# of inflows									
7									
yavrucak									
colova									
baspinar									
sukesen									
golcuk									
tatlim									
colakpinar									
YrDayNum	InfNum	VOLUME	TEMPURE	SALINITY	PH	DO	NH4	NO3	PO4
2002060	1	24624	3.3	0	8.38	11.8	0.09	4.5	0.11
2002060	2	6566.4	12.7	1	8.49	10.39	0.05	1	0.05
2002060	3	259.2	13	0.4	8.5	6.04	1.2	6.8	0.96
2002060	4	6220.8	15	0	8.04	9.95	3	2.7	0.04
2002060	5	4233.6	14.9	0.2	8.81	9.5	0.05	1.03	0.03
2002060	6	172.8	7.9	0.2	8.12	8.65	0.12	3.9	0.07
2002060	7	172.8	8.6	0.1	8.4	10.1	0.01	1.2	0.5
2002061	1	21600	3.45	0	8.39	11.78	0.09	4.48	0.11
2002061	2	6566.4	12.53	1	8.49	10.23	0.05	0.97	0.05
2002061	3	259.2	12.78	0.4	8.49	6.01	1.19	6.71	0.94
2002061	4	6220.8	14.78	0	8.05	9.81	2.91	2.67	0.04
2002061	5	3888	14.72	0.2	8.8	9.39	0.05	1.04	0.03
2002061	6	172.8	7.81	0.2	8.12	8.46	0.12	3.96	0.07

Figure 4.7 Mogan Inflow File

Eymir									
# of inflows									
2									
kanal									
kisilakci									
Yrdaynum	InfNum	VOLUME	TEMPURE	SALINITY	PH	DO	NH4	NO3	PO4
2002060	1	0	0	0	0	0	0	0	0
2002060	2	3715.2	15.1	0	9.02	9.4	0.39	2.3	0.18
2002061	1	0	0	0	0	0	0	0	0
2002061	2	3801.6	14.84	0	9.01	9.36	0.38	2.25	0.18
2002062	1	0	0	0	0	0	0	0	0
2002062	2	3974.4	14.58	0	8.99	9.32	0.37	2.21	0.17
2002063	1	0	0	0	0	0	0	0	0
2002063	2	4060.8	14.33	0	8.98	9.28	0.36	2.16	0.17
2002064	1	0	0	0	0	0	0	0	0
2002064	2	4233.6	14.07	0	8.97	9.25	0.35	2.12	0.16
2002065	1	0	0	0	0	0	0	0	0
2002065	2	4320	13.81	0	8.96	9.21	0.34	2.07	0.16
2002066	1	0	0	0	0	0	0	0	0
2002066	2	4492.8	13.55	0	8.94	9.17	0.33	2.03	0.16
2002067	1	0	0	0	0	0	0	0	0
2002067	2	4579.2	13.29	0	8.93	9.13	0.32	1.98	0.15
2002068	1	0	0	0	0	0	0	0	0
2002068	2	4752	13.04	0	8.92	9.09	0.32	1.94	0.15
2002069	1	0	0	0	0	0	0	0	0
2002069	2	4838.4	12.78	0	8.91	9.05	0.31	1.89	0.15
2002070	1	0	0	0	0	0	0	0	0

Figure 4.8 Eymir Inflow File

```

<#3>
! mogan meteorological data
86400          # met data input time step (seconds)
CLOUD_COVER   # longwave radiation type (Cloud_cover, INCIDENT_LW)
FIXED_HT 15
JDAY          SW[W/m2]      CL[%} AIRT[C]  VP[mb]  WS[m/s]  RAIN
2002060      211,8         0,275 4,71   5,026   3,79    0
2002061      213          0,219 8,01   5,793   3,06    0
2002062      221          0,243 7,52   5,824   5,2     0
2002063      194,8        0,301 4,622  5,170   4,17    0
2002064      218,9        0,178 7,09   5,045   2,02    0
2002065      208,9        0,116 7,64   4,510   2,14    0
2002066      207,7        0,148 9,16   5,445   3,68    0
2002067      202,4        0,110 10,02  5,207   5,05    0
2002068      222,7        0,189 8,04   5,506   3,55    0

```

Figure 4.9 Mogan Meteorological Data File

```

<#3>
! eymir meteorological data
86400          # met data input time step (seconds)
CLOUD_COVER   # longwave radiation type (Cloud_cover. INCIDENT_LW)
FIXED_HT 15
JDAY          SW[W/m2]      CL[%} AIRT[C]  VP[mb]  WS[m/s]  RAIN
2002060      211.8         0.475 1.710   5.026   3.79    0
2002061      213          0.419 5.010   5.793   3.06    0
2002062      221          0.443 4.520   5.824   5.2     0
2002063      194.8        0.501 1.622   5.170   4.17    0
2002064      218.9        0.378 4.090   5.045   2.02    0
2002065      208.9        0.316 4.640   4.513   2.14    0
2002066      207.7        0.348 6.160   5.445   3.68    0
2002067      202.4        0.310 7.020   5.207   5.05    0
2002068      222.7        0.389 5.040   5.506   3.55    0
2002069      209.6        0.639 -3.063   5.00    1.82    0

```

Figure 4.10 Eymir Meteorological Data File

4.3.3 Simulation

After the required input files are created, the model becomes ready to run. The information in input files are moved to the 'reference file' and the 'simulation file' by the 'Modeller' program. Then, the Model takes all data from these two files. In Figs. 4.11 and 4.12, the basic processes in Modeller program are shown. After

running the model, obtained results can be visualised again by Modeller program as shown in Figure 4.13.

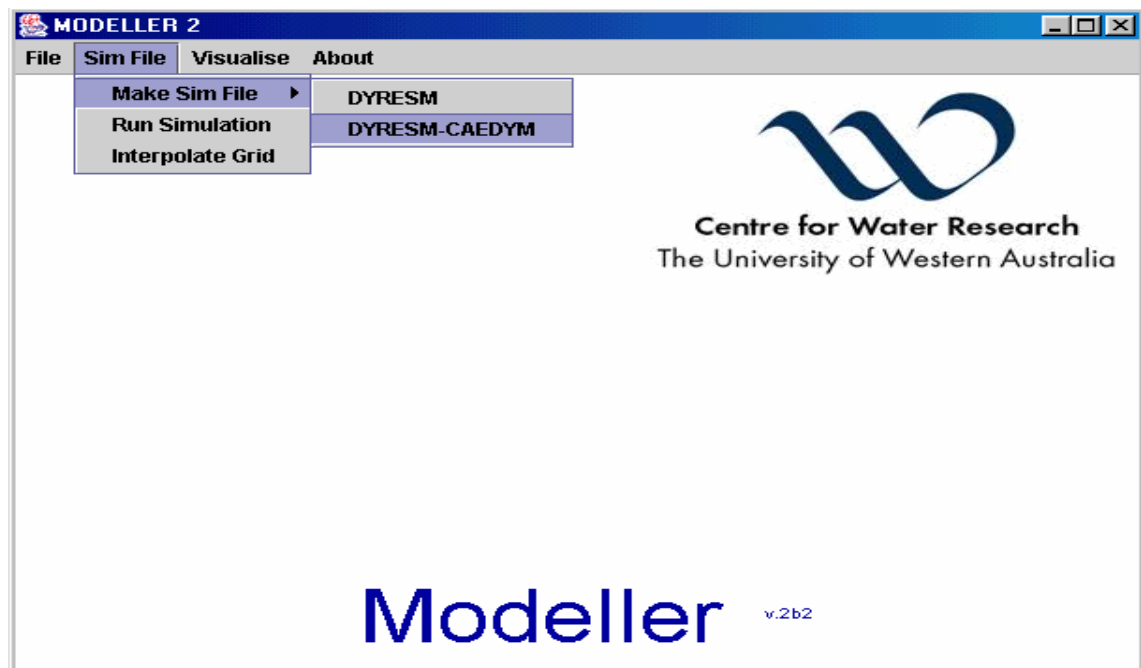


Figure 4.11 Running Simulation with the Modeller Program

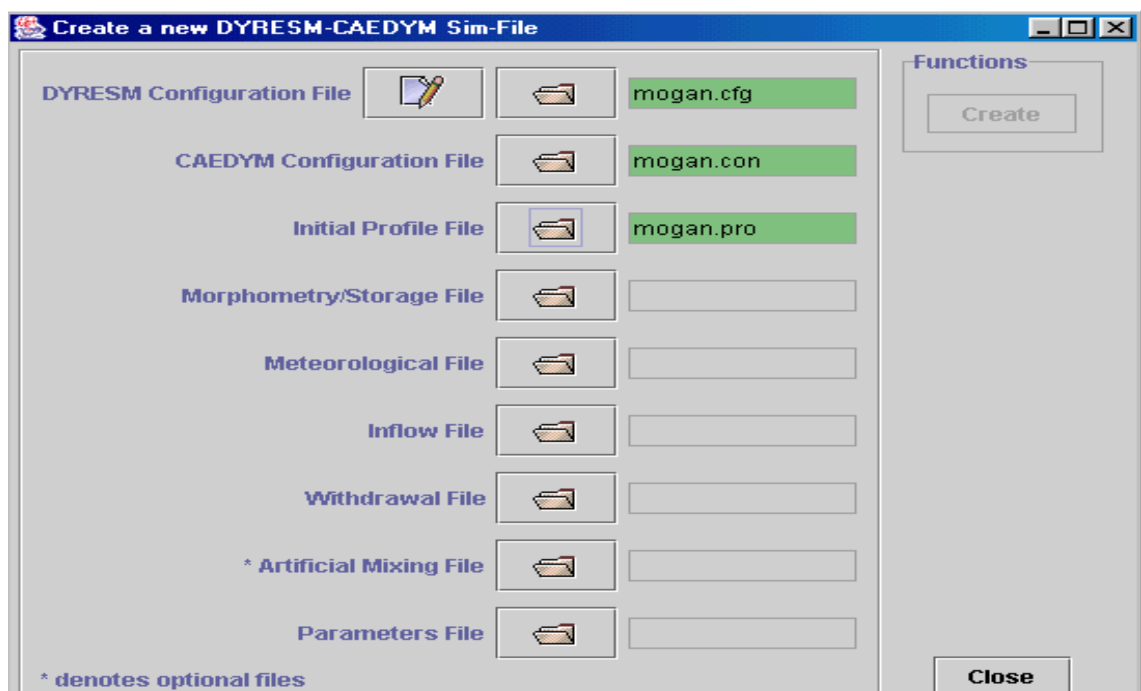


Figure 4.12 Running Simulation with Modeller where All Configuration and Input Files Are Utilized

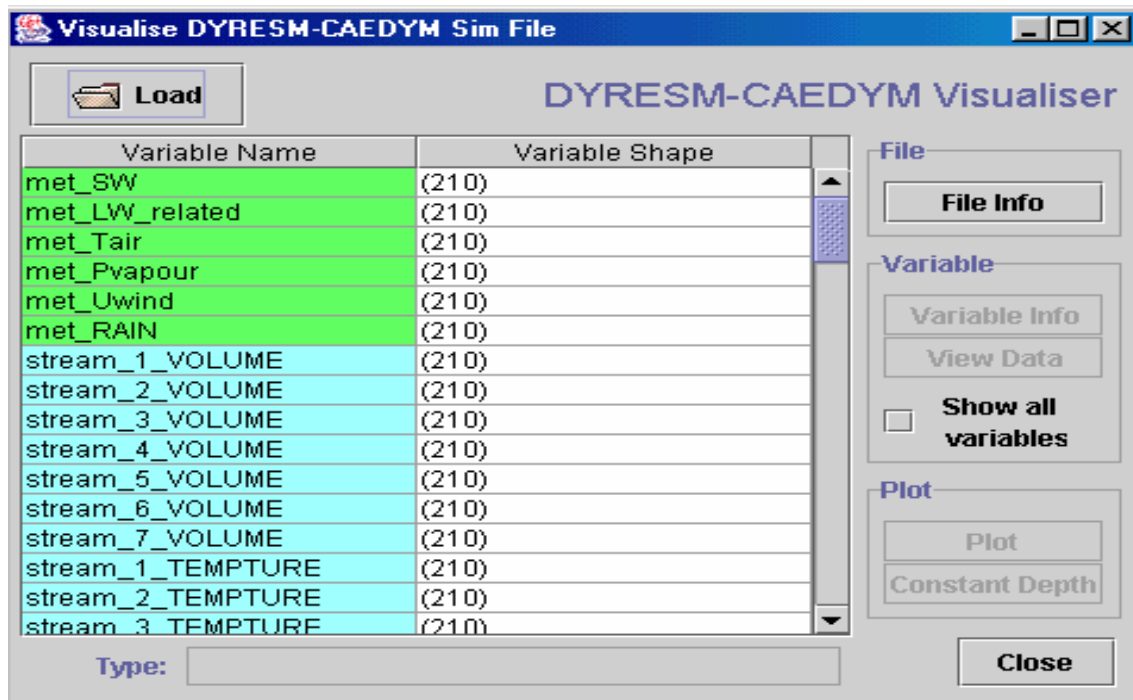


Figure 4.13 Visualising Model Results with Modeller

CHAPTER FIVE

RESULTS

The results obtained by application of the DYRESM-CAEDYM model in Eymir-Mogan Lakes Basin are summarized in this chapter. Figure 5.1 shows the observed (the pink line) and the modelled (the blue line) water depths of Mogan Lake. It can be seen in the figure that observed values are very close to the model results, especially for the first 110 days. Within the last 100 days, there is a gap between the two lines, which indicates that there is actually less water in the lake than those obtained by model estimations. It is possible that *leaking* is the main reason of this gap. However, since this discrepancy occurs in summer months, it may also mean that the model does not estimate evaporation values correctly.

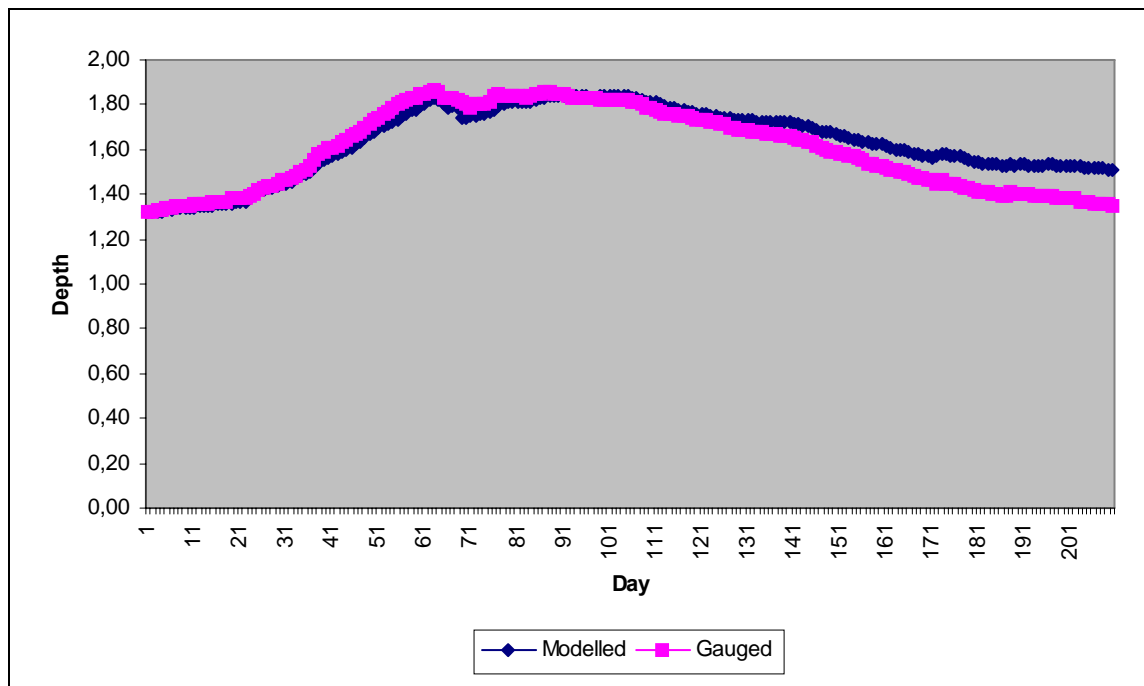


Figure 5.1 Gauged and Modelled Water Depths in Mogan Lake

Modelled water quality parameters DO, NH_4 , NO_3 , and PO_4 are given in Figs. 5.2, 5.3, 5.4, and 5.5 respectively. Like terrestrial animals, fish and other aquatic organisms need oxygen to live. Oxygen also is used for many chemical reactions that are important to lakes. Discharge of industrial and domestic waste waters leads to increased amounts of NO_3 and PO_4 concentrations. Figure 5.4 shows that NO_3

concentrations are quite high in May and at the end of August. PO_4 and NH_4 concentrations are increased in summer months (Figs. 5.3 and 5.5). However, steadily decreases from March to August. It is because cold water can hold more gas than warmer water; but this result basically shows that the lake receives more pollutants during this period so that DO is depleted.

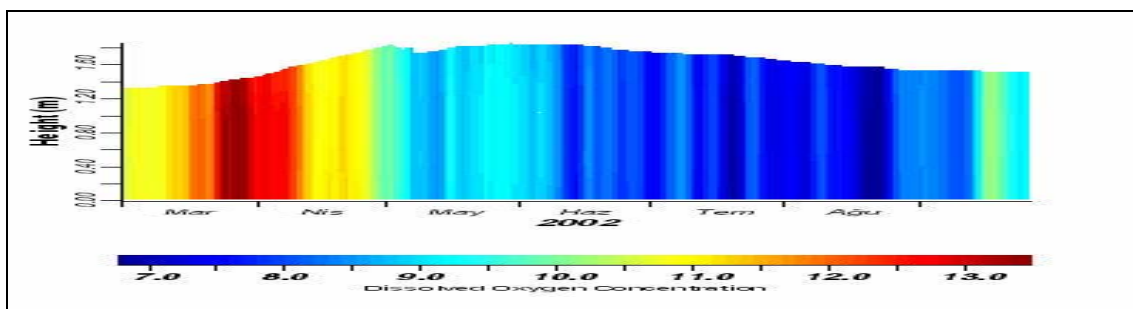


Figure 5.2 Modelled DO Concentrations in Mogan Lake

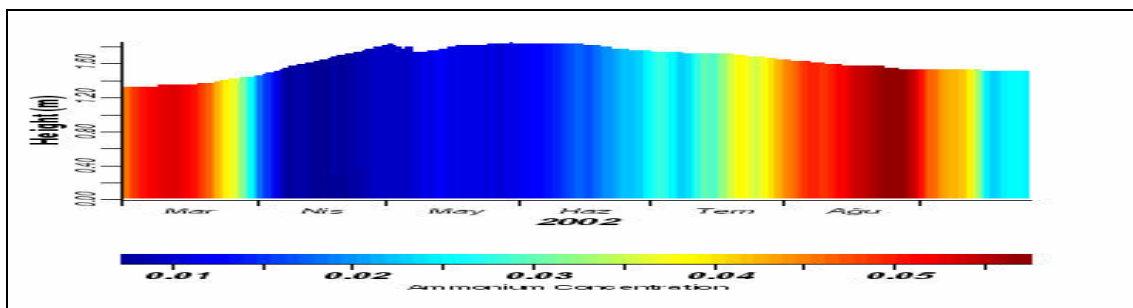


Figure 5.3 Modelled NH_4 Concentrations in Mogan Lake

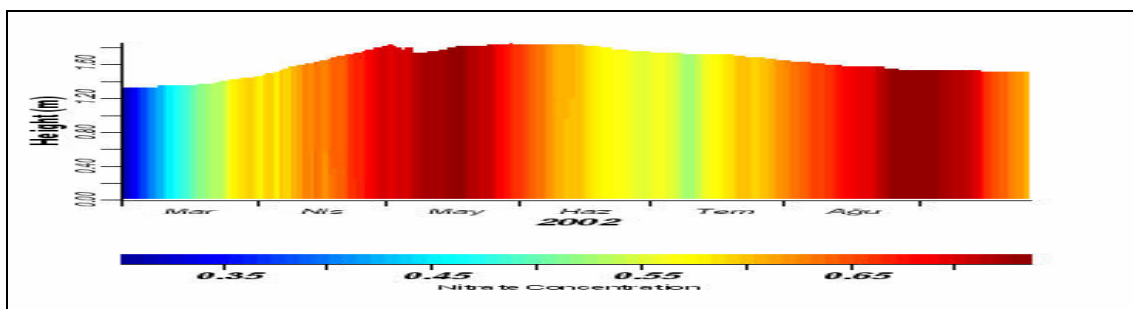


Figure 5.4 Modelled NO_3 Concentrations in Mogan Lake

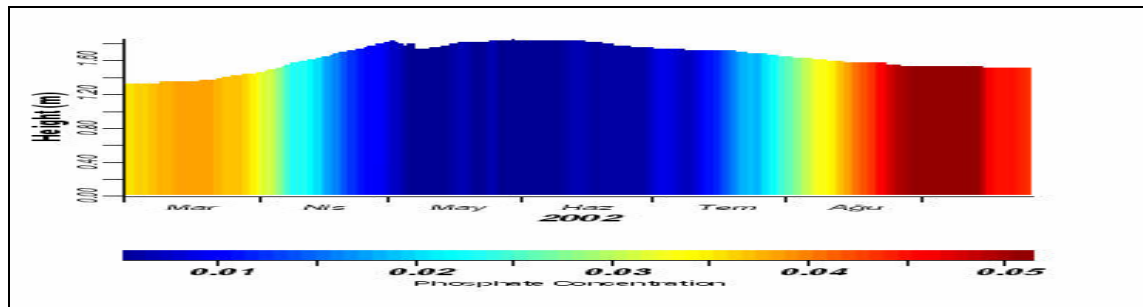


Figure 5.5 Modelled PO_4 Concentrations in Mogan Lake

Salinity values indicate whether the lake water is appropriate for irrigation or not. The maximum salinity in Mogan Lake is found to be 1,1 (Fig. 5.6) in March. In the other months it fluctuates between 1 and 0,80 values.

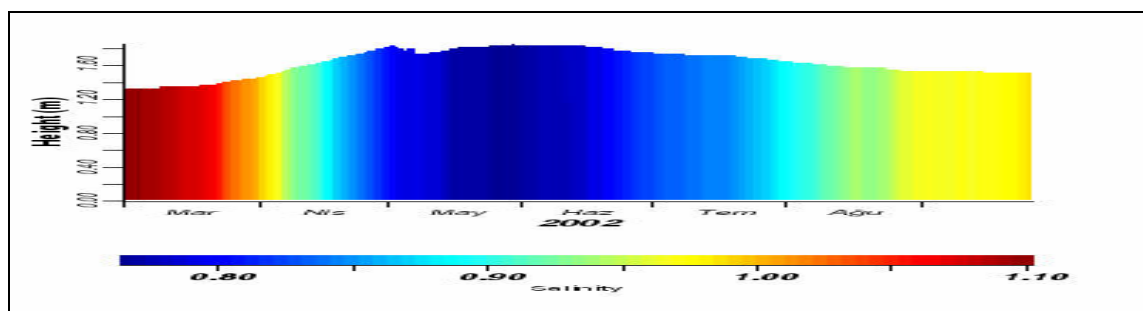


Figure 5.6 Modelled Salinity in Mogan Lake

Temperature is an important variable for surface waters. Water temperature affects many physical, chemical, and biological processes to affect also the values of various water quality parameters like DO and BOD (Uslu & Türkman 1987). In Figure 5.7 modelled temperatures of Mogan Lake are given. It is clearly seen from this figure that the lake experiences high temperature variations between summer and winter months (there is about $28-5 = 23$ °C temperature difference) due to climate of the region.

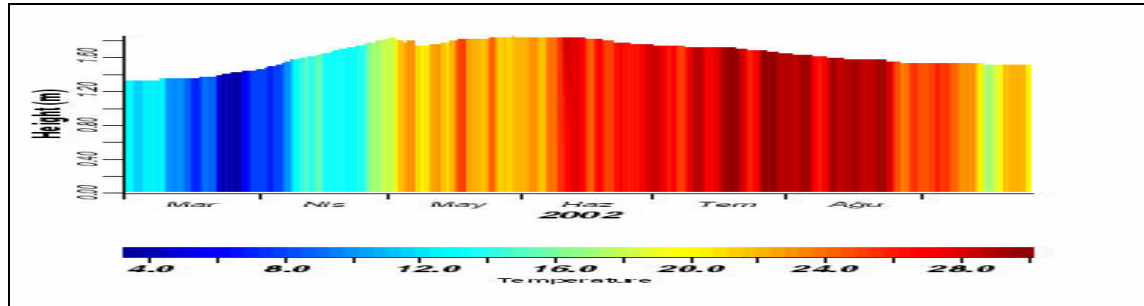


Figure 5.7 Modelled Temperatures in Mogan Lake

In Figure 5.8 modelled and observed water depths in Eymir Lake are shown only for the first 61 days of simulation because gauged water depths exist only for this period. In Figure 5.9, the graph of monthly water depths are given, which initially start as Mogan Lake water depths. For the first 40 days, observed values and model results are very close to each other; but, after 40 days observed values exceed the model results. The same result was found in the study by Altınbilek (1995). As mentioned before, model results show that Mogan Lake has less and Eymir has more water than the observed values. Ungauged flows on the Mogan Regulator or waters leaking from Mogan to Eymir may be responsible for this result. Ungauged Eymir Regulator outflows may also lead to this result.

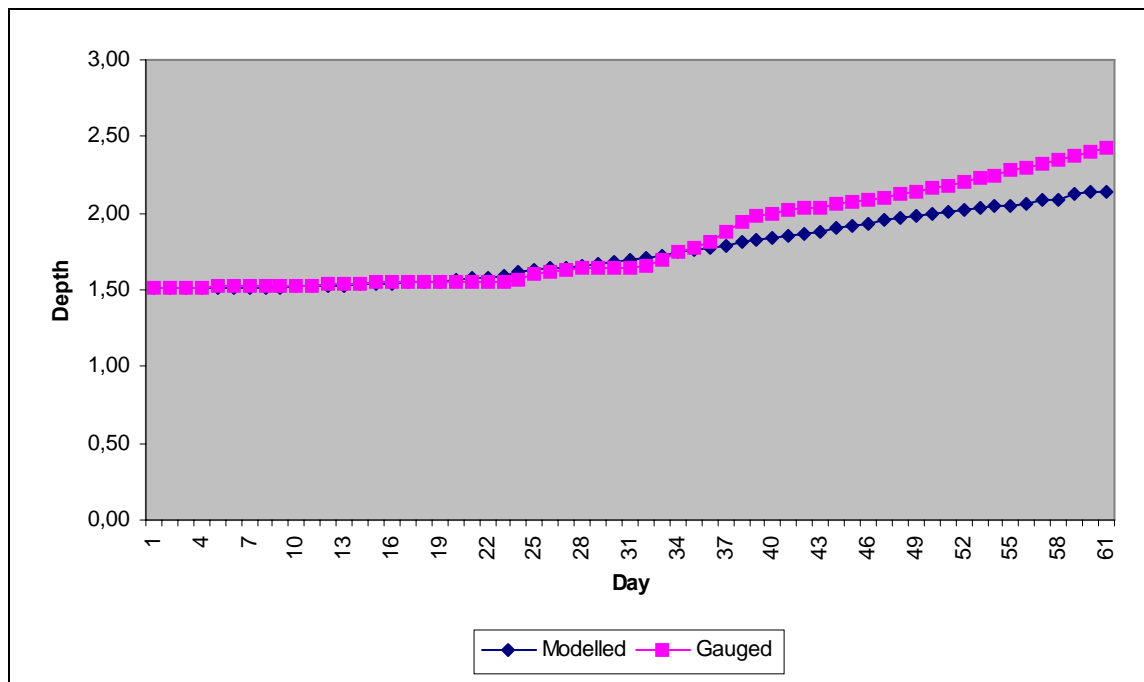


Figure 5.8 Gauged and Modelled Water Levels in Eymir Lake

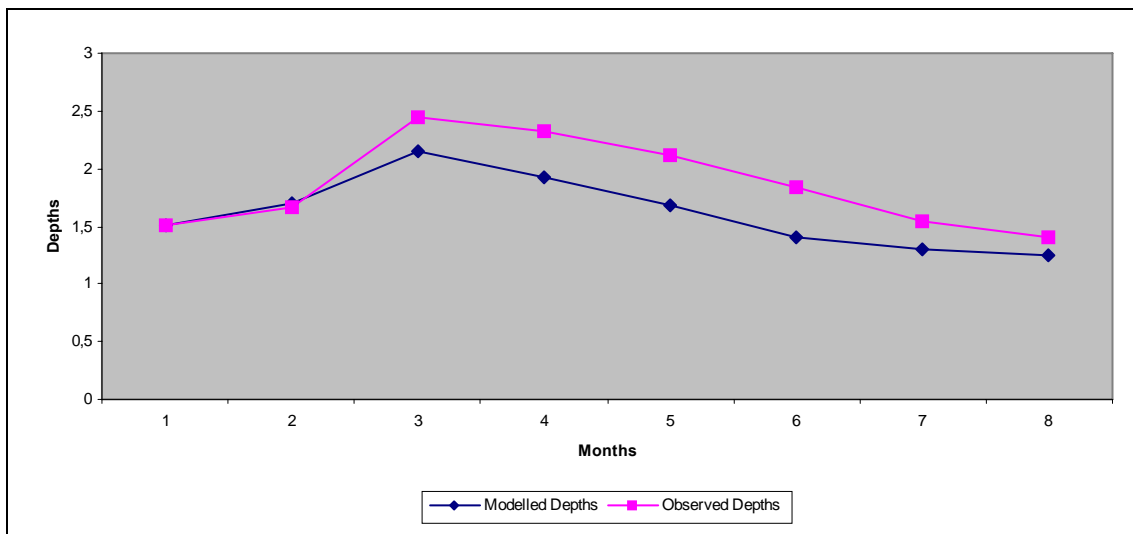


Figure 5.9 Monthly Gauged and Modelled Water Levels in Eymir Lake

DO, NH_4 , NO_3 , and PO_4 concentrations for Eymir Lake are given in Figs. 5.10, 5.11, 5.12, and 5.13 respectively. As in the case of Mogan, DO concentrations decrease in summer months. NH_4 and NO_3 concentrations decrease while precipitation which is main resource of NH_4 and NO_3 , decreases.

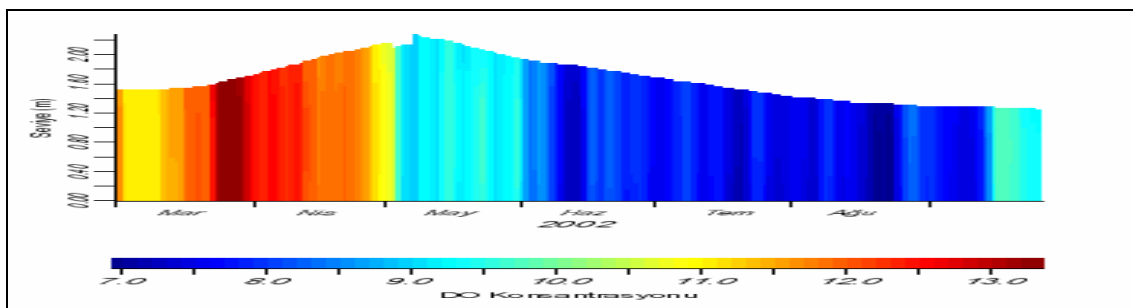


Figure 5.10 Modelled DO Concentrations in Eymir Lake

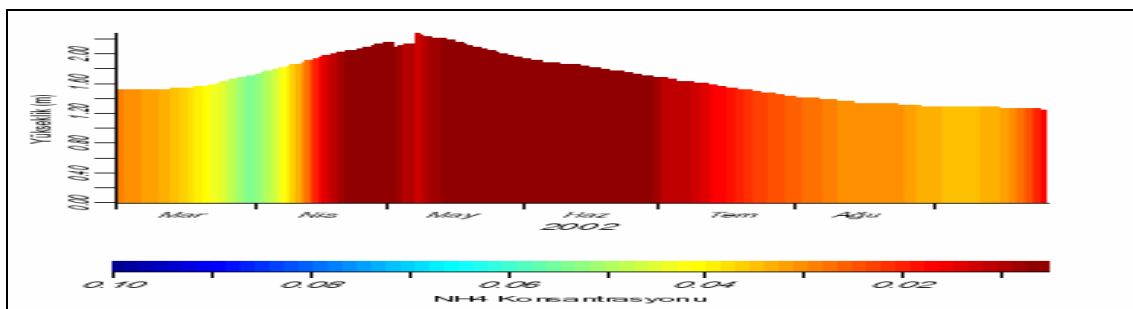


Figure 5.11 Modelled NH_4 concentrations in Eymir Lake

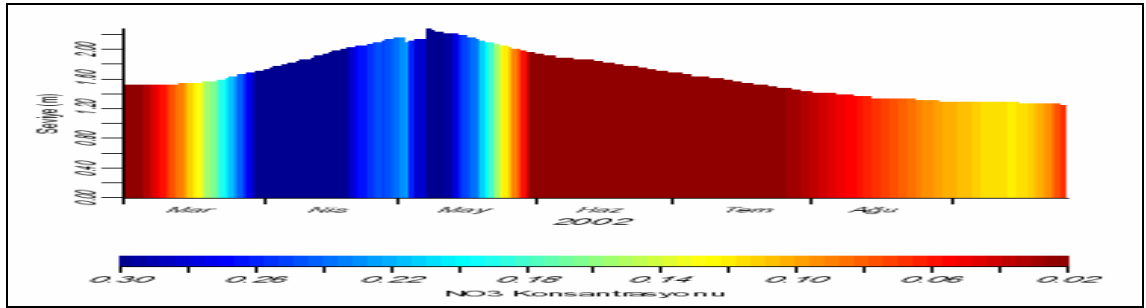
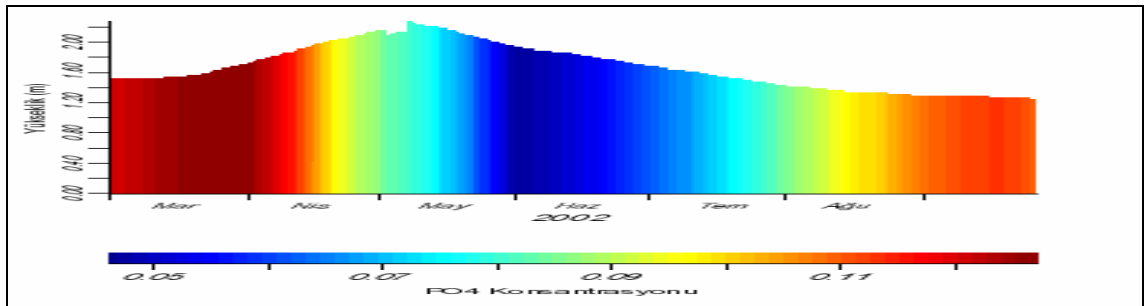
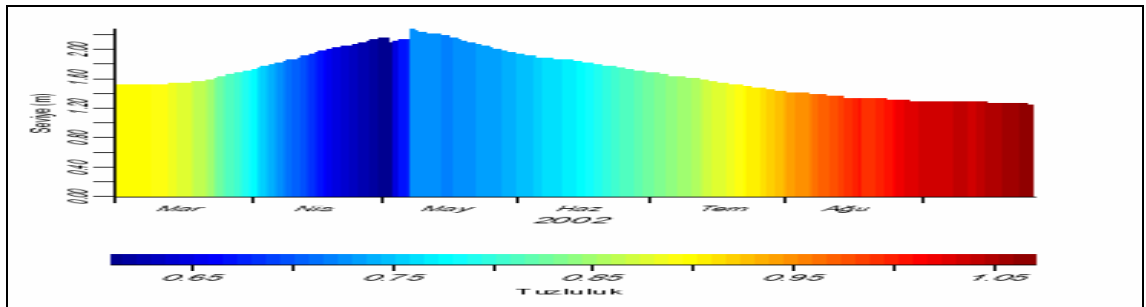
Figure 5.12 Modelled NO_3 concentrations in Eymir LakeFigure 5.13 Modelled PO_4 concentrations in Eymir Lake

Figure 5.14 Modelled salinity in Eymir Lake

In Fig. 5.15, modelled temperatures of Eymir Lake are given. Like Mogan, these values vary significantly between summer and winter sections (about $30-3=27$ °C). The difference is more in Eymir than in Mogan due to the size of the lakes.

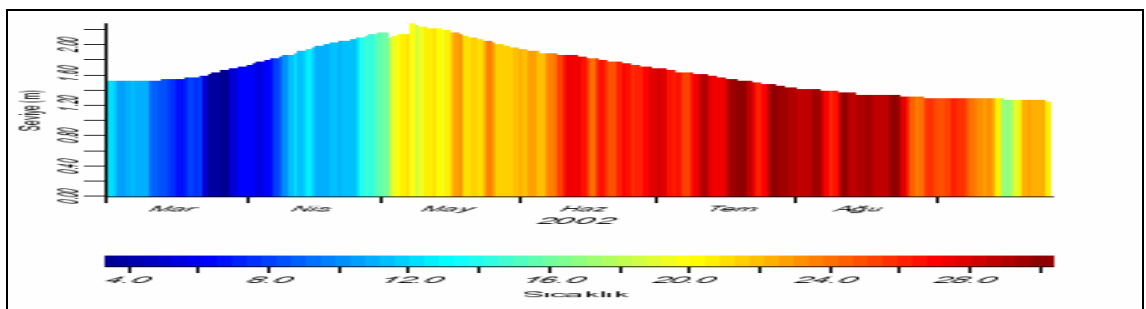


Figure 5.15 Modelled Temperatures in Eymir Lake

Eymir Lake is the property of Middle East Technical University (METU), and there is no settlement or wastewater discharge into the lake. Thus, it can be said that Mogan is the main pollution source for the Eymir Lake. Both lakes have heavier pollution loads in summer months than they do in winter.

CHAPTER SIX

CONCLUSIONS

The aim of this study was to evaluate the water quality conditions and the water budgets in Eymir-Mogan Lakes basin. To this end, the coupled lake model DYRESM-CAEDYM was applied, using the limited available data.

Since monitoring data required by the model were not available except for the period of March-September 2002, the model could not be executed for different seasons and years. Even for the specified period, some data were not available so that they had to be estimated as explained in section 4.3.1. To acquire better and more realistic modeling results in the basin, it is necessary that water quality parameters of the streams which are discharge into Eymir or Mogan Lakes are monitored on a daily basis instead of monthly. In addition, the daily water volumes of the Eymir Regulator must be gauged regularly to avoid sporadic measurements that create difficulties in modeling. The same requirement holds true for the gauging station at the Mogan Regulator. If such regular monitoring practices are adopted in the basin, the DYRESM-CAEDYM model can provide more accurate results can be.

DYRESM-CAEDYM is a practical model in the sense that it produces fairly satisfactory results, particularly in the case of water quality simulations when sufficient amounts of data are not available for calibration. DYRESM is a process-oriented model, which means that it is based on well-defined physical relationships rather than on empirical relationships so that calibration is generally not required for water budget studies.

On the other hand, the DYRESM-CAEDYM model comes in Java Language, which makes the model runs pretty cumbersome even on computers with P4 cpu. Furthermore, it has substantial data requirements, which often are not met by the monitoring practices in Turkey. The preparation of input files is also difficult as the model does not indicate possible errors in these files so that it is up to the user to bug the sources of errors. Consequently, simulation by the DYRESM-CAEDYM model may be quite time and labor consuming due to the above difficulties.

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APPENDICES

APPENDIX A
STREAM VOLUMES

YAVRUCAK Stream- YAVRUCAK FGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,004	0,088	0,285	0,285	0,285	0,520	0,285	0,115	0,006	0,003
2	0,000	0,000	0,004	0,250	0,320	0,250	0,606	0,563	0,250	0,145	0,006	0,003
3	0,000	0,000	0,004	0,180	0,360	0,250	0,400	0,440	0,215	0,145	0,006	0,004
4	0,000	0,000	0,004	0,145	0,320	0,250	0,400	0,400	0,250	0,180	0,004	0,006
5	0,000	0,000	0,004	0,145	0,360	0,215	0,480	0,400	0,285	0,180	0,004	0,014
6	0,000	0,000	0,004	0,145	0,360	0,250	1,390	0,360	0,250	0,215	0,004	0,007
7	0,000	0,000	0,004	0,145	0,320	0,215	0,735	0,400	0,215	0,145	0,006	0,039
8	0,000	0,001	0,006	0,145	0,360	0,215	0,649	0,360	0,180	0,088	0,006	0,029
9	0,000	0,001	0,004	0,145	0,360	0,215	0,563	0,320	0,180	0,115	0,004	0,021
10	0,000	0,003	0,004	0,145	0,360	0,215	0,520	0,320	0,180	0,115	0,004	0,014
11	0,000	0,003	0,004	0,145	0,400	0,215	0,520	0,320	0,180	0,480	0,004	0,021
12	0,000	0,003	0,004	0,145	0,520	0,215	0,563	0,285	0,215	0,400	0,004	0,029
13	0,000	0,000	0,006	0,145	0,400	0,180	0,520	0,320	0,180	0,606	0,004	0,039
14	0,000	0,000	0,006	0,145	0,360	0,215	0,649	0,440	0,145	0,563	0,004	0,029
15	0,000	0,000	0,003	0,145	0,360	0,180	0,520	1,100	0,115	0,400	0,001	0,021
16	0,000	0,000	0,003	0,145	0,320	0,180	0,520	0,520	0,115	0,285	0,001	0,014
17	0,000	0,000	0,006	0,145	0,320	0,180	0,786	0,440	0,072	0,180	0,001	0,029
18	0,000	0,000	0,134	0,145	0,285	0,180	0,649	0,440	0,072	0,115	0,001	0,021
19	0,000	0,001	0,049	0,145	0,320	0,215	0,649	0,360	0,088	0,072	0,001	0,021
20	0,000	0,004	0,014	0,145	0,320	0,145	0,786	0,360	0,088	0,049	0,072	0,021
21	0,000	0,006	0,014	0,215	0,320	0,215	0,649	0,320	0,088	0,039	0,049	0,014
22	0,000	0,006	0,014	0,250	0,285	0,215	0,606	0,440	0,088	0,029	0,021	0,014
23	0,000	0,004	0,014	0,250	0,285	0,215	0,563	0,837	0,072	0,021	0,007	0,014
24	0,000	0,004	0,014	0,215	0,320	0,480	0,563	0,520	0,060	0,014	0,007	0,014
25	0,000	0,006	0,014	0,180	0,320	0,649	0,563	0,400	0,072	0,014	0,007	0,014
26	0,000	0,004	0,039	0,180	0,320	0,360	0,606	0,360	0,088	0,007	0,006	0,014
27	0,000	0,003	0,029	0,180	0,320	0,320	0,520	0,320	0,115	0,007	0,006	0,007
28	0,000	0,004	0,4	0,215	0,285	0,285	0,480	0,320	0,145	0,007	0,006	0,007
29	0,000	0,004	0,215	0,180	-----	0,285	0,480	0,320	0,145	0,007	0,004	0,007
30	0,000	0,004	0,088	0,180	-----	0,250	0,520	0,285	0,115	0,006	0,003	0,007
31	0,000	-----	0,088	0,250	-----	0,285	-----	0,285	-----	0,006	0,003	-----

Çölova Stream- YAVRUCAK FGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,000	0,132	0,103	0,076	0,076	0,148	0,148	0,000	0,000	0,000
2	0,000	0,000	0,000	0,103	0,117	0,076	0,132	0,204	0,124	0,000	0,000	0,000
3	0,000	0,000	0,000	0,076	0,132	0,065	0,184	0,204	0,124	0,000	0,000	0,000
4	0,000	0,000	0,000	0,065	0,132	0,065	0,184	0,175	0,124	0,000	0,000	0,000
5	0,000	0,000	0,000	0,065	0,149	0,065	0,166	0,175	0,148	0,000	0,000	0,000
6	0,000	0,000	0,000	0,065	0,166	0,065	0,240	0,148	0,124	0,000	0,000	0,000
7	0,000	0,000	0,000	0,065	0,166	0,054	0,218	0,148	0,124	0,000	0,000	0,000
8	0,000	0,000	0,000	0,065	0,166	0,054	0,218	0,204	0,101	0,000	0,000	0,000
9	0,000	0,000	0,000	0,065	0,149	0,054	0,184	0,175	0,101	0,000	0,000	0,000
10	0,000	0,000	0,000	0,065	0,149	0,044	0,166	0,175	0,080	0,000	0,000	0,000
11	0,000	0,000	0,000	0,065	0,166	0,044	0,149	0,175	0,080	0,000	0,000	0,000
12	0,000	0,000	0,000	0,065	0,218	0,044	0,166	0,148	0,060	0,000	0,000	0,000
13	0,000	0,000	0,000	0,065	0,184	0,035	0,166	0,175	0,060	0,000	0,000	0,000
14	0,000	0,000	0,000	0,065	0,149	0,035	0,201	0,234	0,060	0,000	0,000	0,000
15	0,000	0,000	0,000	0,076	0,132	0,044	0,184	0,592	0,040	0,000	0,000	0,000
16	0,000	0,000	0,000	0,076	0,132	0,044	0,166	0,295	0,030	0,000	0,000	0,000
17	0,000	0,000	0,000	0,076	0,117	0,044	0,124	0,234	0,010	0,000	0,000	0,000
18	0,000	0,000	0,027	0,076	0,103	0,044	0,124	0,234	0,000	0,000	0,000	0,000
19	0,000	0,000	0,020	0,076	0,103	0,044	0,148	0,204	0,000	0,000	0,000	0,000
20	0,000	0,000	0,020	0,076	0,089	0,044	0,175	0,204	0,000	0,000	0,000	0,000
21	0,000	0,000	0,117	0,089	0,089	0,044	0,175	0,175	0,000	0,000	0,000	0,000
22	0,000	0,000	0,065	0,089	0,117	0,044	0,148	0,234	0,000	0,000	0,000	0,000
23	0,000	0,000	0,035	0,103	0,103	0,054	0,124	0,472	0,000	0,000	0,000	0,000
24	0,000	0,000	0,054	0,103	0,089	0,103	0,101	0,295	0,000	0,000	0,000	0,000
25	0,000	0,000	0,103	0,089	0,089	0,184	0,101	0,234	0,000	0,000	0,000	0,000
26	0,000	0,000	0,117	0,089	0,089	0,184	0,101	0,204	0,000	0,000	0,000	0,000
27	0,000	0,000	0,132	0,076	0,076	0,149	0,124	0,175	0,000	0,000	0,000	0,000
28	0,000	0,000	0,356	0,076	0,076	0,117	0,148	0,175	0,000	0,000	0,000	0,000
29	0,000	0,000	0,382	0,076	-----	0,103	0,148	0,175	0,000	0,000	0,000	0,000
30	0,000	0,000	0,201	0,089	-----	0,089	0,148	0,148	0,000	0,000	0,000	0,000
31	0,000	-----	0,166	0,103	-----	0,076	-----	0,148	-----	0,000	0,000	-----

Başpınar Stream- OĞULBEY FGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
2	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
3	0,000	0,001	0,002	0,001	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
4	0,000	0,001	0,002	0,001	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
5	0,000	0,001	0,002	0,001	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
6	0,000	0,001	0,002	0,001	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
7	0,000	0,001	0,002	0,001	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
8	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
9	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
10	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
11	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
12	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
13	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
14	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
15	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
16	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
17	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
18	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003
19	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,004
20	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,004
21	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,004
22	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,004
23	0,000	0,001	0,002	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,004
24	0,000	0,001	0,002	0,003	0,003	0,003	0,003	0,003	0,004	0,005	0,003	0,004
25	0,000	0,001	0,002	0,003	0,003	0,003	0,003	0,004	0,004	0,005	0,003	0,004
26	0,000	0,001	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,005	0,003	0,004
27	0,000	0,001	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003	0,004
28	0,000	0,001	0,002	0,003	0,003	0,003	0,003	0,004	0,005	0,004	0,003	0,004
29	0,000	0,002	0,002	0,003	-----	0,003	0,003	0,004	0,005	0,004	0,003	0,004
30	0,001	0,002	0,002	0,003	-----	0,003	0,003	0,004	0,005	0,004	0,003	0,004
31	0,001	-----	0,002	0,003	-----	0,003	-----	0,004	-----	0,004	0,003	-----

Sukesen Stream- GÖLBAŞI FGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,006	0,121	0,072	0,072	0,091	0,155	0,017	0,008	0,006	0,002
2	0,000	0,002	0,006	0,217	0,091	0,072	0,132	0,155	0,017	0,017	0,006	0,002
3	0,000	0,002	0,006	0,150	0,072	0,072	0,111	0,111	0,008	0,008	0,006	0,002
4	0,000	0,006	0,006	0,096	0,072	0,072	0,091	0,091	0,025	0,017	0,006	0,006
5	0,000	0,006	0,006	0,053	0,072	0,072	0,111	0,091	0,059	0,017	0,006	0,014
6	0,000	0,006	0,006	0,037	0,072	0,072	0,450	0,072	0,047	0,017	0,006	0,006
7	0,000	0,006	0,006	0,037	0,072	0,059	0,282	0,072	0,047	0,008	0,006	0,023
8	0,000	0,006	0,006	0,037	0,072	0,072	0,206	0,072	0,047	0,008	0,006	0,014
9	0,000	0,006	0,006	0,037	0,072	0,072	0,180	0,072	0,034	0,025	0,006	0,014
10	0,000	0,006	0,006	0,037	0,072	0,072	0,155	0,072	0,034	0,025	0,006	0,014
11	0,000	0,006	0,006	0,037	0,111	0,072	0,155	0,059	0,034	0,025	0,006	0,023
12	0,000	0,006	0,006	0,037	0,111	0,072	0,180	0,059	0,034	0,025	0,006	0,037
13	0,000	0,006	0,006	0,037	0,091	0,072	0,155	0,072	0,034	0,025	0,006	0,073
14	0,000	0,006	0,006	0,037	0,072	0,059	0,206	0,072	0,034	0,017	0,006	0,053
15	0,000	0,006	0,014	0,037	0,091	0,059	0,155	0,072	0,025	0,017	0,006	0,053
16	0,000	0,006	0,014	0,037	0,111	0,059	0,155	0,059	0,025	0,017	0,006	0,037
17	0,000	0,006	0,037	0,037	0,091	0,059	0,257	0,059	0,008	0,017	0,006	0,073
18	0,000	0,006	0,073	0,037	0,072	0,059	0,206	0,059	0,008	0,008	0,002	0,073
19	0,000	0,006	0,037	0,037	0,072	0,059	0,206	0,047	0,017	0,008	0,002	0,053
20	0,000	0,006	0,014	0,053	0,072	0,059	0,257	0,047	0,008	0,008	0,002	0,053
21	0,000	0,006	0,014	0,073	0,072	0,059	0,206	0,047	0,025	0,008	0,002	0,037
22	0,000	0,006	0,014	0,059	0,072	0,072	0,180	0,047	0,017	0,008	0,002	0,037
23	0,000	0,006	0,014	0,034	0,072	0,072	0,155	0,072	0,008	0,006	0,002	0,037
24	0,000	0,006	0,014	0,034	0,072	0,091	0,155	0,072	0,008	0,006	0,002	0,037
25	0,000	0,006	0,014	0,034	0,091	0,132	0,155	0,059	0,008	0,006	0,002	0,023
26	0,000	0,006	0,037	0,047	0,072	0,111	0,155	0,047	0,008	0,006	0,002	0,023
27	0,000	0,006	0,023	0,059	0,072	0,111	0,155	0,034	0,008	0,006	0,002	0,023
28	0,000	0,006	0,253	0,047	0,072	0,091	0,132	0,034	0,008	0,006	0,002	0,023
29	0,000	0,006	0,183	0,047	-----	0,091	0,132	0,025	0,017	0,006	0,002	0,023
30	0,000	0,006	0,150	0,059	-----	0,072	0,155	0,025	0,008	0,006	0,002	0,023
31	0,000	-----	0,121	0,072	-----	0,091	-----	0,025	-----	0,006	0,002	-----

Mogan Regulator Out FGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,000	0,000	0,000	0,000	0,000	0,093	0,020	0,001	0,000	0,000
2	0,000	0,000	0,000	0,000	0,000	0,000	0,020	1,220	0,020	0,001	0,000	0,000
3	0,000	0,000	0,000	0,000	0,000	0,000	0,000	2,450	0,020	0,001	0,000	0,000
4	0,000	0,000	0,000	0,000	0,000	0,000	0,000	1,950	0,020	0,001	0,000	0,000
5	0,000	0,000	0,000	0,000	0,000	0,000	0,000	0,020	0,020	0,001	0,000	0,000
6	0,000	0,000	0,000	0,000	0,000	0,000	0,001	0,529	0,020	0,001	0,000	0,000
7	0,000	0,000	0,000	0,000	0,000	0,000	0,000	4,110	0,020	0,001	0,000	0,000
8	0,000	0,000	0,000	0,000	0,000	0,000	0,000	0,196	0,020	0,001	0,000	0,000
9	0,000	0,000	0,000	0,000	0,000	0,000	0,000	0,020	0,020	0,000	0,000	0,000
10	0,000	0,000	0,000	0,000	0,000	0,000	0,001	0,020	0,020	0,001	0,000	0,000
11	0,000	0,000	0,000	0,000	0,000	0,000	0,000	0,020	0,020	0,000	0,000	0,000
12	0,000	0,000	0,000	0,000	0,001	0,000	0,001	0,020	0,020	0,000	0,000	0,000
13	0,000	0,000	0,000	0,000	0,001	0,000	0,001	0,020	0,020	0,000	0,000	0,000
14	0,000	0,000	0,000	0,000	0,001	0,000	0,001	0,020	0,020	0,000	0,000	0,000
15	0,000	0,000	0,000	0,000	0,000	0,000	0,001	0,020	0,020	0,000	0,000	0,000
16	0,000	0,000	0,000	0,000	0,000	0,000	0,001	0,020	0,020	0,000	0,000	0,000
17	0,000	0,000	0,000	0,000	0,000	0,000	0,001	0,020	0,020	0,000	0,000	0,000
18	0,000	0,000	0,000	0,000	0,001	0,001	0,001	0,020	0,020	0,000	0,000	0,000
19	0,000	0,000	0,000	0,000	0,001	0,001	0,001	0,020	0,003	0,000	0,000	0,000
20	0,000	0,000	0,000	0,000	0,001	0,001	0,003	0,020	0,000	0,000	0,000	0,000
21	0,000	0,000	0,000	0,000	0,001	0,001	0,000	0,020	0,000	0,000	0,000	0,000
22	0,000	0,000	0,000	0,000	0,001	0,001	0,000	0,020	0,001	0,000	0,000	0,000
23	0,000	0,000	0,000	0,000	0,001	0,001	0,000	0,020	0,001	0,000	0,000	0,000
24	0,000	0,000	0,000	0,000	0,001	0,000	0,000	0,020	0,001	0,000	0,000	0,000
25	0,000	0,000	0,000	0,000	0,001	0,000	0,000	0,020	0,000	0,000	0,000	0,000
26	0,000	0,000	0,000	0,000	0,000	0,000	0,001	0,020	0,001	0,000	0,000	0,000
27	0,000	0,000	0,000	0,000	0,000	0,000	0,340	0,020	0,001	0,000	0,000	0,000
28	0,000	0,000	0,000	0,000	0,000	0,000	0,000	0,020	0,001	0,000	0,000	0,000
29	0,000	0,000	0,000	0,000	-----	0,000	0,001	0,020	0,001	0,000	0,000	0,000
30	0,000	0,000	0,000	0,000	-----	0,000	0,003	0,020	0,001	0,000	0,000	0,000
31	0,000	-----	0,000	0,000	-----	0,000	-----	0,020	-----	0,000	0,000	-----

Tatlim Stream - Hacilar MFGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
2	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
3	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
4	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
5	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
6	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
7	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
8	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
9	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
10	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
11	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
12	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
13	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
14	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
15	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
16	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
17	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
18	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
19	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
20	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
21	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
22	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
23	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
24	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
25	0,000	0,001	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001
26	0,000	0,001	0,001	0,001	0,002	0,001	0,001	0,001	0,001	0,001	0,001	0,001
27	0,000	0,001	0,001	0,002	0,002	0,001	0,001	0,001	0,001	0,001	0,001	0,001
28	0,000	0,001	0,001	0,002	0,002	0,001	0,001	0,002	0,001	0,001	0,001	0,001
29	0,000	0,001	0,001	0,002	-----	0,001	0,001	0,002	0,001	0,001	0,001	0,001
30	0,000	0,001	0,001	0,002	-----	0,001	0,001	0,002	0,001	0,001	0,001	0,001
31	0,000	-----	0,001	0,002	-----	0,001	-----	0,002	-----	0,001	0,001	-----

Çolakpınar Stream - Besihane MFGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,000	0,001	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
2	0,000	0,000	0,000	0,001	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
3	0,000	0,000	0,000	0,001	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
4	0,000	0,000	0,000	0,001	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
5	0,000	0,000	0,000	0,001	0,004	0,002	0,003	0,003	0,002	0,002	0,002	0,002
6	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
7	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
8	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
9	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
10	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
11	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
12	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
13	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
14	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
15	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
16	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
17	0,000	0,000	0,000	0,001	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
18	0,000	0,000	0,000	0,002	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
19	0,000	0,000	0,000	0,002	0,004	0,001	0,003	0,003	0,002	0,002	0,002	0,002
20	0,000	0,000	0,000	0,002	0,003	0,001	0,003	0,003	0,002	0,002	0,002	0,002
21	0,000	0,000	0,000	0,002	0,003	0,001	0,003	0,003	0,002	0,002	0,002	0,002
22	0,000	0,000	0,000	0,002	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
23	0,000	0,000	0,001	0,002	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
24	0,000	0,000	0,001	0,002	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
25	0,000	0,000	0,001	0,002	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
26	0,000	0,000	0,001	0,002	0,003	0,002	0,003	0,003	0,002	0,002	0,002	0,002
27	0,000	0,000	0,001	0,003	0,002	0,002	0,003	0,003	0,002	0,002	0,002	0,002
28	0,000	0,000	0,001	0,003	0,002	0,002	0,003	0,002	0,002	0,002	0,002	0,002
29	0,000	0,000	0,001	0,003	-----	0,002	0,003	0,002	0,002	0,002	0,002	0,002
30	0,000	0,000	0,001	0,003	-----	0,002	0,003	0,002	0,002	0,002	0,002	0,002
31	0,000	-----	0,001	0,003	-----	0,003	-----	0,002	-----	0,002	0,002	-----

Kışlak Stream - Eymir MFGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,000	0,064	0,052	0,043	0,173	0,089	0,015	0,000	0,000	0,000
2	0,000	0,000	0,000	0,068	0,049	0,044	0,179	0,082	0,014	0,000	0,000	0,000
3	0,000	0,000	0,000	0,071	0,047	0,046	0,184	0,075	0,013	0,000	0,000	0,000
4	0,000	0,000	0,000	0,075	0,045	0,047	0,190	0,068	0,012	0,000	0,000	0,000
5	0,000	0,000	0,000	0,079	0,043	0,049	0,196	0,061	0,011	0,000	0,000	0,000
6	0,000	0,000	0,000	0,082	0,040	0,050	0,202	0,054	0,010	0,000	0,000	0,000
7	0,000	0,000	0,000	0,086	0,038	0,052	0,207	0,046	0,008	0,000	0,000	0,000
8	0,000	0,000	0,000	0,089	0,036	0,053	0,213	0,039	0,006	0,000	0,000	0,000
9	0,000	0,000	0,000	0,093	0,033	0,055	0,219	0,038	0,004	0,000	0,000	0,000
10	0,000	0,000	0,000	0,096	0,031	0,056	0,224	0,037	0,002	0,000	0,000	0,000
11	0,000	0,000	0,000	0,100	0,029	0,058	0,231	0,036	0,001	0,000	0,000	0,000
12	0,000	0,000	0,000	0,098	0,026	0,059	0,224	0,035	0,000	0,000	0,000	0,000
13	0,000	0,000	0,000	0,095	0,024	0,065	0,217	0,034	0,000	0,000	0,000	0,000
14	0,000	0,000	0,000	0,093	0,021	0,070	0,210	0,033	0,000	0,000	0,000	0,000
15	0,000	0,000	0,004	0,091	0,022	0,076	0,203	0,032	0,000	0,000	0,000	0,000
16	0,000	0,000	0,007	0,089	0,024	0,082	0,196	0,031	0,000	0,000	0,000	0,000
17	0,000	0,000	0,011	0,086	0,025	0,088	0,188	0,030	0,000	0,000	0,000	0,000
18	0,000	0,000	0,014	0,084	0,027	0,094	0,181	0,029	0,000	0,000	0,000	0,000
19	0,000	0,000	0,018	0,082	0,028	0,099	0,174	0,028	0,000	0,000	0,000	0,000
20	0,000	0,000	0,021	0,079	0,030	0,105	0,167	0,027	0,000	0,000	0,000	0,000
21	0,000	0,000	0,025	0,077	0,031	0,110	0,160	0,026	0,000	0,000	0,000	0,000
22	0,000	0,000	0,029	0,075	0,033	0,116	0,153	0,025	0,000	0,000	0,000	0,000
23	0,000	0,000	0,032	0,072	0,034	0,122	0,146	0,024	0,000	0,000	0,000	0,000
24	0,000	0,000	0,036	0,070	0,036	0,127	0,139	0,023	0,000	0,000	0,000	0,000
25	0,000	0,000	0,039	0,068	0,037	0,133	0,132	0,022	0,000	0,000	0,000	0,000
26	0,000	0,000	0,043	0,066	0,039	0,139	0,125	0,021	0,000	0,000	0,000	0,000
27	0,000	0,000	0,046	0,063	0,040	0,145	0,117	0,020	0,000	0,000	0,000	0,000
28	0,000	0,000	0,050	0,061	0,041	0,150	0,110	0,019	0,000	0,000	0,000	0,000
29	0,000	0,000	0,054	0,059	-----	0,156	0,103	0,018	0,000	0,000	0,000	0,000
30	0,000	0,000	0,057	0,056	-----	0,162	0,096	0,017	0,000	0,000	0,000	0,000
31	0,000	-----	0,061	0,054	-----	0,167	-----	0,016	-----	0,000	0,000	-----

Yağlıpınar Stream - Yağlıpınar MFGS 2002												
	Ekim	Kasım	Aralık	Ocak	Şubat	Mart	Nisan	Mayıs	Haziran	Temmuz	Ağustos	Eylül
1	0,000	0,000	0,001	0,001	0,002	0,002	0,001	0,001	0,000	0,000	0,000	0,000
2	0,000	0,000	0,001	0,001	0,003	0,002	0,001	0,001	0,000	0,000	0,000	0,000
3	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
4	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
5	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
6	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
7	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
8	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
9	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
10	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
11	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
12	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
13	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
14	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
15	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
16	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
17	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
18	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
19	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
20	0,000	0,000	0,001	0,001	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
21	0,000	0,000	0,001	0,002	0,003	0,001	0,001	0,001	0,000	0,000	0,000	0,000
22	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,001	0,000	0,000	0,000	0,000
23	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,001	0,000	0,000	0,000	0,000
24	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,001	0,000	0,000	0,000	0,000
25	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,001	0,000	0,000	0,000	0,000
26	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,001	0,000	0,000	0,000	0,000
27	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,001	0,000	0,000	0,000	0,000
28	0,000	0,000	0,001	0,002	0,002	0,001	0,001	0,000	0,000	0,000	0,000	0,000
29	0,000	0,001	0,001	0,002	-----	0,001	0,001	0,000	0,000	0,000	0,000	0,000
30	0,000	0,001	0,001	0,002	-----	0,001	0,001	0,000	0,000	0,000	0,000	0,000
31	0,000	-----	0,001	0,002	-----	0,001	-----	0,000	-----	0,000	0,000	-----

APPENDIX B
METEOROLOGICAL DATA

Date	Shortwave Radiation (Wm ⁻²)	Cloud Cover (%)	Temperature (C)	Vapour Pressure (mb)	Wind Speed (m/s)	Rain (m)
01.03.2002	211,8	0,27	4,71	5,03	3,79	0
02.03.2002	213	0,22	8,01	5,79	3,06	0
03.03.2002	221	0,24	7,52	5,82	5,2	0
04.03.2002	194,8	0,30	4,62	5,17	4,17	0
05.03.2002	218,9	0,18	7,09	5,04	2,02	0
06.03.2002	208,9	0,12	7,64	4,51	2,14	0
07.03.2002	207,7	0,15	9,16	5,44	3,68	0
08.03.2002	202,4	0,11	10,02	5,21	5,05	0
09.03.2002	222,7	0,19	8,04	5,51	3,55	0
10.03.2002	209,6	0,64	-0,06	3,34	1,82	0
11.03.2002	114,4	0,55	0,78	4,99	3,56	0
12.03.2002	231,1	0,32	4,32	5,19	4,35	0
13.03.2002	151,6	0,20	6,69	5,10	2,67	0,0015
14.03.2002	180	0,22	6,55	5,22	3,06	0,0001
15.03.2002	154,8	0,46	1,60	4,95	1,77	0
16.03.2002	163,8	0,45	-3,58	3,34	2,26	0
17.03.2002	204,6	0,46	-1,64	3,91	4,89	0
18.03.2002	165,5	0,88	0,54	5,98	1,75	0
19.03.2002	145,1	0,64	5,92	7,68	2,96	0
20.03.2002	237,8	0,70	5,56	7,75	4,63	0
21.03.2002	154,4	0,76	2,82	6,63	6,15	0,0031
22.03.2002	244,7	0,78	-1,36	4,96	4,03	0
23.03.2002	59,2	0,63	-0,47	4,83	10,64	0,0186
24.03.2002	99,5	0,37	1,86	4,62	6,27	0,0124
25.03.2002	167,5	0,39	5,99	6,29	9,36	0,0008
26.03.2002	155,8	0,42	0,90	4,53	7,06	0,0008
27.03.2002	155,6	0,25	0,61	3,62	4,95	0
28.03.2002	163,8	0,12	5,41	3,92	4,25	0
29.03.2002	208,3	0,77	5,64	8,13	4,11	0
30.03.2002	117,2	0,69	6,16	8,01	2,45	0,0003
31.03.2002	190,9	0,70	5,41	7,68	4,75	0,0005
01.04.2002	122,9	0,57	5,75	7,20	4,85	0,0054
02.04.2002	148,2	0,72	4,25	7,15	2,39	0,0097
03.04.2002	131,4	0,51	5,30	6,69	2,03	0,0006
04.04.2002	36,4	0,57	5,76	7,19	1,21	0,0029
05.04.2002	181,4	0,59	6,02	7,45	6,76	0,0028
06.04.2002	145	0,66	6,46	8,06	5,13	0,0041
07.04.2002	217,6	0,45	5,96	6,64	5,38	0,0016
08.04.2002	288,9	0,19	7,10	5,20	5,1	0,0017
09.04.2002	227,4	0,13	9,05	5,17	2,65	0
10.04.2002	280,4	0,09	11,61	5,49	1,3	0
11.04.2002	220,8	0,11	12,70	6,24	1,82	0,0014
12.04.2002	241,9	0,51	9,00	8,62	1,8	0
13.04.2002	117,4	0,56	6,26	7,41	3,79	0,0028
14.04.2002	263,8	0,50	7,69	7,81	3,49	0,0001
15.04.2002	282,4	0,57	6,75	7,72	2,45	0
16.04.2002	96,1	0,41	8,31	7,54	3,49	0,015
17.04.2002	133,6	0,28	10,92	7,72	3,67	0,0014
18.04.2002	126,5	0,23	14,02	8,78	2,58	0,0009
19.04.2002	111,5	0,13	15,45	7,82	2,6	0,0079
20.04.2002	240,5	0,20	9,33	6,16	3,42	0,0017
21.04.2002	170,3	0,26	9,30	6,71	4,45	0,0022
22.04.2002	175,5	0,24	6,75	5,50	2,83	0
23.04.2002	246,3	0,16	6,60	4,67	1,47	0
24.04.2002	149,2	0,14	10,97	6,08	2,32	0,0004
25.04.2002	183,6	0,25	13,36	8,70	3,03	0,0086
26.04.2002	187	0,14	15,58	8,19	1,63	0,0027
27.04.2002	267,9	0,22	14,63	8,95	1,58	0,0025
28.04.2002	238,6	0,22	13,45	8,36	1,3	0
29.04.2002	129,7	0,29	11,10	7,90	2,26	0,0081
30.04.2002	280,9	0,29	10,60	7,69	1,22	0

Date	Shortwave Radiation (Wm ⁻²)	Cloud Cover (%)	Temperature (C)	Vapour Pressure (mb)	Wind Speed (m/s)	Rain (m)
01.05.2002	182,8	0,19	14,25	8,34	2,99	0,0131
02.05.2002	236,7	0,26	15,46	10,07	3,45	0,0004
03.05.2002	334,9	0,21	17,09	10,34	1,76	0
04.05.2002	318,7	0,24	14,95	9,46	2,44	0
05.05.2002	287,7	0,14	14,59	7,61	1,99	0
06.05.2002	249,2	0,18	17,27	9,87	1,46	0
07.05.2002	291,5	0,32	12,02	8,76	3,23	0
08.05.2002	344,9	0,39	3,80	5,40	5,04	0
09.05.2002	264,6	0,18	5,49	4,52	1,65	0,0009
10.05.2002	349,5	0,10	10,87	5,31	2	0
11.05.2002	351,4	0,06	14,44	5,67	1,58	0
12.05.2002	239,1	0,07	15,81	6,46	2,01	0
13.05.2002	261,4	0,08	17,21	7,37	2,38	0,0001
14.05.2002	207,7	0,24	16,13	10,28	4,75	0,0165
15.05.2002	214,5	0,22	17,08	10,51	3,85	0
16.05.2002	338,7	0,13	19,45	10,12	2,38	0
17.05.2002	307,9	0,18	18,25	10,54	1,78	0
18.05.2002	361,4	0,35	13,49	9,96	2,12	0
19.05.2002	358,1	0,08	12,44	5,47	2,48	0
20.05.2002	279,8	0,23	7,59	5,71	5,66	0
21.05.2002	365,2	0,07	11,41	4,93	2,12	0
22.05.2002	315,7	0,03	17,93	5,72	4,35	0
23.05.2002	298,3	0,14	19,37	10,26	6,55	0
24.05.2002	366,1	0,14	18,33	9,78	2,93	0
25.05.2002	361,1	0,39	13,60	10,45	1,79	0
26.05.2002	206,6	0,32	12,41	8,96	3,65	0,0017
27.05.2002	232,3	0,35	11,57	8,74	3,93	0,0038
28.05.2002	323,9	0,19	13,97	8,16	2,96	0
29.05.2002	281,2	0,14	16,04	8,27	4,05	0
30.05.2002	321,7	0,18	15,74	8,94	4,02	0
31.05.2002	363,4	0,14	14,87	7,82	4,25	0
01.06.2002	367,1	0,18	14,29	8,22	4,06	0
02.06.2002	330,5	0,12	15,49	7,56	4,68	0
03.06.2002	356,8	0,43	14,24	11,34	2,56	0
04.06.2002	361,8	0,45	13,64	11,11	6,12	0
05.06.2002	370,6	0,31	15,68	10,92	7,06	0
06.06.2002	280,9	0,28	17,25	11,59	4,39	0
07.06.2002	369	0,35	15,54	11,38	2,1	0
08.06.2002	270,2	0,34	15,83	11,42	2,93	0
09.06.2002	282	0,30	15,44	10,60	2,11	0
10.06.2002	370,5	0,69	12,35	12,16	1,66	0
11.06.2002	370,5	0,57	14,31	12,78	2,11	0
12.06.2002	370,2	0,54	15,86	13,78	3,01	0
13.06.2002	357,7	0,48	15,57	12,93	2,92	0
14.06.2002	333,2	0,51	15,86	13,49	3,11	0
15.06.2002	331,5	0,51	16,01	13,64	4,65	0
16.06.2002	314,6	0,46	17,09	13,95	6,1	0
17.06.2002	261,3	0,37	18,80	14,33	4,81	0
18.06.2002	367,2	0,19	21,28	13,05	1,73	0
19.06.2002	354,6	0,08	23,14	10,77	4,16	0
20.06.2002	344,3	0,22	21,87	14,04	8,2	0
21.06.2002	366,8	0,23	18,80	11,93	5,07	0
22.06.2002	346,6	0,08	21,00	9,45	4,13	0
23.06.2002	366,9	0,15	21,49	12,07	2,32	0
24.06.2002	365,1	0,22	17,36	10,64	3,03	0
25.06.2002	335,2	0,50	13,68	11,62	3,89	0
26.06.2002	350	0,50	14,70	12,46	3,59	0
27.06.2002	369,4	0,44	14,83	11,93	3,26	0
28.06.2002	368,7	0,33	16,83	12,02	3,58	0
29.06.2002	370,4	0,21	19,59	11,99	3,14	0
30.06.2002	364,5	0,18	20,28	11,83	2,25	0

Date	Shortwave Radiation (Wm ⁻²)	Cloud Cover (%)	Temperature (C)	Vapour Pressure (mb)	Wind Speed (m/s)	Rain (m)
01.07.2002	318,8	0,25	18,79	12,20	3,26	0
02.07.2002	344,5	0,37	17,74	13,31	2,35	0
03.07.2002	307,5	0,25	19,51	12,76	3,48	0,0002
04.07.2002	236,6	0,16	20,31	11,52	3,53	0
05.07.2002	261,2	0,18	21,10	12,46	3,03	0
06.07.2002	347,6	0,17	21,78	12,84	3,61	0
07.07.2002	187,3	0,20	20,78	12,74	3,78	0,0057
08.07.2002	296,8	0,34	19,22	14,13	4,18	0
09.07.2002	349,5	0,29	20,48	14,45	2,02	0
10.07.2002	317	0,10	23,61	11,75	3,05	0
11.07.2002	353	0,09	25,93	13,08	2,63	0
12.07.2002	295,2	0,06	26,26	11,61	3,59	0
13.07.2002	231,6	0,09	23,96	11,67	3,13	0,0004
14.07.2002	329,5	0,07	22,88	10,09	4,39	0
15.07.2002	341,1	0,05	21,48	8,37	3,18	0
16.07.2002	314,5	0,10	23,10	11,40	2,99	0
17.07.2002	342,1	0,34	19,13	14,11	1,55	0
18.07.2002	329,4	0,33	19,48	14,31	2	0
19.07.2002	337	0,51	17,95	15,42	2,75	0
20.07.2002	345,5	0,42	17,57	13,90	1,77	0
21.07.2002	315,6	0,24	18,21	11,70	2,89	0
22.07.2002	309,2	0,16	18,29	10,08	3,37	0
23.07.2002	318,6	0,13	19,13	10,03	3,79	0
24.07.2002	296	0,11	19,92	9,72	4,36	0,0002
25.07.2002	344	0,10	21,39	10,50	1,81	0
26.07.2002	307,7	0,11	22,79	11,67	1,38	0
27.07.2002	314,8	0,04	26,00	10,35	1,65	0
28.07.2002	330,1	0,03	27,20	10,71	4,07	0
29.07.2002	298,4	0,19	22,80	14,25	2,77	0
30.07.2002	336,5	0,17	22,64	13,55	3,44	0
31.07.2002	283,5	0,22	22,57	14,75	3,4	0
01.08.2002	334,4	0,25	22,29	15,29	3,46	0
02.08.2002	296,7	0,26	22,11	15,34	3,11	0
03.08.2002	295,2	0,39	21,17	16,87	3,19	0
04.08.2002	286,4	0,47	20,70	17,66	2,72	0
05.08.2002	318,7	0,46	20,77	17,66	2,35	0
06.08.2002	280,5	0,39	20,23	15,88	2,81	0,0036
07.08.2002	287,3	0,28	19,65	13,57	3,09	0
08.08.2002	282	0,09	20,75	9,74	4,54	0
09.08.2002	277,2	0,08	22,43	10,52	3,92	0
10.08.2002	299,3	0,06	23,39	10,09	1,97	0
11.08.2002	324,4	0,12	22,52	11,92	2,13	0
12.08.2002	306,8	0,18	22,41	13,71	1,14	0
13.08.2002	265,4	0,07	24,94	11,44	4	0,0005
14.08.2002	294,3	0,03	26,93	9,99	3,68	0
15.08.2002	306,1	0,13	24,32	13,43	2,37	0
16.08.2002	262,9	0,26	22,49	15,67	2,68	0
17.08.2002	292,7	0,24	21,59	14,38	2,16	0
18.08.2002	253,7	0,06	23,51	10,33	2,22	0
19.08.2002	193,8	0,03	25,37	9,44	1,58	0,022
20.08.2002	161,5	0,01	27,43	8,90	1,21	0,0003
21.08.2002	218,9	0,02	27,41	9,18	2,1	0
22.08.2002	285,1	0,02	25,33	8,66	2	0
23.08.2002	241,4	0,04	24,39	9,35	1,54	0
24.08.2002	262,8	0,37	19,30	14,76	2,22	0
25.08.2002	280,3	0,60	16,48	15,00	4,16	0
26.08.2002	249,2	0,66	12,90	12,37	3,26	0
27.08.2002	292	0,34	14,84	10,72	4,3	0
28.08.2002	293,2	0,37	13,24	9,97	3,49	0
29.08.2002	304,2	0,45	13,31	10,92	2,21	0
30.08.2002	292,7	0,30	15,16	10,42	0,92	0
31.08.2002	221,2	0,22	16,87	10,36	0,92	0

Date	Shortwave Radiation (Wm ⁻²)	Cloud Cover (%)	Temperature (C)	Vapour Pressure (mb)	Wind Speed (m/s)	Rain (m)
01.09.2002	192,4	0,10	19,37	9,17	2,56	0
02.09.2002	236,3	0,08	21,31	9,77	2,45	0
03.09.2002	187	0,38	17,18	13,10	1,43	0,0034
04.09.2002	228	0,26	18,80	12,49	1,64	0,0041
05.09.2002	257,1	0,39	18,77	14,53	1,62	0
06.09.2002	171,5	0,55	16,01	14,03	1,91	0,0052
07.09.2002	258,8	0,40	14,00	10,81	1,64	0
08.09.2002	179	0,37	13,99	10,49	1	0,001
09.09.2002	166,9	0,17	16,44	9,24	1,57	0,0002
10.09.2002	156,5	0,15	17,58	9,43	1,07	0
11.09.2002	166,6	0,23	17,46	10,86	1,88	0,0045
12.09.2002	177,5	0,25	17,34	11,23	1,81	0,005
13.09.2002	222,9	0,35	15,83	11,55	2,1	0
14.09.2002	191,6	0,28	17,17	11,55	3,52	0
15.09.2002	149,4	0,56	13,31	11,86	3,58	0,0003
16.09.2002	144,7	0,24	13,18	8,52	7,34	0,0066
17.09.2002	225,6	0,15	13,63	7,39	3,21	0
18.09.2002	215,1	0,08	15,51	6,76	3,17	0
19.09.2002	252,9	0,05	18,33	6,82	2,04	0
20.09.2002	247,8	0,05	18,79	7,31	0,92	0
21.09.2002	245,4	0,27	16,71	11,05	1,55	0
22.09.2002	240,5	0,25	14,32	9,25	1,96	0
23.09.2002	232,5	0,11	14,42	6,99	2,22	0
24.09.2002	232,8	0,03	17,69	6,06	2,11	0
25.09.2002	228,5	0,13	16,82	8,57	2,77	0
26.09.2002	190,8	0,13	14,88	7,66	4,02	0
27.09.2002	165,1	0,10	15,59	7,24	4,12	0
28.09.2002	190,4	0,05	18,51	7,14	1,57	0,0007
29.09.2002	153,5	0,04	20,24	7,15	2,78	0
30.09.2002	210,1	0,01	21,50	5,71	1,66	0,0029
01.10.2002	226,3	0,01	21,14	5,19	1,983	0
02.10.2002	188,9	0,01	22,31	6,01	2,155	0
03.10.2002	202,2	0,02	21,65	6,40	1,507	0
04.10.2002	205,5	0,02	21,29	6,74	1,921	0
05.10.2002	209	0,01	20,87	5,27	1,243	0
06.10.2002	205,1	0,01	20,66	5,83	1,581	0
07.10.2002	196,3	0,05	20,02	7,53	2,089	0
08.10.2002	185,3	0,09	19,77	9,08	1,727	0
09.10.2002	165,5	0,47	15,31	12,58	5,304	0,0444
10.10.2002	76,4	0,76	8,40	9,74	4,388	0,0018
11.10.2002	176	0,50	9,38	8,72	2,348	0
12.10.2002	165,4	0,50	6,18	7,07	4,452	0
13.10.2002	210,2	0,30	7,58	6,35	1,303	0
14.10.2002	204,9	0,18	11,22	6,72	1,397	0
15.10.2002	195,7	0,14	12,62	6,78	1,887	0
16.10.2002	192,9	0,31	11,02	8,05	4,121	0
17.10.2002	107,9	0,30	8,47	6,77	1,824	0,0007
18.10.2002	39,05	0,77	8,29	9,71	1,377	0,0034
19.10.2002	119	0,53	7,09	7,66	1,782	0
20.10.2002	178,9	0,37	10,84	8,60	3,543	0
21.10.2002	149,2	0,46	13,16	10,91	3,889	0,0065
22.10.2002	166,9	0,51	12,05	10,56	2,593	0
23.10.2002	129,1	0,56	10,81	10,09	1,377	0,0012
24.10.2002	34,54	0,86	10,63	11,90	1,77	0,0058
25.10.2002	65,04	0,77	8,85	10,12	1,093	0,0001
26.10.2002	158,5	0,49	8,95	8,44	1,322	0
27.10.2002	172,2	0,46	10,57	9,15	1,87	0
28.10.2002	163,1	0,36	12,92	9,71	4,397	0,0007
29.10.2002	84,3	0,51	6,81	7,39	4,111	0
30.10.2002	157,6	0,50	5,83	6,85	3,339	0
31.10.2002	97,1	0,47	5,14	6,40	4,014	0

APPENDICES C
QUALITY DATAS

Yavrucak Stream

Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄	Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄
01.03.2002	3,3	0	8,38	11,8	0,09	4,5	0,11	01.05.2002	4,8	0	8,36	6,3	0,12	4,4	0,09
02.03.2002	3,45	0	8,39	11,78	0,09	4,48	0,11	02.05.2002	5,02	0	8,36	6,4	0,12	4,37	0,09
03.03.2002	3,6	0	8,39	11,76	0,08	4,47	0,11	03.05.2002	5,25	0	8,36	6,51	0,11	4,34	0,09
04.03.2002	3,75	0	8,4	11,74	0,08	4,45	0,11	04.05.2002	5,47	0	8,36	6,61	0,11	4,3	0,09
05.03.2002	3,91	0	8,41	11,71	0,08	4,44	0,12	05.05.2002	5,69	0	8,36	6,71	0,11	4,27	0,08
06.03.2002	4,06	0	8,42	11,69	0,08	4,42	0,12	06.05.2002	5,91	0	8,36	6,82	0,11	4,24	0,08
07.03.2002	4,21	0	8,42	11,67	0,07	4,4	0,12	07.05.2002	6,14	0	8,36	6,92	0,1	4,21	0,08
08.03.2002	4,36	0	8,43	11,65	0,07	4,39	0,12	08.05.2002	6,36	0	8,36	7,02	0,1	4,17	0,08
09.03.2002	4,51	0	8,44	11,63	0,07	4,37	0,12	09.05.2002	6,58	0	8,36	7,13	0,1	4,14	0,08
10.03.2002	4,66	0	8,45	11,61	0,07	4,35	0,12	10.05.2002	6,8	0	8,36	7,23	0,1	4,11	0,08
11.03.2002	4,82	0	8,45	11,58	0,06	4,34	0,13	11.05.2002	7,03	0	8,36	7,33	0,09	4,08	0,08
12.03.2002	4,97	0	8,46	11,56	0,06	4,32	0,13	12.05.2002	7,25	0	8,36	7,44	0,09	4,05	0,08
13.03.2002	5,12	0	8,47	11,54	0,06	4,31	0,13	13.05.2002	7,47	0	8,36	7,54	0,09	4,01	0,07
14.03.2002	5,27	0	8,48	11,52	0,06	4,29	0,13	14.05.2002	7,69	0	8,36	7,64	0,09	3,98	0,07
15.03.2002	5,42	0	8,48	11,5	0,05	4,27	0,13	15.05.2002	7,92	0	8,36	7,75	0,08	3,95	0,07
16.03.2002	5,57	0	8,49	11,48	0,05	4,26	0,13	16.05.2002	8,14	0	8,36	7,85	0,08	3,92	0,07
17.03.2002	5,73	0	8,5	11,45	0,05	4,24	0,14	17.05.2002	8,36	0	8,37	7,95	0,08	3,88	0,07
18.03.2002	5,88	0	8,51	11,43	0,05	4,23	0,14	18.05.2002	8,58	0	8,37	8,05	0,08	3,85	0,07
19.03.2002	6,03	0	8,51	11,41	0,04	4,21	0,14	19.05.2002	8,81	0	8,37	8,16	0,07	3,82	0,07
20.03.2002	6,18	0	8,52	11,39	0,04	4,19	0,14	20.05.2002	9,03	0	8,37	8,26	0,07	3,79	0,07
21.03.2002	6,33	0	8,53	11,37	0,04	4,18	0,14	21.05.2002	9,25	0	8,37	8,36	0,07	3,75	0,06
22.03.2002	6,48	0	8,54	11,35	0,04	4,16	0,14	22.05.2002	9,47	0	8,37	8,47	0,07	3,72	0,06
23.03.2002	6,64	0	8,54	11,32	0,03	4,15	0,15	23.05.2002	9,7	0	8,37	8,57	0,06	3,69	0,06
24.03.2002	6,79	0	8,55	11,3	0,03	4,13	0,15	24.05.2002	9,92	0	8,37	8,67	0,06	3,66	0,06
25.03.2002	6,94	0	8,56	11,28	0,03	4,11	0,15	25.05.2002	10,14	0	8,37	8,78	0,06	3,63	0,06
26.03.2002	7,09	0	8,57	11,26	0,03	4,1	0,15	26.05.2002	10,36	0	8,37	8,88	0,06	3,59	0,06
27.03.2002	7,24	0	8,57	11,24	0,02	4,08	0,15	27.05.2002	10,59	0	8,37	8,98	0,05	3,56	0,06
28.03.2002	7,39	0	8,58	11,22	0,02	4,06	0,15	28.05.2002	10,81	0	8,37	9,09	0,05	3,53	0,06
29.03.2002	7,55	0	8,59	11,19	0,02	4,05	0,16	29.05.2002	11,03	0	8,37	9,19	0,05	3,5	0,05
30.03.2002	7,7	0	8,6	11,17	0,02	4,03	0,16	30.05.2002	11,25	0	8,37	9,29	0,05	3,46	0,05
31.03.2002	7,85	0	8,6	11,15	0,01	4,02	0,16	31.05.2002	11,48	0	8,37	9,4	0,04	3,43	0,05
01.04.2002	8	0	8,61	11,13	0,01	4	0,16	01.06.2002	11,7	0	8,37	9,5	0,04	3,4	0,05
02.04.2002	7,89	0	8,6	10,97	0,01	4,01	0,16	02.06.2002	11,84	0	8,37	9,5	0,04	3,37	0,05
03.04.2002	7,79	0	8,59	10,81	0,02	4,03	0,16	03.06.2002	11,97	0	8,37	9,51	0,04	3,35	0,05
04.04.2002	7,68	0	8,58	10,65	0,02	4,04	0,15	04.06.2002	12,11	0	8,36	9,51	0,04	3,32	0,05
05.04.2002	7,57	0	8,58	10,49	0,02	4,05	0,15	05.06.2002	12,25	0	8,36	9,52	0,04	3,29	0,05
06.04.2002	7,47	0	8,57	10,33	0,03	4,07	0,15	06.06.2002	12,38	0	8,36	9,52	0,05	3,27	0,05
07.04.2002	7,36	0	8,56	10,16	0,03	4,08	0,15	07.06.2002	12,52	0	8,36	9,52	0,05	3,24	0,05
08.04.2002	7,25	0	8,55	10	0,04	4,09	0,14	08.06.2002	12,66	0	8,35	9,53	0,05	3,21	0,05
09.04.2002	7,15	0	8,54	9,84	0,04	4,11	0,14	09.06.2002	12,79	0	8,35	9,53	0,05	3,19	0,05
10.04.2002	7,04	0	8,54	9,68	0,04	4,12	0,14	10.06.2002	12,93	0	8,35	9,54	0,05	3,16	0,05
11.04.2002	6,93	0	8,53	9,52	0,05	4,13	0,14	11.06.2002	13,07	0	8,35	9,54	0,05	3,13	0,05
12.04.2002	6,83	0	8,52	9,36	0,05	4,15	0,13	12.06.2002	13,2	0	8,34	9,54	0,05	3,11	0,05
13.04.2002	6,72	0	8,51	9,2	0,05	4,16	0,13	13.06.2002	13,34	0	8,34	9,55	0,05	3,08	0,05
14.04.2002	6,61	0	8,5	9,04	0,06	4,17	0,13	14.06.2002	13,48	0	8,34	9,55	0,05	3,05	0,05
15.04.2002	6,51	0	8,49	8,88	0,06	4,19	0,13	15.06.2002	13,61	0	8,34	9,56	0,05	3,03	0,05
16.04.2002	6,4	0	8,49	8,72	0,07	4,2	0,13	16.06.2002	13,75	0	8,34	9,56	0,06	3	0,05
17.04.2002	6,29	0	8,48	8,55	0,07	4,21	0,12	17.06.2002	13,89	0	8,33	9,56	0,06	2,97	0,05
18.04.2002	6,19	0	8,47	8,39	0,07	4,23	0,12	18.06.2002	14,02	0	8,33	9,57	0,06	2,95	0,05
19.04.2002	6,08	0	8,46	8,23	0,08	4,24	0,12	19.06.2002	14,16	0	8,33	9,57	0,06	2,92	0,05
20.04.2002	5,97	0	8,45	8,07	0,08	4,25	0,12	20.06.2002	14,3	0	8,33	9,58	0,06	2,89	0,05
21.04.2002	5,87	0	8,44	7,91	0,08	4,27	0,11	21.06.2002	14,43	0	8,32	9,58	0,06	2,87	0,05
22.04.2002	5,76	0	8,43	7,75	0,09	4,28	0,11	22.06.2002	14,57	0	8,32	9,58	0,06	2,84	0,05
23.04.2002	5,65	0	8,43	7,59	0,09	4,29	0,11	23.06.2002	14,71	0	8,32	9,59	0,06	2,81	0,05
24.04.2002	5,55	0	8,42	7,43	0,09	4,31	0,11	24.06.2002	14,84	0	8,32	9,59	0,06	2,79	0,05
25.04.2002	5,44	0	8,41	7,27	0,1	4,32	0,1	25.06.2002	14,98	0	8,31	9,6	0,06	2,76	0,05
26.04.2002	5,33	0	8,4	7,11	0,1	4,33	0,1	26.06.2002	15,12	0	8,31	9,6	0,07	2,73	0,05
27.04.2002	5,23	0	8,39	6,94	0,11	4,35	0,1	27.06.2002	15,25	0	8,31	9,6	0,07	2,71	0,05
28.04.2002	5,12	0	8,39	6,78	0,11	4,36	0,1	28.06.2002	15,39	0	8,31	9,61	0,07	2,68	0,05
29.04.2002	5,01	0	8,38	6,62	0,11	4,37	0,09	29.06.2002	15,53	0	8,3	9,61	0,07	2,65	0,05
30.04.2002	4,91	0	8,37	6,46	0,12	4,39	0,09	30.06.2002	15,66	0	8,3	9,62	0,07	2,63	0,05

Başpınar Stream

Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄	Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄
01.03.2002	13	0,4	8,5	6,04	1,2	6,8	0,96	01.05.2002	14,7	0,3	8,1	3,7	0,38	4	0,33
02.03.2002	12,78	0,4	8,49	6,01	1,19	6,71	0,94	02.05.2002	14,79	0,3	8,09	3,62	0,56	3,89	0,42
03.03.2002	12,57	0,39	8,49	5,97	1,18	6,61	0,92	03.05.2002	14,88	0,31	8,09	3,55	0,74	3,77	0,51
04.03.2002	12,35	0,39	8,48	5,94	1,18	6,52	0,91	04.05.2002	14,97	0,31	8,08	3,47	0,92	3,66	0,61
05.03.2002	12,14	0,39	8,48	5,9	1,17	6,43	0,89	05.05.2002	15,06	0,31	8,07	3,39	1,11	3,55	0,7
06.03.2002	11,92	0,38	8,47	5,87	1,16	6,33	0,87	06.05.2002	15,15	0,32	8,07	3,31	1,29	3,44	0,79
07.03.2002	11,7	0,38	8,47	5,84	1,15	6,24	0,85	07.05.2002	15,24	0,32	8,06	3,24	1,47	3,32	0,88
08.03.2002	11,49	0,38	8,46	5,8	1,15	6,15	0,83	08.05.2002	15,33	0,32	8,05	3,16	1,65	3,21	0,98
09.03.2002	11,27	0,37	8,46	5,77	1,14	6,05	0,82	09.05.2002	15,42	0,33	8,05	3,08	1,83	3,1	1,07
10.03.2002	11,05	0,37	8,45	5,74	1,13	5,96	0,8	10.05.2002	15,51	0,33	8,04	3	2,01	2,98	1,16
11.03.2002	10,84	0,37	8,45	5,7	1,12	5,86	0,78	11.05.2002	15,6	0,33	8,03	2,93	2,19	2,87	1,25
12.03.2002	10,62	0,36	8,44	5,67	1,11	5,77	0,76	12.05.2002	15,69	0,34	8,03	2,85	2,37	2,76	1,34
13.03.2002	10,41	0,36	8,43	5,63	1,11	5,68	0,74	13.05.2002	15,78	0,34	8,02	2,77	2,56	2,65	1,44
14.03.2002	10,19	0,36	8,43	5,6	1,1	5,58	0,73	14.05.2002	15,87	0,34	8,01	2,69	2,74	2,53	1,53
15.03.2002	9,97	0,35	8,42	5,57	1,09	5,49	0,71	15.05.2002	15,96	0,35	8,01	2,62	2,92	2,42	1,62
16.03.2002	9,76	0,35	8,42	5,53	1,08	5,4	0,69	16.05.2002	16,05	0,35	8	2,54	3,1	2,31	1,71
17.03.2002	9,54	0,35	8,41	5,5	1,08	5,3	0,67	17.05.2002	16,15	0,35	7,99	2,46	3,28	2,19	1,81
18.03.2002	9,33	0,35	8,41	5,46	1,07	5,21	0,65	18.05.2002	16,24	0,35	7,98	2,38	3,46	2,08	1,9
19.03.2002	9,11	0,34	8,4	5,43	1,06	5,12	0,63	19.05.2002	16,33	0,36	7,98	2,31	3,64	1,97	1,99
20.03.2002	8,89	0,34	8,4	5,4	1,05	5,02	0,62	20.05.2002	16,42	0,36	7,97	2,23	3,82	1,85	2,08
21.03.2002	8,68	0,34	8,39	5,36	1,05	4,93	0,6	21.05.2002	16,51	0,36	7,96	2,15	4,01	1,74	2,18
22.03.2002	8,46	0,33	8,38	5,33	1,04	4,84	0,58	22.05.2002	16,6	0,37	7,96	2,07	4,19	1,63	2,27
23.03.2002	8,25	0,33	8,38	5,29	1,03	4,74	0,56	23.05.2002	16,69	0,37	7,95	2	4,37	1,52	2,36
24.03.2002	8,03	0,33	8,37	5,26	1,02	4,65	0,54	24.05.2002	16,78	0,37	7,94	1,92	4,55	1,4	2,45
25.03.2002	7,81	0,32	8,37	5,23	1,01	4,55	0,53	25.05.2002	16,87	0,38	7,94	1,84	4,73	1,29	2,54
26.03.2002	7,6	0,32	8,36	5,19	1,01	4,46	0,51	26.05.2002	16,96	0,38	7,93	1,76	4,91	1,18	2,64
27.03.2002	7,38	0,32	8,36	5,16	1	4,37	0,49	27.05.2002	17,05	0,38	7,92	1,69	5,09	1,06	2,73
28.03.2002	7,16	0,31	8,35	5,13	0,99	4,27	0,47	28.05.2002	17,14	0,39	7,92	1,61	5,27	0,95	2,82
29.03.2002	6,95	0,31	8,35	5,09	0,98	4,18	0,45	29.05.2002	17,23	0,39	7,91	1,53	5,46	0,84	2,91
30.03.2002	6,73	0,31	8,34	5,06	0,98	4,09	0,44	30.05.2002	17,32	0,39	7,9	1,45	5,64	0,73	3,01
31.03.2002	6,52	0,3	8,34	5,02	0,97	3,99	0,42	31.05.2002	17,41	0,4	7,9	1,38	5,82	0,61	3,1
01.04.2002	6,3	0,3	8,33	4,99	0,96	3,9	0,4	01.06.2002	17,5	0,4	7,89	1,3	6	0,5	3,19
02.04.2002	6,58	0,3	8,32	4,95	0,94	3,9	0,4	02.06.2002	17,55	0,4	7,89	1,34	5,9	0,51	3,17
03.04.2002	6,86	0,3	8,31	4,9	0,92	3,91	0,4	03.06.2002	17,61	0,4	7,9	1,39	5,81	0,52	3,16
04.04.2002	7,14	0,3	8,31	4,86	0,9	3,91	0,39	04.06.2002	17,66	0,4	7,9	1,43	5,71	0,52	3,14
05.04.2002	7,42	0,3	8,3	4,82	0,88	3,91	0,39	05.06.2002	17,72	0,39	7,9	1,47	5,61	0,53	3,12
06.04.2002	7,7	0,3	8,29	4,78	0,86	3,92	0,39	06.06.2002	17,77	0,39	7,9	1,51	5,52	0,54	3,11
07.04.2002	7,98	0,3	8,28	4,73	0,84	3,92	0,39	07.06.2002	17,82	0,39	7,91	1,56	5,42	0,55	3,09
08.04.2002	8,26	0,3	8,28	4,69	0,82	3,92	0,38	08.06.2002	17,88	0,39	7,91	1,6	5,32	0,56	3,07
09.04.2002	8,54	0,3	8,27	4,65	0,81	3,93	0,38	09.06.2002	17,93	0,39	7,91	1,64	5,23	0,57	3,06
10.04.2002	8,82	0,3	8,26	4,6	0,79	3,93	0,38	10.06.2002	17,99	0,39	7,92	1,68	5,13	0,57	3,04
11.04.2002	9,1	0,3	8,25	4,56	0,77	3,93	0,38	11.06.2002	18,04	0,38	7,92	1,73	5,03	0,58	3,02
12.04.2002	9,38	0,3	8,25	4,52	0,75	3,94	0,37	12.06.2002	18,1	0,38	7,92	1,77	4,94	0,59	3,01
13.04.2002	9,66	0,3	8,24	4,47	0,73	3,94	0,37	13.06.2002	18,15	0,38	7,93	1,81	4,84	0,6	2,99
14.04.2002	9,94	0,3	8,23	4,43	0,71	3,94	0,37	14.06.2002	18,2	0,38	7,93	1,85	4,74	0,61	2,97
15.04.2002	10,22	0,3	8,22	4,39	0,69	3,95	0,37	15.06.2002	18,26	0,38	7,93	1,9	4,65	0,61	2,96
16.04.2002	10,5	0,3	8,22	4,35	0,67	3,95	0,37	16.06.2002	18,31	0,38	7,93	1,94	4,55	0,62	2,94
17.04.2002	10,78	0,3	8,21	4,3	0,65	3,95	0,36	17.06.2002	18,37	0,37	7,94	1,98	4,46	0,63	2,93
18.04.2002	11,06	0,3	8,2	4,26	0,63	3,96	0,36	18.06.2002	18,42	0,37	7,94	2,02	4,36	0,64	2,91
19.04.2002	11,34	0,3	8,19	4,22	0,61	3,96	0,36	19.06.2002	18,47	0,37	7,94	2,07	4,26	0,65	2,89
20.04.2002	11,62	0,3	8,18	4,17	0,59	3,96	0,36	20.06.2002	18,53	0,37	7,95	2,11	4,17	0,66	2,88
21.04.2002	11,9	0,3	8,18	4,13	0,57	3,97	0,35	21.06.2002	18,58	0,37	7,95	2,15	4,07	0,66	2,86
22.04.2002	12,18	0,3	8,17	4,09	0,55	3,97	0,35	22.06.2002	18,64	0,37	7,95	2,2	3,97	0,67	2,84
23.04.2002	12,46	0,3	8,16	4,04	0,53	3,97	0,35	23.06.2002	18,69	0,36	7,95	2,24	3,88	0,68	2,83
24.04.2002	12,74	0,3	8,15	4	0,52	3,98	0,35	24.06.2002	18,74	0,36	7,96	2,28	3,78	0,69	2,81
25.04.2002	13,02	0,3	8,15	3,96	0,5	3,98	0,34	25.06.2002	18,8	0,36	7,96	2,32	3,68	0,7	2,79
26.04.2002	13,3	0,3	8,14	3,92	0,48	3,98	0,34	26.06.2002	18,85	0,36	7,96	2,37	3,59	0,7	2,78
27.04.2002	13,58	0,3	8,13	3,87	0,46	3,99	0,34	27.06.2002	18,91	0,36	7,97	2,41	3,49	0,71	2,76
28.04.2002	13,86	0,3	8,12	3,83	0,44	3,99	0,34	28.06.2002	18,96	0,36	7,97	2,45	3,39	0,72	2,74
29.04.2002	14,14	0,3	8,12	3,79	0,42	3,99	0,33	29.06.2002	19,01	0,35	7,97	2,49	3,3	0,73	2,73
30.04.2002	14,42	0,3	8,11	3,74	0,4	4	0,33	30.06.2002	19,07	0,35	7,98	2,54	3,2	0,74	2,71

Sukesen Stream

Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄	Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄
01.03.2002	15	0	8,04	9,95	3	2,7	0,04	01.05.2002	21,1	0	8,66	10,8	0,17	3,1	0,07
02.03.2002	14,78	0	8,05	9,81	2,91	2,67	0,04	02.05.2002	21,09	0	8,66	10,73	0,17	3,15	0,07
03.03.2002	14,57	0	8,06	9,68	2,81	2,65	0,04	03.05.2002	21,08	0,01	8,67	10,66	0,17	3,19	0,08
04.03.2002	14,35	0	8,07	9,54	2,72	2,62	0,05	04.05.2002	21,07	0,01	8,67	10,6	0,17	3,24	0,08
05.03.2002	14,14	0	8,07	9,4	2,63	2,6	0,05	05.05.2002	21,06	0,01	8,67	10,53	0,17	3,28	0,08
06.03.2002	13,92	0	8,08	9,26	2,53	2,57	0,05	06.05.2002	21,05	0,02	8,68	10,46	0,17	3,33	0,09
07.03.2002	13,7	0	8,09	9,13	2,44	2,55	0,05	07.05.2002	21,04	0,02	8,68	10,39	0,17	3,37	0,09
08.03.2002	13,49	0	8,1	8,99	2,35	2,52	0,06	08.05.2002	21,03	0,02	8,68	10,33	0,17	3,42	0,09
09.03.2002	13,27	0	8,11	8,85	2,25	2,49	0,06	09.05.2002	21,02	0,03	8,69	10,26	0,17	3,46	0,1
10.03.2002	13,05	0	8,12	8,71	2,16	2,47	0,06	10.05.2002	21,01	0,03	8,69	10,19	0,17	3,51	0,1
11.03.2002	12,84	0	8,13	8,58	2,06	2,44	0,06	11.05.2002	21	0,03	8,69	10,12	0,17	3,55	0,11
12.03.2002	12,62	0	8,14	8,44	1,97	2,42	0,06	12.05.2002	20,99	0,04	8,7	10,05	0,17	3,6	0,11
13.03.2002	12,41	0	8,14	8,3	1,88	2,39	0,07	13.05.2002	20,98	0,04	8,7	9,99	0,17	3,64	0,11
14.03.2002	12,19	0	8,15	8,16	1,78	2,36	0,07	14.05.2002	20,97	0,04	8,7	9,92	0,17	3,69	0,12
15.03.2002	11,97	0	8,16	8,03	1,69	2,34	0,07	15.05.2002	20,96	0,05	8,71	9,85	0,17	3,73	0,12
16.03.2002	11,76	0	8,17	7,89	1,6	2,31	0,07	16.05.2002	20,95	0,05	8,71	9,78	0,17	3,78	0,12
17.03.2002	11,54	0	8,18	7,75	1,5	2,29	0,08	17.05.2002	20,95	0,05	8,71	9,72	0,16	3,82	0,13
18.03.2002	11,33	0	8,19	7,61	1,41	2,26	0,08	18.05.2002	20,94	0,05	8,71	9,65	0,16	3,87	0,13
19.03.2002	11,11	0	8,2	7,48	1,32	2,24	0,08	19.05.2002	20,93	0,06	8,72	9,58	0,16	3,91	0,13
20.03.2002	10,89	0	8,21	7,34	1,22	2,21	0,08	20.05.2002	20,92	0,06	8,72	9,51	0,16	3,96	0,14
21.03.2002	10,68	0	8,21	7,2	1,13	2,18	0,09	21.05.2002	20,91	0,06	8,72	9,45	0,16	4	0,14
22.03.2002	10,46	0	8,22	7,06	1,04	2,16	0,09	22.05.2002	20,9	0,07	8,73	9,38	0,16	4,05	0,14
23.03.2002	10,25	0	8,23	6,93	0,94	2,13	0,09	23.05.2002	20,89	0,07	8,73	9,31	0,16	4,09	0,15
24.03.2002	10,03	0	8,24	6,79	0,85	2,11	0,09	24.05.2002	20,88	0,07	8,73	9,24	0,16	4,14	0,15
25.03.2002	9,81	0	8,25	6,65	0,75	2,08	0,09	25.05.2002	20,87	0,08	8,74	9,17	0,16	4,18	0,16
26.03.2002	9,6	0	8,26	6,51	0,66	2,05	0,1	26.05.2002	20,86	0,08	8,74	9,11	0,16	4,23	0,16
27.03.2002	9,38	0	8,27	6,38	0,57	2,03	0,1	27.05.2002	20,85	0,08	8,74	9,04	0,16	4,27	0,16
28.03.2002	9,16	0	8,28	6,24	0,47	2	0,1	28.05.2002	20,84	0,09	8,75	8,97	0,16	4,32	0,17
29.03.2002	8,95	0	8,28	6,1	0,38	1,98	0,1	29.05.2002	20,83	0,09	8,75	8,9	0,16	4,36	0,17
30.03.2002	8,73	0	8,29	5,96	0,29	1,95	0,11	30.05.2002	20,82	0,09	8,75	8,84	0,16	4,41	0,17
31.03.2002	8,52	0	8,3	5,83	0,19	1,93	0,11	31.05.2002	20,81	0,1	8,76	8,77	0,16	4,45	0,18
01.04.2002	8,3	0	8,31	5,69	0,1	1,9	0,11	01.06.2002	20,8	0,1	8,76	8,7	0,16	4,5	0,18
02.04.2002	8,73	0	8,32	5,86	0,1	1,94	0,11	02.06.2002	21,05	0,1	8,76	8,91	0,16	4,44	0,18
03.04.2002	9,15	0	8,33	6,03	0,1	1,98	0,11	03.06.2002	21,31	0,1	8,76	9,13	0,17	4,37	0,18
04.04.2002	9,58	0	8,35	6,2	0,11	2,02	0,11	04.06.2002	21,56	0,1	8,75	9,34	0,17	4,31	0,18
05.04.2002	10,01	0	8,36	6,37	0,11	2,06	0,1	05.06.2002	21,81	0,1	8,75	9,55	0,18	4,25	0,18
06.04.2002	10,43	0	8,37	6,54	0,11	2,1	0,1	06.06.2002	22,07	0,1	8,75	9,77	0,18	4,18	0,18
07.04.2002	10,86	0	8,38	6,71	0,11	2,14	0,1	07.06.2002	22,32	0,1	8,75	9,98	0,18	4,12	0,18
08.04.2002	11,29	0	8,39	6,88	0,12	2,18	0,1	08.06.2002	22,57	0,1	8,75	10,19	0,19	4,06	0,18
09.04.2002	11,71	0	8,4	7,05	0,12	2,22	0,1	09.06.2002	22,83	0,1	8,74	10,41	0,19	3,99	0,18
10.04.2002	12,14	0	8,42	7,22	0,12	2,26	0,1	10.06.2002	23,08	0,1	8,74	10,62	0,2	3,93	0,18
11.04.2002	12,57	0	8,43	7,39	0,12	2,3	0,1	11.06.2002	23,33	0,1	8,74	10,83	0,2	3,87	0,18
12.04.2002	12,99	0	8,44	7,56	0,13	2,34	0,1	12.06.2002	23,59	0,1	8,74	11,05	0,2	3,8	0,18
13.04.2002	13,42	0	8,45	7,73	0,13	2,38	0,09	13.06.2002	23,84	0,1	8,74	11,26	0,21	3,74	0,18
14.04.2002	13,85	0	8,46	7,9	0,13	2,42	0,09	14.06.2002	24,09	0,1	8,73	11,47	0,21	3,68	0,18
15.04.2002	14,27	0	8,47	8,07	0,13	2,46	0,09	15.06.2002	24,35	0,1	8,73	11,69	0,22	3,61	0,18
16.04.2002	14,7	0	8,49	8,25	0,14	2,5	0,09	16.06.2002	24,6	0,1	8,73	11,9	0,22	3,55	0,18
17.04.2002	15,13	0	8,5	8,42	0,14	2,54	0,09	17.06.2002	24,85	0,1	8,73	12,11	0,22	3,49	0,17
18.04.2002	15,55	0	8,51	8,59	0,14	2,58	0,09	18.06.2002	25,11	0,1	8,73	12,33	0,23	3,42	0,17
19.04.2002	15,98	0	8,52	8,76	0,14	2,62	0,09	19.06.2002	25,36	0,1	8,72	12,54	0,23	3,36	0,17
20.04.2002	16,41	0	8,53	8,93	0,14	2,66	0,08	20.06.2002	25,61	0,1	8,72	12,75	0,24	3,3	0,17
21.04.2002	16,83	0	8,54	9,1	0,15	2,7	0,08	21.06.2002	25,87	0,1	8,72	12,97	0,24	3,23	0,17
22.04.2002	17,26	0	8,56	9,27	0,15	2,74	0,08	22.06.2002	26,12	0,1	8,72	13,18	0,24	3,17	0,17
23.04.2002	17,69	0	8,57	9,44	0,15	2,78	0,08	23.06.2002	26,37	0,1	8,72	13,39	0,25	3,11	0,17
24.04.2002	18,11	0	8,58	9,61	0,15	2,82	0,08	24.06.2002	26,63	0,1	8,71	13,61	0,25	3,04	0,17
25.04.2002	18,54	0	8,59	9,78	0,16	2,86	0,08	25.06.2002	26,88	0,1	8,71	13,82	0,26	2,98	0,17
26.04.2002	18,97	0	8,6	9,95	0,16	2,9	0,08	26.06.2002	27,13	0,1	8,71	14,03	0,26	2,92	0,17
27.04.2002	19,39	0	8,61	10,12	0,16	2,94	0,08	27.06.2002	27,39	0,1	8,71	14,25	0,26	2,85	0,17
28.04.2002	19,82	0	8,63	10,29	0,16	2,98	0,07	28.06.2002	27,64	0,1	8,71	14,46	0,27	2,79	0,17
29.04.2002	20,25	0	8,64	10,46	0,17	3,02	0,07	29.06.2002	27,89	0,1	8,7	14,67	0,27	2,73	0,17
30.04.2002	20,67	0	8,65	10,63	0,17	3,06	0,07	30.06.2002	28,15	0,1	8,7	14,89	0,28	2,66	0,17

Golcuk Stream

Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄	Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄
01.03.2002	14,9	0,2	8,81	9,5	0,05	1,03	0,03	01.05.2002	17,7	0,2	8,14	8,8	0,05	0,7	0
02.03.2002	14,72	0,2	8,8	9,39	0,05	1,04	0,03	02.05.2002	17,71	0,2	8,14	8,67	0,05	0,71	0
03.03.2002	14,55	0,2	8,78	9,29	0,05	1,04	0,03	03.05.2002	17,72	0,2	8,13	8,54	0,06	0,72	0
04.03.2002	14,37	0,2	8,77	9,18	0,05	1,05	0,03	04.05.2002	17,73	0,2	8,13	8,41	0,06	0,73	0
05.03.2002	14,19	0,2	8,75	9,07	0,04	1,05	0,03	05.05.2002	17,74	0,2	8,13	8,28	0,06	0,74	0,01
06.03.2002	14,01	0,2	8,74	8,97	0,04	1,06	0,03	06.05.2002	17,75	0,2	8,12	8,15	0,06	0,75	0,01
07.03.2002	13,84	0,2	8,72	8,86	0,04	1,06	0,03	07.05.2002	17,76	0,2	8,12	8,03	0,07	0,76	0,01
08.03.2002	13,66	0,2	8,71	8,75	0,04	1,07	0,03	08.05.2002	17,77	0,2	8,12	7,9	0,07	0,77	0,01
09.03.2002	13,48	0,2	8,7	8,65	0,04	1,07	0,03	09.05.2002	17,78	0,2	8,11	7,77	0,07	0,78	0,01
10.03.2002	13,3	0,2	8,68	8,54	0,04	1,08	0,03	10.05.2002	17,79	0,2	8,11	7,64	0,08	0,79	0,01
11.03.2002	13,13	0,2	8,67	8,44	0,04	1,08	0,03	11.05.2002	17,8	0,2	8,1	7,51	0,08	0,8	0,02
12.03.2002	12,95	0,2	8,65	8,33	0,04	1,09	0,03	12.05.2002	17,81	0,2	8,1	7,38	0,08	0,81	0,02
13.03.2002	12,77	0,2	8,64	8,22	0,03	1,1	0,03	13.05.2002	17,82	0,2	8,1	7,25	0,08	0,82	0,02
14.03.2002	12,59	0,2	8,63	8,12	0,03	1,1	0,03	14.05.2002	17,83	0,2	8,09	7,12	0,09	0,83	0,02
15.03.2002	12,42	0,2	8,61	8,01	0,03	1,11	0,03	15.05.2002	17,84	0,2	8,09	6,99	0,09	0,84	0,02
16.03.2002	12,24	0,2	8,6	7,9	0,03	1,11	0,03	16.05.2002	17,85	0,2	8,09	6,86	0,09	0,85	0,02
17.03.2002	12,06	0,2	8,58	7,8	0,03	1,12	0,02	17.05.2002	17,85	0,2	8,08	6,74	0,1	0,85	0,03
18.03.2002	11,88	0,2	8,57	7,69	0,03	1,12	0,02	18.05.2002	17,86	0,2	8,08	6,61	0,1	0,86	0,03
19.03.2002	11,71	0,2	8,55	7,58	0,03	1,13	0,02	19.05.2002	17,87	0,2	8,08	6,48	0,1	0,87	0,03
20.03.2002	11,53	0,2	8,54	7,48	0,03	1,13	0,02	20.05.2002	17,88	0,2	8,07	6,35	0,11	0,88	0,03
21.03.2002	11,35	0,2	8,53	7,37	0,02	1,14	0,02	21.05.2002	17,89	0,2	8,07	6,22	0,11	0,89	0,03
22.03.2002	11,17	0,2	8,51	7,26	0,02	1,15	0,02	22.05.2002	17,9	0,2	8,07	6,09	0,11	0,9	0,03
23.03.2002	11	0,2	8,5	7,16	0,02	1,15	0,02	23.05.2002	17,91	0,2	8,06	5,96	0,11	0,91	0,04
24.03.2002	10,82	0,2	8,48	7,05	0,02	1,16	0,02	24.05.2002	17,92	0,2	8,06	5,83	0,12	0,92	0,04
25.03.2002	10,64	0,2	8,47	6,95	0,02	1,16	0,02	25.05.2002	17,93	0,2	8,05	5,7	0,12	0,93	0,04
26.03.2002	10,46	0,2	8,46	6,84	0,02	1,17	0,02	26.05.2002	17,94	0,2	8,05	5,57	0,12	0,94	0,04
27.03.2002	10,29	0,2	8,44	6,73	0,02	1,17	0,02	27.05.2002	17,95	0,2	8,05	5,45	0,13	0,95	0,04
28.03.2002	10,11	0,2	8,43	6,63	0,02	1,18	0,02	28.05.2002	17,96	0,2	8,04	5,32	0,13	0,96	0,04
29.03.2002	9,93	0,2	8,41	6,52	0,01	1,18	0,02	29.05.2002	17,97	0,2	8,04	5,19	0,13	0,97	0,05
30.03.2002	9,75	0,2	8,4	6,41	0,01	1,19	0,02	30.05.2002	17,98	0,2	8,04	5,06	0,13	0,98	0,05
31.03.2002	9,58	0,2	8,38	6,31	0,01	1,19	0,02	31.05.2002	17,99	0,2	8,03	4,93	0,14	0,99	0,05
01.04.2002	9,4	0,2	8,37	6,2	0,01	1,2	0,02	01.06.2002	18	0,2	8,03	4,8	0,14	1	0,05
02.04.2002	9,68	0,2	8,36	6,29	0,01	1,18	0,02	02.06.2002	18	0,2	8,02	4,77	0,14	0,97	0,05
03.04.2002	9,95	0,2	8,35	6,37	0,01	1,17	0,02	03.06.2002	18,01	0,2	8,02	4,73	0,13	0,94	0,05
04.04.2002	10,23	0,2	8,35	6,46	0,01	1,15	0,02	04.06.2002	18,01	0,2	8,01	4,7	0,13	0,91	0,05
05.04.2002	10,51	0,2	8,34	6,55	0,02	1,13	0,02	05.06.2002	18,01	0,2	8	4,67	0,13	0,88	0,04
06.04.2002	10,78	0,2	8,33	6,63	0,02	1,12	0,02	06.06.2002	18,02	0,2	8	4,63	0,13	0,85	0,04
07.04.2002	11,06	0,2	8,32	6,72	0,02	1,1	0,02	07.06.2002	18,02	0,2	7,99	4,6	0,12	0,82	0,04
08.04.2002	11,34	0,2	8,32	6,81	0,02	1,08	0,02	08.06.2002	18,02	0,2	7,99	4,57	0,12	0,79	0,04
09.04.2002	11,61	0,2	8,31	6,89	0,02	1,07	0,01	09.06.2002	18,03	0,2	7,98	4,53	0,12	0,75	0,04
10.04.2002	11,89	0,2	8,3	6,98	0,02	1,05	0,01	10.06.2002	18,03	0,2	7,97	4,5	0,11	0,72	0,03
11.04.2002	12,17	0,2	8,29	7,07	0,02	1,03	0,01	11.06.2002	18,03	0,2	7,97	4,47	0,11	0,69	0,03
12.04.2002	12,44	0,2	8,29	7,15	0,02	1,02	0,01	12.06.2002	18,04	0,2	7,96	4,43	0,11	0,66	0,03
13.04.2002	12,72	0,2	8,28	7,24	0,03	1	0,01	13.06.2002	18,04	0,2	7,95	4,4	0,1	0,63	0,03
14.04.2002	13	0,2	8,27	7,33	0,03	0,98	0,01	14.06.2002	18,04	0,2	7,95	4,37	0,1	0,6	0,03
15.04.2002	13,27	0,2	8,26	7,41	0,03	0,97	0,01	15.06.2002	18,05	0,2	7,94	4,33	0,1	0,57	0,03
16.04.2002	13,55	0,2	8,25	7,5	0,03	0,95	0,01	16.06.2002	18,05	0,2	7,94	4,3	0,1	0,54	0,03
17.04.2002	13,83	0,2	8,25	7,59	0,03	0,93	0,01	17.06.2002	18,05	0,2	7,93	4,27	0,09	0,51	0,02
18.04.2002	14,1	0,2	8,24	7,67	0,03	0,92	0,01	18.06.2002	18,06	0,2	7,92	4,23	0,09	0,48	0,02
19.04.2002	14,38	0,2	8,23	7,76	0,03	0,9	0,01	19.06.2002	18,06	0,2	7,92	4,2	0,09	0,45	0,02
20.04.2002	14,66	0,2	8,22	7,85	0,04	0,88	0,01	20.06.2002	18,06	0,2	7,91	4,17	0,08	0,42	0,02
21.04.2002	14,93	0,2	8,22	7,93	0,04	0,87	0,01	21.06.2002	18,07	0,2	7,9	4,13	0,08	0,39	0,02
22.04.2002	15,21	0,2	8,21	8,02	0,04	0,85	0,01	22.06.2002	18,07	0,2	7,9	4,1	0,08	0,36	0,02
23.04.2002	15,49	0,2	8,2	8,11	0,04	0,83	0,01	23.06.2002	18,07	0,2	7,89	4,07	0,07	0,33	0,01
24.04.2002	15,76	0,2	8,19	8,19	0,04	0,82	0	24.06.2002	18,08	0,2	7,88	4,03	0,07	0,29	0,01
25.04.2002	16,04	0,2	8,19	8,28	0,04	0,8	0	25.06.2002	18,08	0,2	7,88	4	0,07	0,26	0,01
26.04.2002	16,32	0,2	8,18	8,37	0,04	0,78	0	26.06.2002	18,08	0,2	7,87	3,97	0,07	0,23	0,01
27.04.2002	16,59	0,2	8,17	8,45	0,04	0,77	0	27.06.2002	18,09	0,2	7,87	3,93	0,06	0,2	0,01
28.04.2002	16,87	0,2	8,16	8,54	0,05	0,75	0	28.06.2002	18,09	0,2	7,86	3,9	0,06	0,17	0,01
29.04.2002	17,15	0,2	8,16	8,63	0,05	0,73	0	29.06.2002	18,09	0,2	7,85	3,87	0,06	0,14	0
30.04.2002	17,42	0,2	8,15	8,71	0,05	0,72	0	30.06.2002	18,1	0,2	7,85	3,83	0,05	0,11	0

Tatlim Stream

Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄	Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄
01.03.2005	7,9	0,2	8,12	8,65	0,12	3,9	0,07	01.05.2005	10,5	0,3	7,88	6,9	0,08	5,2	0
02.03.2005	7,81	0,2	8,12	8,46	0,12	3,96	0,07	02.05.2005	10,66	0,3	7,88	6,82	0,08	5,13	0
03.03.2005	7,72	0,2	8,11	8,28	0,12	4,02	0,07	03.05.2005	10,82	0,3	7,88	6,75	0,08	5,06	0
04.03.2005	7,63	0,2	8,11	8,09	0,11	4,07	0,06	04.05.2005	10,98	0,3	7,88	6,67	0,08	5	0
05.03.2005	7,54	0,2	8,11	7,91	0,11	4,13	0,06	05.05.2005	11,15	0,3	7,88	6,59	0,08	4,93	0
06.03.2005	7,45	0,2	8,1	7,72	0,11	4,19	0,06	06.05.2005	11,31	0,3	7,88	6,51	0,08	4,86	0
07.03.2005	7,36	0,2	8,1	7,54	0,11	4,25	0,06	07.05.2005	11,47	0,3	7,89	6,44	0,07	4,79	0
08.03.2005	7,27	0,2	8,1	7,35	0,1	4,31	0,06	08.05.2005	11,63	0,3	7,89	6,36	0,07	4,73	0
09.03.2005	7,18	0,2	8,09	7,17	0,1	4,36	0,05	09.05.2005	11,79	0,3	7,89	6,28	0,07	4,66	0,01
10.03.2005	7,09	0,2	8,09	6,98	0,1	4,42	0,05	10.05.2005	11,95	0,3	7,89	6,2	0,07	4,59	0,01
11.03.2005	7	0,2	8,08	6,8	0,1	4,48	0,05	11.05.2005	12,11	0,3	7,89	6,13	0,07	4,52	0,01
12.03.2005	6,91	0,2	8,08	6,61	0,1	4,54	0,05	12.05.2005	12,27	0,3	7,89	6,05	0,07	4,45	0,01
13.03.2005	6,82	0,2	8,08	6,42	0,09	4,6	0,05	13.05.2005	12,44	0,3	7,89	5,97	0,07	4,39	0,01
14.03.2005	6,73	0,2	8,07	6,24	0,09	4,65	0,04	14.05.2005	12,6	0,3	7,89	5,89	0,07	4,32	0,01
15.03.2005	6,64	0,2	8,07	6,05	0,09	4,71	0,04	15.05.2005	12,76	0,3	7,89	5,82	0,07	4,25	0,01
16.03.2005	6,55	0,2	8,07	5,87	0,09	4,77	0,04	16.05.2005	12,92	0,3	7,89	5,74	0,07	4,18	0,01
17.03.2005	6,45	0,2	8,06	5,68	0,08	4,83	0,04	17.05.2005	13,08	0,3	7,9	5,66	0,06	4,12	0,01
18.03.2005	6,36	0,2	8,06	5,5	0,08	4,89	0,04	18.05.2005	13,24	0,3	7,9	5,58	0,06	4,05	0,01
19.03.2005	6,27	0,2	8,06	5,31	0,08	4,95	0,04	19.05.2005	13,4	0,3	7,9	5,51	0,06	3,98	0,01
20.03.2005	6,18	0,2	8,05	5,13	0,08	5	0,03	20.05.2005	13,56	0,3	7,9	5,43	0,06	3,91	0,01
21.03.2005	6,09	0,2	8,05	4,94	0,07	5,06	0,03	21.05.2005	13,73	0,3	7,9	5,35	0,06	3,85	0,01
22.03.2005	6	0,2	8,05	4,75	0,07	5,12	0,03	22.05.2005	13,89	0,3	7,9	5,27	0,06	3,78	0,01
23.03.2005	5,91	0,2	8,04	4,57	0,07	5,18	0,03	23.05.2005	14,05	0,3	7,9	5,2	0,06	3,71	0,01
24.03.2005	5,82	0,2	8,04	4,38	0,07	5,24	0,03	24.05.2005	14,21	0,3	7,9	5,12	0,06	3,64	0,01
25.03.2005	5,73	0,2	8,03	4,2	0,07	5,29	0,02	25.05.2005	14,37	0,3	7,9	5,04	0,06	3,57	0,02
26.03.2005	5,64	0,2	8,03	4,01	0,06	5,35	0,02	26.05.2005	14,53	0,3	7,9	4,96	0,06	3,51	0,02
27.03.2005	5,55	0,2	8,03	3,83	0,06	5,41	0,02	27.05.2005	14,69	0,3	7,91	4,89	0,05	3,44	0,02
28.03.2005	5,46	0,2	8,02	3,64	0,06	5,47	0,02	28.05.2005	14,85	0,3	7,91	4,81	0,05	3,37	0,02
29.03.2005	5,37	0,2	8,02	3,46	0,06	5,53	0,02	29.05.2005	15,02	0,3	7,91	4,73	0,05	3,3	0,02
30.03.2005	5,28	0,2	8,02	3,27	0,05	5,58	0,01	30.05.2005	15,18	0,3	7,91	4,65	0,05	3,24	0,02
31.03.2005	5,19	0,2	8,01	3,09	0,05	5,64	0,01	31.05.2005	15,34	0,3	7,91	4,58	0,05	3,17	0,02
01.04.2005	5,1	0,2	8,01	2,9	0,05	5,7	0,01	01.06.2005	15,5	0,3	7,91	4,5	0,05	3,1	0,02
02.04.2005	5,28	0,2	8,01	3,03	0,05	5,68	0,01	02.06.2005	15,51	0,3	7,9	4,49	0,05	3,1	0,02
03.04.2005	5,46	0,21	8	3,17	0,05	5,67	0,01	03.06.2005	15,52	0,29	7,89	4,49	0,05	3,1	0,02
04.04.2005	5,64	0,21	8	3,3	0,05	5,65	0,01	04.06.2005	15,53	0,29	7,88	4,48	0,05	3,1	0,02
05.04.2005	5,82	0,21	7,99	3,43	0,05	5,63	0,01	05.06.2005	15,54	0,29	7,86	4,47	0,06	3,1	0,02
06.04.2005	6	0,22	7,99	3,57	0,06	5,62	0,01	06.06.2005	15,55	0,28	7,85	4,47	0,06	3,1	0,02
07.04.2005	6,18	0,22	7,98	3,7	0,06	5,6	0,01	07.06.2005	15,56	0,28	7,84	4,46	0,06	3,1	0,02
08.04.2005	6,36	0,22	7,98	3,83	0,06	5,58	0,01	08.06.2005	15,57	0,28	7,83	4,45	0,06	3,1	0,02
09.04.2005	6,54	0,23	7,98	3,97	0,06	5,57	0,01	09.06.2005	15,58	0,27	7,82	4,45	0,06	3,1	0,02
10.04.2005	6,72	0,23	7,97	4,1	0,06	5,55	0,01	10.06.2005	15,59	0,27	7,81	4,44	0,06	3,1	0,02
11.04.2005	6,9	0,23	7,97	4,23	0,06	5,53	0,01	11.06.2005	15,6	0,27	7,79	4,43	0,06	3,1	0,02
12.04.2005	7,08	0,24	7,96	4,37	0,06	5,52	0,01	12.06.2005	15,61	0,26	7,78	4,43	0,06	3,1	0,02
13.04.2005	7,26	0,24	7,96	4,5	0,06	5,5	0,01	13.06.2005	15,62	0,26	7,77	4,42	0,07	3,1	0,02
14.04.2005	7,44	0,24	7,95	4,63	0,06	5,48	0,01	14.06.2005	15,63	0,26	7,76	4,41	0,07	3,1	0,02
15.04.2005	7,62	0,25	7,95	4,77	0,06	5,47	0,01	15.06.2005	15,64	0,25	7,75	4,41	0,07	3,1	0,02
16.04.2005	7,8	0,25	7,95	4,9	0,07	5,45	0,01	16.06.2005	15,65	0,25	7,74	4,4	0,07	3,1	0,02
17.04.2005	7,98	0,25	7,94	5,03	0,07	5,43	0	17.06.2005	15,66	0,25	7,72	4,39	0,07	3,1	0,02
18.04.2005	8,16	0,26	7,94	5,17	0,07	5,42	0	18.06.2005	15,67	0,24	7,71	4,39	0,07	3,1	0,02
19.04.2005	8,34	0,26	7,93	5,3	0,07	5,4	0	19.06.2005	15,68	0,24	7,7	4,38	0,07	3,1	0,02
20.04.2005	8,52	0,26	7,93	5,43	0,07	5,38	0	20.06.2005	15,69	0,24	7,69	4,37	0,08	3,1	0,02
21.04.2005	8,7	0,27	7,92	5,57	0,07	5,37	0	21.06.2005	15,7	0,23	7,68	4,37	0,08	3,1	0,02
22.04.2005	8,88	0,27	7,92	5,7	0,07	5,35	0	22.06.2005	15,71	0,23	7,67	4,36	0,08	3,1	0,02
23.04.2005	9,06	0,27	7,91	5,83	0,07	5,33	0	23.06.2005	15,72	0,23	7,65	4,35	0,08	3,1	0,02
24.04.2005	9,24	0,28	7,91	5,97	0,07	5,32	0	24.06.2005	15,73	0,22	7,64	4,35	0,08	3,1	0,02
25.04.2005	9,42	0,28	7,91	6,1	0,07	5,3	0	25.06.2005	15,74	0,22	7,63	4,34	0,08	3,1	0,02
26.04.2005	9,6	0,28	7,9	6,23	0,08	5,28	0	26.06.2005	15,75	0,22	7,62	4,33	0,08	3,1	0,02
27.04.2005	9,78	0,29	7,9	6,37	0,08	5,27	0	27.06.2005	15,76	0,21	7,61	4,33	0,08	3,1	0,02
28.04.2005	9,96	0,29	7,89	6,5	0,08	5,25	0	28.06.2005	15,77	0,21	7,6	4,32	0,09	3,1	0,02
29.04.2005	10,14	0,29	7,89	6,63	0,08	5,23	0	29.06.2005	15,78	0,21	7,58	4,31	0,09	3,1	0,02
30.04.2005	10,32	0,3	7,88	6,77	0,08	5,22	0	30.06.2005	15,79	0,2	7,57	4,31	0,09	3,1	0,02

Çolakpınar Stream

Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄	Date	Temp	Sal.	PH	DO	NH ₄	NO ₃	PO ₄
01.03.2005	8,6	0,1	8,4	10,1	0,01	1,2	0,5	01.05.2005	11,7	0,1	8,19	8,6	0,07	2,4	0,02
02.03.2005	8,44	0,1	8,39	9,97	0,01	1,28	0,48	02.05.2005	11,81	0,1	8,17	8,47	0,07	2,36	0,02
03.03.2005	8,28	0,09	8,39	9,85	0,01	1,36	0,47	03.05.2005	11,91	0,1	8,15	8,33	0,07	2,32	0,02
04.03.2005	8,12	0,09	8,38	9,72	0,01	1,44	0,45	04.05.2005	12,02	0,1	8,13	8,2	0,07	2,27	0,02
05.03.2005	7,95	0,09	8,38	9,6	0,01	1,52	0,44	05.05.2005	12,13	0,1	8,11	8,06	0,07	2,23	0,02
06.03.2005	7,79	0,08	8,37	9,47	0,01	1,6	0,42	06.05.2005	12,23	0,1	8,09	7,93	0,07	2,19	0,02
07.03.2005	7,63	0,08	8,36	9,35	0,02	1,68	0,41	07.05.2005	12,34	0,1	8,07	7,8	0,07	2,15	0,02
08.03.2005	7,47	0,08	8,36	9,22	0,02	1,76	0,39	08.05.2005	12,45	0,1	8,05	7,66	0,07	2,11	0,02
09.03.2005	7,31	0,07	8,35	9,09	0,02	1,85	0,38	09.05.2005	12,55	0,1	8,03	7,53	0,07	2,06	0,03
10.03.2005	7,15	0,07	8,34	8,97	0,02	1,93	0,36	10.05.2005	12,66	0,1	8,01	7,4	0,07	2,02	0,03
11.03.2005	6,99	0,07	8,34	8,84	0,02	2,01	0,35	11.05.2005	12,76	0,1	7,99	7,26	0,07	1,98	0,03
12.03.2005	6,83	0,06	8,33	8,72	0,02	2,09	0,33	12.05.2005	12,87	0,1	7,97	7,13	0,07	1,94	0,03
13.03.2005	6,66	0,06	8,33	8,59	0,02	2,17	0,32	13.05.2005	12,98	0,1	7,95	6,99	0,07	1,9	0,03
14.03.2005	6,5	0,06	8,32	8,46	0,02	2,25	0,3	14.05.2005	13,08	0,1	7,93	6,86	0,07	1,85	0,03
15.03.2005	6,34	0,05	8,31	8,34	0,02	2,33	0,29	15.05.2005	13,19	0,1	7,91	6,73	0,07	1,81	0,03
16.03.2005	6,18	0,05	8,31	8,21	0,02	2,41	0,27	16.05.2005	13,3	0,1	7,89	6,59	0,07	1,77	0,03
17.03.2005	6,02	0,05	8,3	8,09	0,03	2,49	0,26	17.05.2005	13,4	0,1	7,86	6,46	0,06	1,73	0,03
18.03.2005	5,86	0,05	8,3	7,96	0,03	2,57	0,24	18.05.2005	13,51	0,1	7,84	6,32	0,06	1,69	0,03
19.03.2005	5,7	0,04	8,29	7,84	0,03	2,65	0,23	19.05.2005	13,62	0,1	7,82	6,19	0,06	1,65	0,03
20.03.2005	5,54	0,04	8,28	7,71	0,03	2,73	0,21	20.05.2005	13,72	0,1	7,8	6,06	0,06	1,6	0,03
21.03.2005	5,37	0,04	8,28	7,58	0,03	2,81	0,2	21.05.2005	13,83	0,1	7,78	5,92	0,06	1,56	0,03
22.03.2005	5,21	0,03	8,27	7,46	0,03	2,89	0,18	22.05.2005	13,94	0,1	7,76	5,79	0,06	1,52	0,03
23.03.2005	5,05	0,03	8,27	7,33	0,03	2,97	0,17	23.05.2005	14,04	0,1	7,74	5,65	0,06	1,48	0,03
24.03.2005	4,89	0,03	8,26	7,21	0,03	3,05	0,15	24.05.2005	14,15	0,1	7,72	5,52	0,06	1,44	0,03
25.03.2005	4,73	0,02	8,25	7,08	0,03	3,14	0,14	25.05.2005	14,25	0,1	7,7	5,39	0,06	1,39	0,04
26.03.2005	4,57	0,02	8,25	6,95	0,03	3,22	0,12	26.05.2005	14,36	0,1	7,68	5,25	0,06	1,35	0,04
27.03.2005	4,41	0,02	8,24	6,83	0,04	3,3	0,11	27.05.2005	14,47	0,1	7,66	5,12	0,06	1,31	0,04
28.03.2005	4,25	0,01	8,23	6,7	0,04	3,38	0,09	28.05.2005	14,57	0,1	7,64	4,99	0,06	1,27	0,04
29.03.2005	4,08	0,01	8,23	6,58	0,04	3,46	0,08	29.05.2005	14,68	0,1	7,62	4,85	0,06	1,23	0,04
30.03.2005	3,92	0,01	8,22	6,45	0,04	3,54	0,06	30.05.2005	14,79	0,1	7,6	4,72	0,06	1,18	0,04
31.03.2005	3,76	0	8,22	6,33	0,04	3,62	0,05	31.05.2005	14,89	0,1	7,58	4,58	0,06	1,14	0,04
01.04.2005	3,6	0	8,21	6,2	0,04	3,7	0,03	01.06.2005	15	0,1	7,56	4,45	0,06	1,1	0,04
02.04.2005	3,87	0	8,21	6,28	0,04	3,66	0,03	02.06.2005	14,97	0,1	7,55	4,54	0,06	1,07	0,04
03.04.2005	4,14	0,01	8,21	6,36	0,04	3,61	0,03	03.06.2005	14,95	0,1	7,55	4,62	0,06	1,03	0,04
04.04.2005	4,41	0,01	8,21	6,44	0,04	3,57	0,03	04.06.2005	14,92	0,1	7,54	4,71	0,06	1	0,04
05.04.2005	4,68	0,01	8,21	6,52	0,04	3,53	0,03	05.06.2005	14,89	0,1	7,53	4,79	0,06	0,96	0,03
06.04.2005	4,95	0,02	8,21	6,6	0,05	3,48	0,03	06.06.2005	14,87	0,1	7,53	4,88	0,06	0,93	0,03
07.04.2005	5,22	0,02	8,21	6,68	0,05	3,44	0,03	07.06.2005	14,84	0,1	7,52	4,96	0,05	0,89	0,03
08.04.2005	5,49	0,02	8,21	6,76	0,05	3,4	0,03	08.06.2005	14,81	0,1	7,51	5,05	0,05	0,86	0,03
09.04.2005	5,76	0,03	8,2	6,84	0,05	3,35	0,03	09.06.2005	14,79	0,1	7,5	5,13	0,05	0,82	0,03
10.04.2005	6,03	0,03	8,2	6,92	0,05	3,31	0,03	10.06.2005	14,76	0,1	7,5	5,22	0,05	0,79	0,03
11.04.2005	6,3	0,03	8,2	7	0,05	3,27	0,03	11.06.2005	14,73	0,1	7,49	5,3	0,05	0,75	0,03
12.04.2005	6,57	0,04	8,2	7,08	0,05	3,22	0,03	12.06.2005	14,71	0,1	7,48	5,39	0,05	0,72	0,03
13.04.2005	6,84	0,04	8,2	7,16	0,05	3,18	0,03	13.06.2005	14,68	0,1	7,48	5,47	0,05	0,68	0,02
14.04.2005	7,11	0,04	8,2	7,24	0,05	3,14	0,03	14.06.2005	14,65	0,1	7,47	5,56	0,05	0,65	0,02
15.04.2005	7,38	0,05	8,2	7,32	0,05	3,09	0,03	15.06.2005	14,63	0,1	7,46	5,64	0,05	0,61	0,02
16.04.2005	7,65	0,05	8,2	7,4	0,06	3,05	0,03	16.06.2005	14,6	0,1	7,46	5,73	0,05	0,58	0,02
17.04.2005	7,92	0,05	8,2	7,48	0,06	3,01	0,02	17.06.2005	14,57	0,1	7,45	5,81	0,04	0,54	0,02
18.04.2005	8,19	0,06	8,2	7,56	0,06	2,96	0,02	18.06.2005	14,55	0,1	7,44	5,9	0,04	0,51	0,02
19.04.2005	8,46	0,06	8,2	7,64	0,06	2,92	0,02	19.06.2005	14,52	0,1	7,43	5,98	0,04	0,47	0,02
20.04.2005	8,73	0,06	8,2	7,72	0,06	2,88	0,02	20.06.2005	14,49	0,1	7,43	6,07	0,04	0,44	0,01
21.04.2005	9	0,07	8,2	7,8	0,06	2,83	0,02	21.06.2005	14,47	0,1	7,42	6,15	0,04	0,4	0,01
22.04.2005	9,27	0,07	8,2	7,88	0,06	2,79	0,02	22.06.2005	14,44	0,1	7,41	6,24	0,04	0,37	0,01
23.04.2005	9,54	0,07	8,2	7,96	0,06	2,75	0,02	23.06.2005	14,41	0,1	7,41	6,32	0,04	0,33	0,01
24.04.2005	9,81	0,08	8,19	8,04	0,06	2,7	0,02	24.06.2005	14,39	0,1	7,4	6,41	0,04	0,3	0,01
25.04.2005	10,08	0,08	8,19	8,12	0,06	2,66	0,02	25.06.2005	14,36	0,1	7,39	6,49	0,04	0,26	0,01
26.04.2005	10,35	0,08	8,19	8,2	0,07	2,62	0,02	26.06.2005	14,33	0,1	7,39	6,58	0,03	0,23	0,01
27.04.2005	10,62	0,09	8,19	8,28	0,07	2,57	0,02	27.06.2005	14,31	0,1	7,38	6,66	0,03	0,19	0,01
28.04.2005	10,89	0,09	8,19	8,36	0,07	2,53	0,02	28.06.2005	14,28	0,1	7,37	6,75	0,03	0,16	0
29.04.2005	11,16	0,09	8,19	8,44	0,07	2,49	0,02	29.06.2005	14,25	0,1	7,36	6,83	0,03	0,12	0
30.04.2005	11,43	0,1	8,19	8,52	0,07	2,44	0,02	30.06.2005	14,23	0,1	7,36	6,92	0,03	0,09	0

