DOKUZ EYLÜL UNIVERSITY GRADUATE SCHOOL OF NATURAL AND APPLIED SCIENCES

OPTIMIZATION OF LC-MS/MS INSTRUMENTAL ANALYSIS CONDITIONS FOR MEASUREMENT OF ESTROGENIC HORMONES

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> February, 2014 İZMİR

OPTIMIZATION OF LC-MS/MS INSTRUMENTAL ANALYSIS CONDITIONS FOR MEASUREMENT OF ESTROGENIC HORMONES

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M.Sc THESIS EXAMINATION RESULT FORM

We have read the thesis entitled "OPTIMIZATION OF LC-MS/MS INSTRUMENTAL ANALYSIS CONDITIONS FOR MEASUREMENT OF ESTROGENIC HORMONES" completed by BİNNAZ ŞAHİNTÜRK under supervision of PROF. DR. İLGİ K. KAPDAN and we certify that in our opinion it is fully adequate, in scope and in quality, as a thesis for the degree of Master of Science.

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OPTIMIZATION OF LC-MS/MS INSTRUMENTAL ANALYSIS CONDITIONS FOR MEASUREMENT OF ESTROGENIC HORMONES

ABSTRACT

Endocrine Disrupting Chemicals are defined as substances that elicit the same chemical reactions as natural hormones, prevent naturally occurring hormones from affecting cells in the usual way by blocking the cell receptors, elicit unusual or abnormal reactions in cells. Estrogenic hormones are one of EDC present in natural waters and wastewaters. Their effect on human and animals is not well known yet. But, it could be a main concern to protect human and animal life soon when their effects on growth and reproductive system are clearly understood. It is evident that their concentration in the water is very low. Therefore, it is not easy to detect their existence in water. There is an urgent need to develop methods to be able to measure very low concentrations of these chemicals at ng/L or pg/L levels.

By considering this fact, the aim of this thesis was to develop an instrumental method for the measurement of estrogenic hormones as E1, E2, E3 and EE2 in LC-MS/MS. For this purpose, the study was designed as two stage optimization of elution conditions and instrumental operational conditions. The first stage was i) pre optimization of mobile phase, injection solution compositions and flow for peak symmetry and resolution factor by using central composite design, ii) improvement of integration area with the addition of alkaline solution (Ammonia) into mobile phase. Ionization was substantially improved by the addition of alkaline solution. Therefore, second stage optimization was conducted for the new mobile phase composition with ammonia solution. The latter stage designed as i) determination of ranges of operation parameters of LC-MS/MS ii) improvement of optimization conditions for LC Elution at determined ranges of operation parameters of LC-MS/MS by using Box Behnken response surface method, iii) improvement of optimized conditions for LC-MS/MS operation for the determined new elution parameters. Peak symmetry, resolution factor and integration area of hormones in chromatograms were substantially improved by the final optimization. Linear range of calibration curve developed at the optimal conditions were between 5 ng/L-30 ng/L which means even 5 ng/L estrogenic hormone concentration can be measured by this method.

Keywords: Estrogenic hormones, endocrine disrupting chemicals, response surface method, LC-MS/MS.

ÖSTROJENİK HORMONLARIN ÖLÇÜMÜNDE LC-MS/MS CİHAZ ANALİZ ŞARTLARININ OPTİMİZASYONU

ÖΖ

Endokrin bozucu kimyasallar, normal hormonların kimyasal reaksiyonlarını taklit ederek, ilgili reseptörlere bağlanarak hormon taklidi yapan ya da aşırı hormon salınımına sebep olarak anormalliklerin meydana gelmesine sebep olan kimyasallar olarak tanımlanmaktadır. Estrojenik hormonlar bu grupta yer almakta olup, yüzeysel ve atıksularda bulunmaktadırlar. İnsan sağlığı üzerine etkileri henüz tam olarak bilinmemektedir. Ancak, büyüme ve üreme sistemi üzerine etkileri anlaşıldığından insan ve hayvanları korumak için yakın zamanda önlemlerin alınması gereken kirleticiler olarak ortaya çıkacaktır. Estrojenik hormonların sudaki derişimlerinin çok düşük olmasından dolayı tespit edilmeleri kolay olmamaktadır. Bu nedenle, ng/L ve pg/L seviyelerinde ölçümlerin yapılabileciği metodların geliştirilmesi gereklidir.

Bu gerçekler göz önüne alınarak, bu tezin amacı östrojenik hormonlardan olan E1, E2, E3 ve EE2'nin LC-MS/MS cihazında ölçümlerine ilişkin enstrumental yöntemlerin geliştirilmesidir. Bu amaçla çalışmalar LC elüsyonun optimizasyonu ve enstrumental operasyon koşullarının optimizasyonu olmak üzere iki aşamada tasarlanmıştır. İlk aşama: i) pik simetrileri ve pik ayrım faktörleri için mobil fazın, enjeksiyon cözeltisi bileşiminin ve akışın merkezi kompozit dizayn yöntemiyle ön optimizasyonu gerçekleştirilmesi, ii) bazik amonyak çözeltisinin mobil faza eklenmesi ile alan değerlerinin iyileştirilmesidir. İyonizasyon bazik çözeltinin eklenmesi ile önemli derecede artmıştır. Bu nedenle, ikinci aşamada amonyak çözeltisi içeren mobil faz kompozisyonu optimize edilmiştir. Sonraki aşamada: i) LC-MS/MS'in calisma parametrelerinin aralıklarının belirlenmesi, ii) belirlenen bu çalışma aralıklarında Box-Behnken deneysel tasarım yöntemi ile LC elüsyonunun iyileştirilmesi, iii) belirlenen yeni elüsyon parametreleri ile LC-MS/MS'in optimize edilen çalışma şartlarının geliştirilmesidir. Pik simetrisi, pik ayrım faktörü ve kromotogramlardaki hormonlara ilişkin alan değerlerinde son optimizasyon ile oldukça gelişme gözlenmiştir. Optimum koşullarda kalibrasyon eğrisinin lineer aralığı 5 ng/L-30 ng/L dir ki bu yöntemle 5 ng/L hormon derişiminin ölçülebileceği anlamına gelmektedir.

Anahtar Kelimeler: Endokrin bozucu kimyasallar, yanıt yüzey yöntemi, östrojenik hormonlar, LC-MS/MS.

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CHAPTER ONE INTRODUCTION

1.1 The Endocrine System and Hormones

The endocrine system is one of communication systems of the body and it has several glands which excrete hormones with different functions in animals regulating and integrating the function of different cells, body growth, reproduction, maintenance, homeostasis and metabolism are managed by the endocrine systems in both plants and animals. (Gill, Súilleabháin, Regan & Moran, 2007). The hypothalamus, pancreas, pineal body, thyroid, parathyroid, adrenals, and the reproductive organs (ovaries and testes), pituitary are the major glands of body (Singhal, Song, Johnson & Swift, 2010).

The role of hormones excreted by body glands (ductless), which called chemical messengers of the body, is to transfer information from one set of cells to another in order to coordinate and regulate functions and metabolism of the body. They are excreted into the bloodstream from glands and transported to receptors where they trigger responses (Singhal et al., 2010).

When the hormones reach target cells (or organs), active area of hormone and active area of target cells (bonding site) bind with each other. This process is called "a lock and key receptor binding" procedure. Hormones attach to the receptor and the effector site is altered which produces the desired response. The receptor sites have a very high affinity for a specific hormone meaning that only very low concentrations are required to get the response (Gill et al., 2007).

There are three classes of hormones that include peptides, amines and steroids (Figure 1.1). Peptides are the most extensive group of them. Amines are excreted from the adrenal medulla and the thyroid gland. Amines are derivative of tyrosine. Peptides molecules are excreted by the parathyroid, heart, stomach, pituitary, kidneys and liver. Steroids are excreted by the adrenal cortex, placenta and gonads, are lipids

derived from cholesterol. Differentiation, sexual determination and development are controlled by the steroid hormones and can be selected as androgens and estrogens. The major estrogens include estriol, 17-estradiol, estrone (female sex hormones), while the major androgens are testosterone (male sex hormone) and 5-dihydrotestosterone. 11-ketotestosterone is the main androgen in fish. The most importance of the androgens and estrogens are having central role in reproductivity (Singhal et al., 2010).

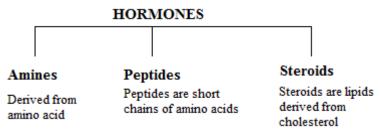


Figure 1.1 Classification of hormones.

1.2 Steroid Hormones

Steroid hormones are synthesized from cholesterol. Steroid hormones biosynthesis requires series of enzymes located in both endoplasmic reticulum and mitochondria. The free cholesterol transportation from the cytoplasm into mitochondria is the rate-limiting step of the process. The first reaction step which is occurred in mitochondria is transformation of cholesterol to pregnenolone by an enzyme in the inner membrane called CYP11A1. All steroid, hormones are synthesized from pregnenolone which is precursor however itself is not a hormone (Figure 1.2). Table 1.1 describes the enzymes required to synthesize the major classes of steroid hormones (Bowen, 2001).

| Common name | "Old" name | Current name |
|---------------------------------------|-----------------------|--------------|
| Side-chain cleavage enzyme; desmolase | P450 _{SCC} | CYP11A1 |
| 3 beta-hydroxysteroid dehydrogenase | 3 beta-HSD | 3 beta-HSD |
| 17 alpha-hydroxylase/17,20 lyase | P450 _{C17} | CYP17 |
| 21-hydroxylase | P450 _{C21} | CYP21A2 |
| 11 beta-hydroxylase | P450 _{C11} | CYP11B1 |
| Aldosterone synthase | P450 _{C11AS} | CYP11B2 |
| Aromatase | P450 _{aro} | CYP19 |

Table 1.1 The enzymes required to synthesize the major classes of steroid hormones (Bowen, 2001).

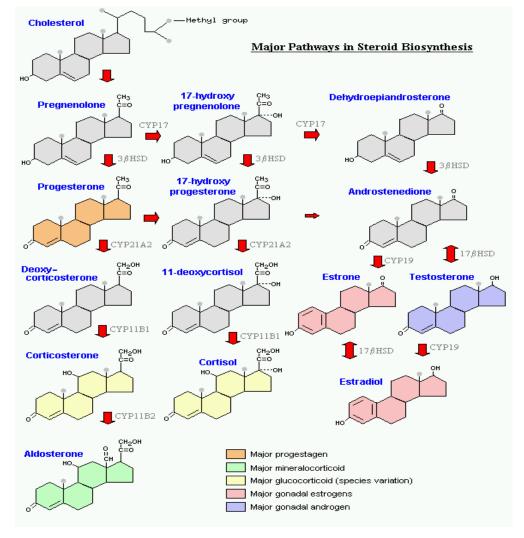


Figure 1.2 The biosynthetic pathways for major representatives of these classes of steroid hormones (Bowen, 2001).

1.3 Endocrine Disrupting Chemicals

Endocrine disrupting chemicals (EDCs) as an exogenous, have an effect on the endocrine system of animals including humans and effect in an intact organism, or its progeny, or (sub) populations (Bergman, Heindel, Jobling, Kidd & Zoeller, 2013). EDCs present in variable environmental areas such as water, air and soil. They mimic an estrogen-like response in organisms or antagonist effect can be seen. These chemicals may be natural or synthetic (Singhal et al., 2010).

EDCs are detected in food products (flax, soybeans, yams), household products (degradation products of detergents and associated surfactants, including octylphenol and nonylphenol), plants (phytoestrogens, grasses, beans, vegetables), plastics (phthalates, bisphenol A), pesticides (atrazine, DDT, nitrofen, endosulphan), pharmaceuticals (cimetidine, drug estrogens - birth control pills), industrial chemicals (benzo(a)pyrene, dioxin, PCBs), metals (cadmium, lead, mercury) (PUBH 5103, 2003a), paper production and fuel combustion. Some of the endocrine disruptive chemicals properties are shown on Table1.2 (Singhal et al., 2010).

| EDC | MOL. WT. | LOG Koc | | LOG Kd (L/kg) FOR SLUDGE | | SOLUBILITY | pKa |
|--|------------------|-----------|-----------|-----------------------------|----------|------------|------------|
| | (g/mol) | (L/kg) | (L/kg) | BIOLOGICAL | DIGESTED | (mg/L) | |
| Estradiol ^C | 272.4 | 2.55-4.01 | NAD | NA | NA | 13.0-32.0 | 10.5-10.71 |
| 17β-Estradiol (E2) | 272.4 | 3.10-4.01 | 3.9-4.0 | 2.4-2.8 | 2.3-2.5 | 13.0 | 10.71 |
| Estrone (E1) | 270.4 | 2.45-3.34 | 3.1-3.4 | 2.4-2.9 | 2.4-2.6 | 6.0-13.0 | 10.3–10.8 |
| Ethinylestradiol (EE2) | 296.4 | 2.91-3.04 | 2.8-4.2 | 2.5-2.8 | 2.3-2.6 | 4.8 | NA |
| Estriol (E3) | 288.4 | 2.13-2.62 | NA | NA | NA | 32 | 10.4 |
| Bisphenol A (BPA) | 228.0 | 2.50-6.60 | NA | NA | NA | 120-300 | 9.6-11.3 |
| Nonylphenol (NP) | 220.2 | 3.56-5.67 | 3.8->4.75 | NA | NA | 4.9-7.0 | 10.28 |
| Nonylphenol ethoxylates (NP1EO- NPnEO; n ≤ 20) | 264.0- 1101.6 | 3.91-5.64 | NA | NA | NA | 3.02-31.9 | NA |
| Octylphenol | 206.3 | 3.54-5.18 | NA | NA | NA | 12.6 | NA |

Table 1.2 Properties of some of the endocrine disruptive chemicals (Singhal et al., 2010).

Endocrine disrupting chemicals can be classified as follows;

EDCs can be categorized into the seven species (Bergman et al., 2013).

- Steroids compounds
- Phytoestrogens
- Surfactants
- Pesticides
- Polychlorinated compounds
- Organotin Compounds
- Organic oxygen compounds

One of the recent major concerns is the steroid compounds in water or wastewater. Steroid compounds are the natural and synthetic steroid hormones. Steroid hormones have lipophilic characters, because of this they tend to be transported through the blood by specific "carrier" proteins, and are able to passively enter cells and interact with receptors inside the cells (Bergman et al., 2013).

Natural estrogens, including at least six different estrogen hormones (e.g.Estrone, Estriol, 17-Estradiol), are generated by female of fertility age. Estrone, estriol and 17-estradiol are the major natural human derived estrogens. All three molecules have a 17-carbon system, which are the steroid with a methyl group at carbon-13 and an aromatic ring with a hydroxyl group at carbon-3 (Figure 1.3). The most active estrogen is 17-estradiol excreted by the ovaries, and is generated from androgens by the aromatize complex of enzymes. Synthetic estrogens are the birth control pill or for Hormone Replacement Treatment example, ethynylestradiol and diethylstilbestrol and they also found in wastewater effluent. Testosterone and progesterone can be detected in lower amounts than estrogens in wastewater. Major sources of testosterone and progesterone are food, in particular meat products. The hormones have been used as growth accelerator in the livestock. Steroid compounds almost never soluble in water because they tend to be lipophilic. Therefore steroid compounds generally adsorbed onto particles in the water or wastewater. Synthetic steroids have lower solubility than natural ones (Gill et al., 2007).

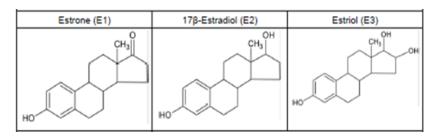


Figure 1.3 Molecular structures of estrogenic hormones.

The EDCs enter the environment from variable sources. The primary sources of EDCs in environment are wastewater treatment plants. In literature, the most common EDCs are reported as Estrone (E1), Estriol (E3), Ethinylestradiol (E2), 17 β -Estradiol (E2), BisphenolA (BPA), Nonylphenol ethoxylates (NPnEO), Octylphenol, Nonylphenol (NP). EDCs possibly cause many disorders in humans. However, no direct link has been established between EDC exposure and a human disorder, yet. On the other hand, the effects of EDCs to wildlife have been reported by laboratory studies (Singhal et al., 2010).

The concentrations of EDCs are partitioned in sediments, wastewater, air and drinking water in natural environment. Most of EDC's lipophilic and their solubility in water is low, which makes them easily adsorbed on a solid phase or associated with solid phase. Therefore, the highest concentration of EDCs could be in sediments and then in wastewater, the small amounts present in air and drinking water because EDCs have low vapor pressure (Singhal et al., 2010).

Biodegradation rates of E1, E2, E3 (the natural estrogens) and EE2 (the synthetic estrogen) are variable in wastewater treatment plant. It has been reported that they are biodegradable under aerobic condition and biodegradability degree is in the order of E3>E2>E1>EE2 (Singhal et al., 2010).

1.4 Health Effects of EDCs

EDCs are believed to have effects on some of women diseases such as endometriosis (PCBs, phthalates and dioxins) and fibroids (phthalates), early puberty

and breast development. But, there is no evidence about polycystic ovary syndrome or infertility. Few researches have reported some chemical could cause these diseases directly (Bergman et al., 2013). According to scientific studies in males, some of reproductive disease increased because of the EDCs exposure. The rate of testicular cancer has increased, semen quality has decreased and sperm counts are in the subfertile in some countries (Bergman et al., 2013). Some scientific studies in the rat indicated that there is an interrelationship between exposure to EDCs during fetal male and testicular dysgenesis (Bergman et al., 2013).

Some effects of EDCs on aquatic animals have been reported so far. The feminized male fish which exposed to estrogenic chemicals from sewage effluents have been seen in many countries. Male fish exposed to endocrine disrupting chemicals have reduced reproductive success of sperm and sperm production (Bergman et al., 2013). Some laboratory studies indicated that sex ratio is imbalanced in some animal populations such as mollusk, wild wish, and mouse when they exposed to EDCs. In the mouse model, the effects of dioxin on sex ratio are now verified (Bergman et al., 2013). Males offspring were exposed to EDCs, are reduced in humans e.g. in relation to 1,2-dibromo-3-chloropropane and dioxin).

EDCs (e.g. for PCBs, lead and methylmercury) have caused behavioural disorders such as sexually dimorphic behaviours in animals and behavioural defects in humans. In addition, there are evidences about neural development disorders in children and wildlife (Bergman et al., 2013).

The relationship between obesity and EDC exposed animals have been established by laboratory studies. Obesogens are disrupting endocrine system components such as controlling weight gain (Bergman et al., 2013).

In summary, it is well understood that EDCs can block, mimic, stimulate or inhibit production of natural hormones, and disrupt homeostasis (Bergman et al., 2013). Some of EDCs effects are shown on Table 1.3 (Singhal et al., 2010).

| EDC | SAMPLE SITE | SPECIES | EDC EFFECT | |
|---|--|--|---|--|
| Mix of WW with PCB, PBDE, APEOs, pesticides (hormones not identified) | Potomac River, Washington, DC | <i>Micropterus</i> <i>dolomieu/</i> small mouth bass | Intersex (oocytes in testes) | |
| WWTP effluent – unidentified mix of compounds | United Kingdom: WWTP receiving waters (rivers) | <i>Rutilus rutilus/</i> roach fish | Intersex (vitellogenin, ova, and tissue changes) characteristics in males | |
| Bisphenol A | Review of several studies | Human | Prostate cancer development | |
| Bisphenol A | Review of several lab studies | Human | Polycystic ovary syndrome, uterotrophic effects, decreased sperm, increased prolactin release | |
| Octylphenol | Lab study | Fisher 344 and Donyru/2 rat strains | Persistent estrus | |
| Ethinylestradiol (EE2) | Lab study | <i>Oryzias latipes/</i> Medaka fish | Intersex in males: testes ova and abnormal tissue development | |
| Ethinylestradiol (EE2) | Review of several studies | Human | Prostate cancer development | |
| Nonylphenol (NP) | Lab study | Sprague-Rawley female rats | Irregular estrous cycles and advanced onset of tissue development | |
| Nonylphenol (NP) | Lab study | Human males | Decrease in sperm production | |
| 17-Estradiol (E2) | Review of several studies | Rats | Delay in age of first estrus and vaginal opening; irregular then persistent estrus; disorders in ovarian and mammarian development | |
| 17-Estradiol (E2) | Field study | Chrysemys pictal/ female painted turtles | Increased E2 levels needed for vitellogenin induction of female eggs | |

Table 1.3 Environmental effects linked to estrogens present in wastewater (Singhal et al., 2010).

1.5 Sources and Pathways of Hormones in Environment

Hormones enter environment through both point (e.g., effluents from WWTPs) and non-point sources (e.g., surface runoff from agriculture operations). Steroidal hormones are mainly excreted to aquatic environment from human and animals. The other source of steroidal hormones is green plant processing industry (point source) which contributes phytoestrogens in surface water bodies. After excretion, all of hormones (the natural and synthetic hormones and their metabolites) reach WWTP. Sources and pathways of hormones in environment are shown in Figure 1.4 and EDC transport pathways through different environmental media are shown in Figure 1.5 (Hamid & Eskicioglu, 2012).

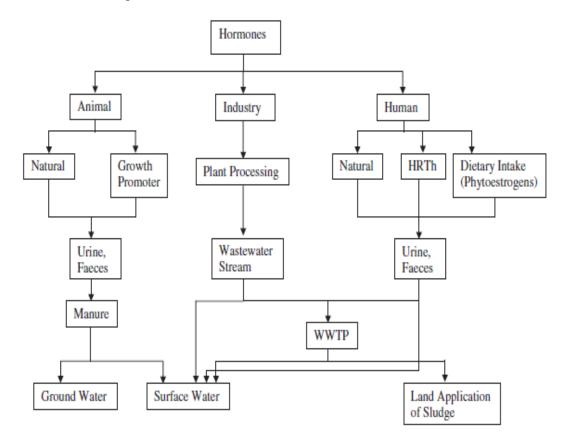


Figure 1.4 Sources and pathways of hormones in environment. HRTh: Hormone replacement therapy WWTP: Wastewater treatment plant (Hamid & Eskicioglu, 2012).

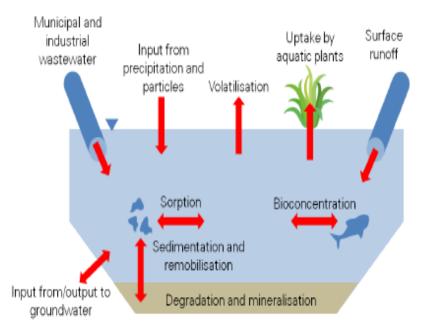


Figure 1.5 EDC transport pathways through different environmental media (Singhal et al., 2010).

1.6 Degradation of Hormones

The natural (E1, E2, E3) and synthetic estrogen (EE2) appear to be biodegradable at varying levels and the observed biodegradation order (highest to lowest) is estriol (E3) > 17 β -estradiol (E2) > estrone (E1) > 17 α -ethinylestradiol (EE2). E2 is oxidized E1 rapidly under aerobic conditions. In contrast, reduction of E1 to E2 under anaerobic condition could occur. But, this reaction has not been approved, yet. Degradation products of E1, E3 and EE2 are presently unknown. These transformations are shown in Figure 1.6. Besides that, microbial degradation ratio of E2 can be intercorrelated with increasing water temperature.

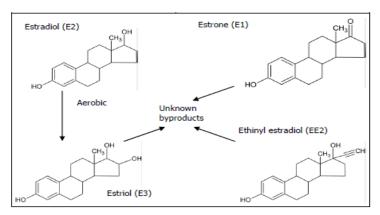


Figure 1.6 Proposed biodegradation and biotransformation mechanisms of estrogenic hormones.

1.7 Measurement Techniques of Steroidal Hormones EDCs

The toxicological studies are displayed that endocrine systems and homeostasis of animals including humans, its progeny and (sub) populations are affected by EDCs. Biological activities of EDCs are even effective in the lower range of concentrations. Because of this, the measurement of EDCs concentrations in wastewater, drinking water, surface water and ground water is very important.

The establishment of method to get real data for the concentration of any EDC is challenging because of: (1) the large number and chemical diversity of the compounds of interest; (2) the need to quantify low levels (ng/ L or pg/L) in an organic matrix; and (3) the complexity of sample concentration techniques. Therefore, a considerable effort should be given to the analytical methods for the measurement of EDCs. Steroid hormones are just one of these EDCs and they are major interest as the other synthetic EDCs. Chromatographic techniques (e.g. GC-MS/MS, LC-MS/MS) and non-cellular assays can be used for determination of different EDCs from different environmental samples. Enzyme linked immunosorbent assay (ELISA) is a widely used non-cellular assay that is available for specific EDCs (Belfroid et al., 1999). Although quantification of the EDCs can be performed rapidly by ELISA methods with low-cost, different responses can be achieved by different ELISA kits and the cross-reactivity can be performed between the different estrogens exist in the sample. GC-MS, GC-MS/MS or LC-MS, LC-MS/MS are the high technology instruments used for analysis of organic substances as well as estrogens (Singhal et al., 2010). These instruments are more reliable than spectrophotometric or immunoassay methods. Therefore, gas and liquid chromatographic techniques have been used for determination of EDCs hormones. The most common problem associated with measurement of estrogenic hormones in GC or GC-MS/MS derivatization of the samples. Endocrine disrupting hormones are non-volatile compounds and they need derivatization to be measured. Various derivatization techniques can be applied. However, derivatization procedures are long and its reproducibility could be low. Due to these problems in GC, liquid chromatographic techniques in estrogenic hormone measurement are preferred.

1.8 Literature Review

Many studies were performed by scientists about determination of EDCs in water samples. One of those studies was carried out by Isobe et al. in 2003. An analytical method was developed and applied for analysis of steroid estrogens and their conjugates in water samples. Samples were collected from lake, river and effluent of WWTP in Japan. The water samples were stored in amber glass bottles and transported in cold. 1L sample was filtered through glass fiber filter and then acidified to pH 3.5-5 with acetic acid. Samples were preconcentrated, purified and fractioned with SPE. Eluates were evaporated by gentle nitrogen gas and then dissolved in 100 μ L–1 mL of 5% acetonitrile /H₂O (v/v). Instrumental analysis was performed with LC-MS/MS (CapLC (Waters, USA) liquid chromatograph equipped with a Quattro (Micromass, UK) tandem mass spectrometer.) Chromatographic separation was performed with Zorbax Extend-C18 column (150 mm ×1 mm I.D 3.5 μ m, Agilent). The column was kept at 30 °C, mobile phase flow rate was 40 μ L/min and injection volume was set at 10 μ L. Mobile phase gradient conditions were shown in Table 1.4.

| Acetonitrile (%) | Water (%) | 100 mM | Time (min) |
|------------------|-----------|---------------|------------|
| | | Triethylamine | |
| | | in Water (%) | |
| 0 | 80 | 20 | 0 |
| 40 | 40 | 20 | 12 |
| 80 | 0 | 20 | 15 |
| 0 | 0 | 20 | 17 |

Table 1.4 Mobile phase gradient conditions reported by Isobe (2003).

The mass spectrometer was operated in negative mode electrospray ionization (ESI (-)) in Multiple Reaction Monitoring (MRM) mode and conditions were as follows; flow: 70 L/h; desolvation gas flow: 500 L/h; 2.7 kV; multiplier voltage: 650 V. Four HPLC columns were compared for chromatographic separation and responses of analytes. The columns used were TRP-100 (150 mm×1 mm I.D., 5 μ m, Supelco), Asahipak ODP-40 (150 mm×1 mm I.D., 4 μ m, Showa Denko K.K.), Zorbax Extend-C₁₈ (150 mm×1 mm I.D., 3.5 μ m, Agilent) and XTerraMS C₁₈ (150

mm×1 mm I.D., 3.5 μ m, Waters). Zorbax Extend-C₁₈ and XTerraMS C₁₈ are provided better chromatographic separation of the target analytes due to smaller particle size (3.5 μ m). Triethylamine (TEA) and ammonia were used to increase efficiency of ionisation of estrogenic hormones. The performance of the analytical method with Zorbax Extend-C₁₈ by using acetonitrile as mobile phase was depicted in Table 1.5.

| Analytes | Sample from | Sample volume(mL) | % Recovery (10 ng of std was spiked to 1 liter) | LOD (ng/L) (from S/N= 3) | Linear Working Range(ng/L) |
|----------|---------------|----------------------|---|--------------------------------|----------------------------------|
| E1 | | | 116 | 0.1 | |
| E2 | Lake Water | 1000 | 92 | 0.3 | 500-100000 |
| E3 | (Kasumigaura) | 1000 | 81 | 1.5 | 200 100000 |
| EE2 | | | 90 | 0.2 | |
| | | | | | |
| E1 | | | 101 | - | |
| E2 | Milli-Q water | 1000 | 76 | - | 500-100000 |
| E3 | water | 1000 | 80 | - | 500-100000 |
| EE2 | | | 82 | - | |

Table 1.5 Validation results of method developed by Isobe (2003).

Laganà et al. (2004) studied on analysis of estrogenic hormones in different matrix as surface water and STP influent, effluent. The samples were collected from Italian river and municipal sewage treatment plants (influent and effluent water) located in Rome, respectively. The samples were preserved at 4°C and extraction was carried out within 24–36 h. The solid phase extraction method was used in this study. Shortly, analytes were extracted and concentrated using Oasis HLB SPE analytical cartridge. 100 mL of influent, 250 mL effluent (STP) and 1000 mL of river water were extracted. After extraction procedure, extracts were concentrated to dryness under gentle N₂ stream. Finally, analytes were redissolved in 0.2 mL H₂O: ACN (50:50). 50µL of sample was injected to LC-MS/MS ESI system (Perkin-Elmer binary LC pump Series 200 (Perkin-Elmer, Norwalk, CT) equipped with a Rheodyne 7125 injector with a 50 µL Loop). The analytes were chromatographed on a 25 cm × 4.6mm i.d. column filled with 5 µm (average particle size) LC-18 packing Alltima (Alltech, Deerfield, IL). The flow rate of mobile phase was 1 mL/min and 200 µL of the column effluent was diverted into the ESI source. Post-column addition (before

splitting) of 0.11 ml/min of ammonia solution (50 mmol) was performed. The MS/MS conditions were optimized for sensitivity and selectivity. Analysis was conducted in the negative ionization mode. Source temperature was 350 °C. Multiple reaction monitoring (MRM) experiments were done to detect ion transitions. Acetonitrile was taken as a mobile phase component as shown in Table 1.6. The chromatographic separation of the method was given in Figure 1.7. Method performance and validation results were presented in Table 1.7.

| Acetonitrile (%) | Water (%) | Time (min) |
|------------------|-----------|------------|
| | | |
| 40 | 60 | 0.00 |
| 40 | 60 | 5.00 |
| 75 | 15 | 20.00 |
| 95 | 5 | 20.01 |
| 100 | 0 | 30.00 |
| 100 | 0 | 35.00 |

Table 1.6 Mobile phase gradient conditions reported by Laganà (2004).

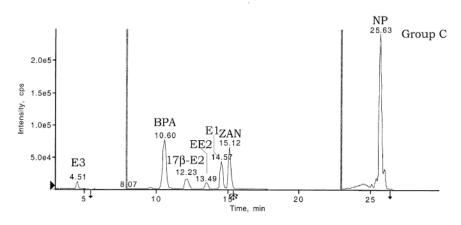


Figure 1.7 Chromatographic separation of analysis (Laganà, 2004).

| Analytes | Sample from | Sample volume(mL) | % Recovery | LOD (ng/L) (from S/N=3) | Linear Working Range(ng/L) |
|-----------------------|-----------------|----------------------|-----------------------|----------------------------|----------------------------------|
| E1 E2 E3 EE2 | Influent of STP | 100 | 95 95 91 96 | 1.2 1.9 7.0 1.6 | - |
| E1 E2 E3 EE2 | Effluent of STP | 250 | 89 95 92 96 | 0.8 0.8 0.5 1.1 | _ |
| E1 E2 E3 EE2 | River Water | 1000 | 99 96 97 100 | 0.1 0.2 0.3 0.4 | _ |

Table 1.7 Validation results of method developed by Laganà (2004).

Another study about estrogenic hormone measurement was performed by Vanderford et al. (Vanderford, Pearson, Rexing & Snyder, 2003). Water samples were collected from Boulder Basin of Lake Mead. They were kept in 1L amber glass bottle at 4°C, pH was adjusted to 2.0 with concentrated sulphuric acid and extracted within 14 days. In sample preparation step, sample was extracted and purified by SPE techniques (HLB cartridges from Waters Corp). First, SPE cartridges were preconditioned with 5 mL of methyl tert-butyl ether (MTBE), 5 mL of methanol, and 5 mL of reagent water and then dried with gentle nitrogen stream. After this process, samples were loaded into SPE and eluated with 5 mL of 10/90 (v/v) methanol/MTBE followed by 5 mL of methanol. Eluates were concentrated to 1mL. After that, 10µL of sample injected to LC-MS/MS (An Agilent (Palo Alto, CA) G1312A binary pump and an HTC-PAL auto sampler (CTC Analytics, Zwingen, Switzerland)) equipped with API 4000 triple quadrupole mass spectrometer (APCI ion source positive mode). Synergi Max-RP C12 (250×4.6mm, 4 µm) column was used. Methanol and 0.1% formic acid (v/v) in water were used as mobile phase component. Gradient method was performed (Table 1.8) and the analysis time was more than 30 minutes. Flow rate of mobile phase was set to 700 μ L/min. The performance of the analytical

method by using methanol as mobile phase was depicted in Table 1.9. Methanol and acetonitrile are the most widely used mobile phase components for chromatographic separation of estrogenic hormones. Methanol and acetonitrile have moderate polarity and a good chromatographic separation was obtained by this method.

| Methanol (%) | 0.1% Formic acid | Time (min) |
|--------------|--------------------|------------|
| | (v/v) in water (%) | |
| 5 | 95 | 0.00 |
| 5 | 95 | 3.50 |
| 80 | 20 | 10.00 |
| 80 | 20 | 13.00 |
| 100 | 0 | 13.01 |
| 100 | 0 | 21.00 |
| 5 | 95 | 21.01 |
| 5 | 95 | 30.00 |

Table 1.8 Mobile phase gradient conditions reported by Vanderford (2003).

Table 1.9 Validation results of method developed by Vanderford (2003).

| Analytes | Sample from | Sample volume(mL) | % Recovery (spiked 10 ng/L) | LOD (ng/L) | Linear Working Range(ng/L) |
|-----------|---------------|----------------------|--------------------------------|------------|----------------------------------|
| E2 EE2 | Surface water | 1000 | 92 96 | 1 | 1 to 100 |

Rodriguez et al. (Rodriguez, López de Alda & Barceló, 2004) studied on method development for measurement of estrogenic hormones at ng/L concentration. The study was performed by HP 1100 auto sampler HPLC system (Agilent Technologies) equipped with a HP 1090A LC pump and Electro Spray Ionization (ESI) mass spectrometer in negative mode (LC-ESI-MS). SPE (LiChrolut RP-18 cartridges 500mg) extraction procedure was applied. Volume of samples that were collected ground water from Llobregat River in Barcelona and drinking water from drinking water treatment plant were 500 mL. The final volumes of the extracts were 300 μ L with methanol after sample preparation. The injection volume to LC-MS/MS system were fixed to 20 μ L. Chromatographic separation was carried out with LiChrospher 100RP-18 (250mm × 4 mm, 5 μ m particle diameter) column. Mobile phase components consisted of acetonitrile and pure water. Flow rate of mobile phase was fixed to 1mL/min. Mobile phase gradient conditions was given in Table 1.10. The performance of the analytical method by using acetonitrile as mobile phase was depicted in Table 1.11.

| Acetonitrile (%) | Pure water (%) | Time (min) |
|------------------|----------------|------------|
| 10 | 90 | 0.00 |
| 100 | 0 | 30.00 |
| 10 | 90 | 30.01 |
| 10 | 90 | 40.00 |

Table 1.10 Mobile phase gradient conditions reported by Rodriguez (2004).

Table 1.11 Validation results of method developed by Rodriguez (2004).

| Analytes | Sample from | Sample volume (mL) | % Recovery | LOD (ng/L) | Linear working range(µg/L) |
|----------|----------------|--------------------------|------------|------------|----------------------------------|
| E1 | | | 100 | 2.5 | |
| E2 | Water | 500 | 98 | 2.5 | 5-1000 |
| E3 | sample | 300 | 94 | 5.04 | 3-1000 |
| EE2 | | | 91 | 3.22 | |

Trenholm et al. (2006) studied on analysis of estrogen hormone in different matrix as wastewater influent and effluent samples (Trenholm, Vanderford, Holady, Rexing & Snyder, 2006). Samples were collected in 1L amber glass bottle and preserved at 4° C, at pH=2 (H₂SO₄). Analytes are extracted and concentrated using a 500 mg Oasis HLB SPE analytical cartridge. After extraction procedure, extracts were concentrated to 1mL under gentle N₂ stream. Finally, 10µL of sample was injected to LC-MS/MS ESI (Agilent G1312A, Palo Alto, CA) and an auto sampler (HTC-PAL, CTC Analytics, Zwingen, Switzerland) system. Synergi Max-RP C12 (25.0cm×0.46 cm) with 4µm particle size chromatographic column was used. The flow rate of mobile phase was 700 µL/min. The MS/MS conditions were optimized for sensitivity and selectivity. Selected reaction monitoring (SRM) experiments were done to detect ion transitions. 0.1% formic acid (v/v) in water and methanol were used as mobile phase components. The condition of mobile phase gradient was shown in Table 1.12 and the results of the study with methanol as mobile phase were summarized in Table 1.13.

| Methanol (%) | 0.1% Formic acid | Time (min) |
|--------------|--------------------|------------|
| | (v/v) in water (%) | |
| 5 | 95 | 0.00 |
| 5 | 95 | 3.50 |
| 80 | 20 | 10.00 |
| 80 | 20 | 13.00 |
| 100 | 0 | 13.01 |
| 100 | 0 | 21.00 |
| 5 | 95 | 21.01 |
| 5 | 95 | 30.00 |

Table 1.12 Mobile phase gradient conditions reported by Trenholm (2006).

Table 1.13 Validation results of method developed by Trenholm (2006).

| Analytes | Sample from | Sample volume (mL) | % Recovery | LOD (ng/L) | Linear working range(µg/L) |
|----------|----------------|--------------------------|------------|------------|----------------------------------|
| E1 | | | 100 | 0.534 | |
| E2 | Water | 500 | 98 | 0.297 | 5-1000 |
| E3 | sample | 300 | 94 | 0.587 | 3-1000 |
| EE2 | | | 91 | 0.256 | |

Farr'e et al. (2007) conducted method development for estrogenic hormone determination in different matrixes as surface water and wastewater. Natural water, river water and WWTP water were collected. 1 L samples was filtered (0.45 μ m HVLP filters) and stored at 4°C in the dark. In sample preparation step, sample was extracted and purified by SPE techniques. Afterwards, reconstituted in 0.5mL methanol and then injected (25 μ L of sample) to LC-MS/MS (Waters Alliance 2690 LC and Quattro LC triple-quadrupole mass spectrometer). Purospher STAR-RP-18 (125×2.0mm, 5 μ m) column was used. LC-MS/MS interface ionization was carried out at ESI in negative ionization mode Acetonitrile and deionized water was the mobile phase. Gradient method was performed (Table 1.14) and flow rate of the mobile phase was fixed at 200 μ L. Purospher STAR-RP-18 (125×2.0mm, 5 μ m)

column and Waters Acquity C_{18} (50×2.1 mm, 1.7 µm) column were compared. The results indicated that chromatographic separation performed with smaller particle size column (Waters Acquity C_{18} with 1.7 µm particle size) provided relatively faster analysis and less solvent consumption. The performance of the analytical method by using acetonitrile as mobile phase and Waters Acquity C_{18} column was depicted in Table 1.15. LC-MS/MS chromatogram obtained by this method was shown in Figure 1.8.

| Acetonitrile (%) | Water (%) | Time (min) |
|------------------|-----------|------------|
| 10 | 90 | 0.00 |
| 50 | 50 | 5.00 |
| 80 | 20 | 25.00 |
| 100 | 0 | 25.01 |
| 100 | 0 | 29.00 |
| 10 | 90 | 31.00 |
| 10 | 90 | 44.00 |

Table 1.14 Mobile phase gradient conditions reported by Farr'e (2007).

Table 1.15 Validation results of method developed by Farr'e (2007).

| Analytes | Sample from | Sample volume (mL) | % Recovery | LOD (ng/L) |
|----------|----------------|--------------------------|------------|------------|
| E1 | | | 100 | 0.4 |
| E2 | Water | 500 | 98 | 0.5 |
| E3 | sample | 500 | 94 | 2 |
| EE2 | | | 91 | 1 |

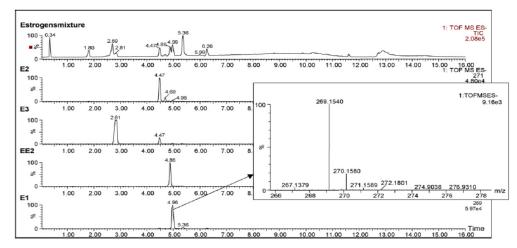


Figure 1.8 Total ion chromatogram for standard solutions of estrogens obtained from method developed by Farr'e (2007).

Another method development study was conducted at ng/L estrogenic hormone concentration in year 2008 by Kuster et al. Water samples were collected from Llobregat River, WWTP effluent and drinking water. It was reported that various sewage treatment plant effluents are connected to Llobregat river basin. Estrogens were extracted (20 mL of samples) with PLRP-s (cross linked styrene divinylbenzene). First, samples were loaded into SPE cartridges by automated solid-phase extraction system. After that, SPE cartridges were washed and eluted directly onto chromatographic column by mobile phase flow. Electrospray ionization mode was performed in negative mode. Auto sampler injection volume was fixed to 20 μ L. Chromatographic separation was carried out with Purospher STAR-RP-18 (125×2.0mm, 5 μ m) column. Mobile phase components consisted of acetonitrile and pure water. Flow rate of mobile phase was fixed to 0.2 mL/min. Mobile phase gradient conditions and method performances were depicted in Table 1.16 and Table 1.17, respectively.

| Acetonitrile (%) | Pure water (%) | Time (min) |
|------------------|----------------|------------|
| 10 | 90 | 0.00 |
| 50 | 50 | 5.00 |
| 80 | 20 | 25.00 |
| 100 | 0 | 25.01 |
| 100 | 0 | 30.00 |
| 10 | 90 | 32.00 |
| 10 | 90 | 45.00 |

Table 1.16 Mobile phase gradient conditions reported by Kuster (2008).

Table 1.17 Validation results of method developed by Kuster (2008).

| Analytes | Sample from | Sample volume (mL) | % Recovery | LOD (ng/L) |
|----------|----------------|--------------------------|------------|------------|
| E1 | | | 99 | 0.24 |
| E2 | Water | 500 | 85 | 0.85 |
| E3 | sample | 300 | 70 | 0.62 |
| EE2 | | | 89 | 0.62 |

Analysis of estrogenic hormone in different matrix as surface water and wastewater was conducted by Pedrouzo et al. (2009) (Pedrouzo, Borrull, Pocurull &

Marcé, 2009). The samples were collected from Ebro river and Catalan domestic sewage treatment plants (influent and effluent water) Spain. They were preserved at 4°C and at pH=2 (HCl). Analytes were extracted and concentrated using a 12mL, 500 mg Oasis HLB SPE analytical cartridge. 100 mL of influent, 250 mL effluent (STP) and 500 mL of river water were extracted. After extraction, extracts were concentrated to dryness under gentle N2 stream. Finally, analytes were redissolved with 1mL H₂O: MeOH (20:80). 50µL of sample was injected to LC-MS/MS ESI system. Kromasil 100 C18 (25.0cm×0.46 cm) with a 5µm particle size was used. The flow-rate of mobile phase was 1 mL/min and the column temperature was kept at 35°C. The MS/MS conditions were optimized for sensitivity and selectivity. Spray potential was 3000 V, a nebulizer was 45 psi and a source temperature was 350 °C and drying gas flow was 12 L/min. Selected reaction monitoring (SRM) experiments were done to detect ion transitions. Acetonitrile and methanol were tested as mobile phase for chromatographic peak shape and resolution of analytes. Acetonitrile resulted in better peak separation compared to methanol. Addition of acetic acid (pH 2.8) improved peak resolution. The mobile phase was selected as acetonitrile, Milli-Q water with acetic acid. Gradient method was performed. The analysis time was nearly 35 minutes. The results of method validation were summarized in Table 1.18.

| Analytes | Sample from | Sample volume(mL) | % Recovery | LOD (ng/L) (from S/N= 3) | Linear Working Range(ng/L) | |
|----------|-----------------|----------------------|------------|-----------------------------|----------------------------------|--|
| E1 | | | 60 | 50 | | |
| E2 | Influent of STP | 100 | 53 | 100 | 150-1000 | |
| E3 | Influent of 511 | 100 | 56 | 50 | 150-1000 | |
| EE2 | | | | 100 | | |
| E1 | | | 51 | 10-35 | | |
| E2 | Effluent of STP | 250 | 61 | 70 | 100-1500 | |
| E3 | Enluent of STP | | 59 | 10-35 | 100–1500 | |
| EE2 | | | 52 | 70 | | |
| | | | | | | |
| E1 | | | 49 | 15 | | |
| E2 | River Water | 500 | 32 | 30 | 75–1500 | |
| E3 | itiver water | 500 | 49 | 30 | 75 1500 | |
| EE2 | | | 68 | 30 | | |
| | | | | | | |

Table 1.18 Validation results of method developed by Pedrouzo (2009).

The extraction method is another question to obtain low detection limits. Sun et al. (Sun, Yong, Chu & Lina, 2009) studied on sample extraction and concentration techniques by using different SPE (Supelco). SPE cartridge and Solid Phase Disk Extraction (SPDE) (ENVI-18 SPE disk from Supelco) techniques were applied for extraction of analytes and compared for extraction efficiencies. 100 mL deionized water, tap water and waste water samples were collected and stored at 4°C in the dark. In sample preparation step, sample was extracted and purified by SPE or SPDE. Afterwards, they were dissolved in 0.1mL acetonitrile and then injected (5 μ L of sample) to LC-MS/MS. Acquity UPLC BEH RP-C18 (50×2.1mm, 1.7 μ m) column was used. Methanol and deionized water were the mobile phase to separate target estrogens. Gradient method was performed and the analysis time was more than 10 minutes. The performance of the analytical method by using methanol as mobile phase was depicted in Table 1.19 with SPE techniques.

| Analytes | Sample from | Sample volume(mL) | % Recovery (spiked 10 ng/L) | LOD (ng/L) (from S/N= 3) | Linear Working Range(ng/L) |
|-----------------------|-----------------|----------------------|--------------------------------|-----------------------------|----------------------------------|
| E1 E2 E3 EE2 | Deionized water | 100 | 88.0 93.2 88.4 90.6 | _ | 1 to 50 |
| E1 E2 E3 EE2 | Tap water | 100 | 82.2 92.9 90.4 86.9 | - | 1 to 50 |
| E1 E2 E3 EE2 | Waste water | 100 | 83.0 91.8 86.7 88.8 | 0.5 0.6 1 1.2 | 1 to 50 |

Table 1.19 Validation results of method developed by Sun (2009).

A study for measurement of sub-ng/L level of estrogens was performed by Vulliet et al. (2008) (Vulliet, Wiest, Baudot, Florence & Loustalot, 2008). HP1100 HPLC system (Agilent Technologies) equipped with a triple quadrupole mass spectrometer (Applied Biosystem/3200 QTrap) was used. SPE (Strata C18-E 200mg and the surface modified styrenedivinylbenzene Strata X 200mg from Phenomenex) extraction procedure was applied. Volume of samples extracted was 1 L. The final volumes of the extracts were 1mL after sample preparation. The injection volume to LC-MS/MS system were fixed to 100μ L. Chromatographic separation was carried out by Zorbax Eclipse XDB C18 ($100mm \times 2.1mm$, 3.5μ m) column. Mobile phase components consisted of acetonitrile and pure water. The resulting detection limits were considerably low compared to the other studies. The column used in this study might be the reason for low LOD values. On the other hand, although the method detection limits range $0.008 \mu g/L$ to $0.02 \mu g/L$, the linear working range was 50 ng/L to 2000 ng/L as shown in Table 1.20. This method is very sensitive for detection of very low concentrations. However, the measuring range (linear working range) is not consistent with these low LOD values. The performance of the analytical method by using acetonitrile as mobile phase was depicted in Table 1.20.

| Analytes | Sample from | Sample volume (mL) | % Recovery (pH=3) | Instrumental detection limit (µg/L) (from S/N= 3) | Method detection limit(ng/L) (from S/N= 3) | Linear working range(µg/L) |
|-----------------------|-----------------|--------------------------|------------------------------|--|---|----------------------------------|
| E1 E2 E3 EE2 | Water sample | 1000 | 97.5 98.8 96.9 96.8 | 0.02 0.008 0.02 0.18 | 0.02 0.01 0.03 0.20 | 0.05–20 |

Table 1.20 Validation results of method developed by Vulliet (2008).

The studies showed that reverse phase chromatographic separations were performed commonly for analysis of estrogenic hormones. Effective surface area of stationary phase, mobile phase composition and flow rate are most important factors for chromatographic separation. In order to achieve low detection limits, ionization efficiencies of target analytes should be advanced and interferences should be removed from samples prior to injection.

1.9 Objectives and Scope

EDCs are complex chemical. Their effect on human and animals are not well known yet. But, it could be a main concern to protect human and animal life soon when their effects are clearly understood. It is evident that their concentration in the water is very low. Therefore, it is not easy to detect their existence in water. There is an urgent need to develop methods to be able to measure very low concentrations of these chemicals. Measuring very low concentrations at ng/ or pg/L levels will help to understand adverse effect of these chemicals.

The objective of this thesis is to develop an instrumental method for the measurement of estrogenic hormones as E1, E2, E3 and EE2 in LC-MS/MS. The scope is to determine the optimum operation conditions of LC-MS/MS to obtain the lowest LOD.

In this scope, the following studies were conducted.

- Determination of optimum mobile phase composition
- Investigation of effect of alkaline mobile phase on ionization of hormones
- Optimization of ionization conditions
- Development of calibration curve for the determined optimum instrument operation conditions.

CHAPTER TWO MATERIALS AND METHODS

2.1 Chemicals

All the reagents used were analytical grade. Estrogenic hormones (E1, E2 and EE2, E3) were bought from Sigma–Aldrich (St Quentin Fallavier, France). The purity of hormones was at least 98%. Stock solutions of hormones were 10 mg/L in methanol. Working solutions to inject LC-MS/MS were prepared by diluting appropriate parts of each individual solutions in acetonitrile/water (28/72, v/v). HPLC grade acetonitrile and ammonia solution (25% in water) were bought from Merck. Milli-Q Pure water (18.2 M Ω cm⁻¹) was set in preparation of mobile phase and solutions.

2.2 Instrument

TSO Quantum Access Max Triple Quadropole Thermo MS liquid chromatography system (with an auto sampler, a degasser, a column oven, and a binary pump) was used in this study. X-calibur software from Thermo was used to data processing. Chromatographic separation was performed with Hypersil gold analytical column C18 / (2.1mm x 50mm / 1.9µm Particle Size). Auto sampler temperature and column oven temperature were fixed at 25^oC and injection volume was set to 25 µL in fool loop mode. Electro Spray Ionization (ESI (-)) technique was performed in negative mode and SRM mode (selected reaction monitoring) was used to analyses hormones. Isocratic elution program was applied. Precursor (Parent mass) and product ion masses as well as the individual declustering potential and collision energy voltages of each hormone are shown in Table 2.1.

| Name | | Parent | Product | SRM | Tube | Polarity |
|------|---|--------|---------|-----------|------|----------|
| | | Mass | Mass | Collision | Lens | |
| | | | | Energy | | |
| E1 | 1 | 269.1 | 143.2 | 51 | 85 | - |
| E1 | 2 | 269.1 | 145.3 | 38 | 85 | - |
| E2 | 3 | 271.1 | 145.1 | 43 | 85 | - |
| E2 | 4 | 271.1 | 183.2 | 41 | 85 | - |
| E3 | 5 | 287.0 | 145.0 | 37 | 85 | - |
| E3 | 6 | 287.0 | 171.1 | 38 | 85 | - |
| EE2 | 7 | 295.1 | 145.0 | 45 | 85 | - |
| EE2 | 8 | 295.1 | 159.1 | 37 | 85 | - |

Table 2.1 SRM mode conditions of the MS/MS detector.

2.3 Experimental Conditions

The study contains six parts as follows; 1) pre-optimization of mobile phase, injection solution compositions and flow for peak symmetry and resolution factor by using central composite design, 2) improvement of integration area with the addition of alkaline solution into mobile phase, 3) determination of ranges of operation parameters of LC-MS/MS 4) improvement of optimization conditions for LC Elution for determined ranges of operation parameters of LC-MS/MS by using Box Behnken response surface method, 5) further improvement of optimized conditions for LC-MS/MS operation, 6) development of calibration curve for the optimized instrumental and elution conditions. The experimental conditions of each study were given in detail in Results and Discussion Chapter.

CHAPTER THREE RESULTS AND DISCUSSIONS

3.1 Pre-Optimization of Mobile Phase, Injection Solution Compositions and Flow for Peak Symmetry and Resolution Factor by Central Composite Design

Optimization studies are generally conducted by using response surface methods (RSM). RSM is a kind of mathematical and statistical technique for designing experiments, building models, evaluating the relative significance of several independent variables, and determining the optimum conditions for desired responses (Box, 1978; Draper, 1988; Zhang, 2009). The two most common designs extensively used in RSM are the central composite design (CCD) and the Box-Behnken design (BBD). The CCD is ideal for sequential experimentation and allows a reasonable amount of information for testing lack of fit while not involving an unusually large number of design points (Montgomery, 1996; Myers, 1971; Somayajula, 2011). CCD is also useful for building a second order (quadratic) model for the response variable without needing to use a complete three-level factorial experiment. Coded variables are often used when constructing the design. After the designed experiment is performed, coefficients of response equation either linear or quadratic are determined by regression analysis with respect to observed responses. The final response equation with coefficients can be used predict the responses for different levels of factors.

The aim of this study was to optimize flow rate through the column, composition of mobile phase and standard solution for the best peak symmetry and resolution factor in LC-MS/MS. In other words, the effect of these three factors on the peak structure was investigated. Central composite design (CCD) was used for optimization purpose. Mobile phase and standard solution compositions were selected as acetonitrile (ACN) and water. Three factors in the design were X₁: percentage of acetonitrile in mobile phase (% ACN_m), X₂: percentage of acetonitrile in standard solution (% ACN_s); and X₃: flow rate of mobile phase through column (μ L/min). The responses were peak symmetry and resolution factor for four different estrogenic hormones as E1, E2, E3 and EE2. Table 3.1 indicates factors and their low and high values used in CCD. Coded and actual experimental points were depicted in Table 3.2. The experiments were conducted randomly and number of replicate at center point was 5. The concentration of hormones in the standard solution was 50 μ g/L in mix.

Table 3.1 Factors and ranges of CCD experimental design.

| Name | Units | Туре | Low Actual | High Actual |
|-------------------|--------|---------|------------|-------------|
| Mobile Phase | %ACN | Numeric | 40 | 70 |
| Standard Solution | %ACN | Numeric | 30 | 80 |
| Flow | μL/min | Numeric | 150 | 400 |

Table 3.2 CCD coded and actual experimental points.

| Run Number | Cod | led vari | ables | | Actual Variables | l Variables | | |
|------------|-----------|-----------|-----------|--------------------|-------------------|------------------|--|--|
| STD | X1 | X2 | X3 | % ACN _m | %ACN _s | Flow Rate µL/min | | |
| 1 | 0 | 0 | -α | 55.00 | 55.00 | 64.78 | | |
| 2 | -1 | -1 | +1 | 40.00 | 30.00 | 150.00 | | |
| 3 | +1 | -1 | -1 | 70.00 | 30.00 | 150.00 | | |
| 4 | -1 | +1 | -1 | 40.00 | 80.00 | 150.00 | | |
| 5 | +1 | +1 | -1 | 70.00 | 80.00 | 150.00 | | |
| 6 | 0 | -α | 0 | 55.00 | 12.96 | 275.00 | | |
| 7 | -α | 0 | 0 | 29.77 | 55.00 | 275.00 | | |
| 8 | $+\alpha$ | 0 | 0 | 80.23 | 55.00 | 275.00 | | |
| 9 | 0 | $+\alpha$ | 0 | 55.00 | 97.04 | 275.00 | | |
| 10 | -1 | -1 | +1 | 40.00 | 30.00 | 400.00 | | |
| 11 | +1 | -1 | +1 | 70.00 | 30.00 | 400.00 | | |
| 12 | -1 | +1 | +1 | 40.00 | 80.00 | 400.00 | | |
| 13 | +1 | +1 | +1 | 70.00 | 80.00 | 400.00 | | |
| 14 | 0 | 0 | $+\alpha$ | 55.00 | 55.00 | 485.22 | | |
| 15-1 | 0 | 0 | 0 | 55.00 | 55.00 | 275.00 | | |
| 15-2 | 0 | 0 | 0 | 55.00 | 55.00 | 275.00 | | |
| 15-3 | 0 | 0 | 0 | 55.00 | 55.00 | 275.00 | | |
| 15-4 | 0 | 0 | 0 | 55.00 | 55.00 | 275.00 | | |
| 15-5 | 0 | 0 | 0 | 55.00 | 55.00 | 275.00 | | |

The experiments were conducted at isocratic conditions, no gradient was applied. The auto sampler, parent and product masses, LC-MS/MS running and selected reaction mode (SRM) conditions were given in Table 3.3, Table 3.4, Table 3.5, Table 3.6, respectively. These are not the optimum conditions in operation of LC-MS/MS for studied hormones. Further studies were carried out for optimization of LC-MS/MS operation conditions.

Table 3.3 Auto sampler operation conditions for optimization of mobile phase, standard solution compositions and flow rate.

| Injection Volume (µL) | 25 |
|--|-------------|
| Needle Height From Bottom (mm) | 0.1 |
| Syringe Speed (µL/s) | 5 |
| Flush Volume (µL) | 400 |
| Flush/Wash Source | Wash Bottle |
| Wash Volume (µL) | 3000 |
| Flush Speed (µL/s) | 100 |
| Post-Injection Valve Switch Time (min) | 0 |
| Injection Mode | Full Loop |
| Tray Temperature (°C) | 25 |
| Column Oven Temperature (°C) | 25 |

Table 3.4 Parent and product masses and running conditions in LC-MS/MS.

| | Parent | Product | SRM | Retention | Time | Tube | Polarity | Trigger | Name |
|---|--------|---------|-----------|-----------|--------|------|----------|---------|------|
| | Mass | Mass | Collision | Time | Window | Lens | | | |
| | | | Energy | | | | | | |
| 1 | 269.1 | 143.2 | 51 | 7.50 | 15.00 | 85 | - | 0 | E1 |
| 2 | 269.1 | 145.3 | 38 | 7.50 | 15.00 | 85 | - | 0 | E1 |
| 3 | 271.1 | 145.1 | 43 | 7.50 | 15.00 | 85 | - | 0 | E2 |
| 4 | 271.1 | 183.2 | 41 | 7.50 | 15.00 | 85 | - | 0 | E2 |
| 5 | 287.0 | 145.0 | 37 | 7.50 | 15.00 | 85 | - | 0 | E3 |
| 6 | 287.0 | 171.1 | 38 | 7.50 | 15.00 | 85 | - | 0 | E3 |
| 7 | 295.1 | 145.0 | 45 | 7.50 | 15.00 | 85 | - | 0 | EE2 |
| 8 | 295.1 | 159.1 | 37 | 7.50 | 15.00 | 85 | - | 0 | EE2 |

Table 3.5 Interface conditions in LC-MS/MS for optimization of mobile phase, standard solution compositions and flow rate.

| Capillary Temperature (°C) | 280 |
|---|-----------|
| Vaporizer Temperature (°C) | 120 |
| Sheath Gas Pressure (Arb) | 25 |
| Aux Gas Pressure (Arb *) | 20 |
| Ion Sweep Gas Pressure (Arb) | 2.0 |
| Spray Voltage (V)(positive/negative polarity) | 2800/3500 |

*Arb: Arbitrary units

Table 3.6 The conditions of selected reaction mode (SRM) for optimization of mobile phase, standard solution compositions and flow rate.

| MS Acquire Time (min) | 15 |
|---------------------------------|-----|
| Collision Gas Pressure (m Torr) | 1.5 |
| Cycle Time (s) | 0.5 |

System was optimized to obtain a good peak shape. Good peak shape can be defined as a symmetrical or gaussian peak and poor peak shape can include both peak fronting and tailing. Good peak shape can be defined by tailing factor of 1.0, high efficiency, narrow peak width. It is important for improved resolution (Rs), more accurate quantitation and longer usable column lifetime.

Asymmetrical peaks are said to be either front or tail. Peak fronting or tailing can be caused by poor quality or polluted columns or by the dead volume of the system. Asymmetry can degrade the quality of a separation. The extent of asymmetry is expressed by either the asymmetry factory (As), or the tailing factor (Tusp or TF). In regard to the peak asymmetry, an asymmetry factor close to AS = 1 is ideal. A typical acceptable range could be 0.8 < AS < 1.8 when working towards a reduced plate height of $h \le 3$.

Symmetry factor (tailing factor, A_s)

The symmetry factor for a peak can be calculated using the following equation:

$$A_s = \frac{VV_x}{2d}$$
(3.1)

Where,

 $W_{\rm x}$ = peak width at 5% of peak height, measured from the baseline

d = baseline distance between the perpendicular dropped from the peak maximum and the leading edge of the peak at 5% of the peak height, measured in the same units as W_x .

Asymmetry factor of 1.0 signifies complete symmetry. Values of A_s which are greater than 2 may lead to incorrect integration, resulting in erroneous quantitation. The main factors that influence peak symmetry depend upon retention, solvent effects, incompatibility of the solute with the mobile phase or development of an excessive void at the inlet of the column.

Resolution is a measurement used to quantify peak spacing in a liquid chromatography (LC) separation. Although very simple at first examination, resolution can be affected significantly by peak sizes and shapes.

The most common equation used for measuring resolution (Rs) is

$$R_{s} = 2(t_{2} - t_{1}) / (w_{1} + w_{2})$$
(3.2)

Where,

 t_1 and t_2 = retention times or baseline distances between the point of injection and the perpendicular dropped from the maximum of each of the two peaks. $t_2 > t_1$ W_1 and W_2 = the respective peak widths measured from the baseline at 5% of peak height, measured in the same units as t_1 and t_2 .

The value of Rs which corresponds to a baseline separation between two symmetric peaks should be greater or equal than 1.5.

Where,

 t_1 and t_2 are the retention times of the two peaks of interest, and W1 and W2 are the peak widths measured at the baseline between tangents drawn to the peak sides. From a practical standpoint, it is much easier to measure the peak width at half the peak height (Dolan, 2002).

The resolution equation using the half-height method is

$$R_{\rm s} = \frac{2(t_2 - t_1)}{1.7 (w_{0.5,1} + w_{0.5,2})}$$
(3.3)

 $W_{0.5,1}$ and $W_{0.5,2}$ are the peak widths measured at half height. The half-height method for measuring resolution is used commonly by data systems because it is much easier to measure the half-height width than the baseline width. This technique is also easier to apply to peaks that are not baseline-resolved. If the peaks are not separated fully, it can be difficult or impossible to measure the baseline width accurately. Equations 1 and 2 will give the same value of Rs if the peaks are symmetric. The valley between two symmetric peaks just touches the baseline when $R_s = 1.5$. Because it is a good idea to have a little extra baseline between peaks to tolerate (Dolan, 2002).

These two methods to calculate Rs could be used for symmetrical peaks. At the beginning of experiments in this study, asymmetrical peak shapes were obtained. Therefore, Rs was calculated with following equation.

$$Rs = \frac{t_2 - t_1}{d_2 - d_1} \tag{3.4}$$

Where,

t₂: retention time of following peak

t₁: retention time of leading peak

d₂: baseline distance between the perpendicular dropped from the peak maximum and the leading edge of the following peak

d₁: baseline distance between the perpendicular dropped from the peak maximum and the fronting edge of the leading peak

Table 3.7 and Table 3.8 depict observed response of experimental points for four different estrogenic hormones. Peak symmetry was calculated for all hormones. But resolution factor was calculated with respect to E1 which is the first peak in the chromatogram. The following response function was used for correlation of the resolution factor (RF) and peak symmetry (A_s) with independent parameters.

$$Y = b_0 + b_1 X_1 + b_2 X_2 + b_3 X_3 + b_{12} X_1 X_2 + b_{13} X_1 X_3 + b_{23} X_2 X_3 + b_{123} X_1 X_2 X_3 + b_{11} X_1^2 + b_{22} X_2^2 + b_{33} X_3^2$$
(3.5)

Where Y is the predicted response for resolution factor (RF) and peak symmetry (A_s), b_0 is model constant, b_1 , b_2 , and b_3 are the linear coefficients, b_{12} , b_{13} , and b_{23} are the coefficients of interactions among the variables, and b_{11} , b_{22} , and b_{33} are the quadratic coefficients. The experimental results presented in Table 3.7 and Table 3.8 was used for determination of the response function coefficients in equation 3.5 by using Design Expert 7.0 statistic program for regression analysis.

| Run Number | Mobile Phase % ACN | Standard Solution %ACN | Flow Rate μL/min | PSE1 | PSE2 | PSE3 | PS EE2 |
|---------------|--------------------------|---------------------------|---------------------|-------|-------|-------|-----------|
| 1 | 55.00 | 55.00 | 64.78 | 3.130 | 2.542 | 2.158 | 1.745 |
| 2 | 40.00 | 30.00 | 150.00 | 4.882 | 3.444 | 3.000 | 2.429 |
| 3 | 70.00 | 30.00 | 150.00 | 2.913 | 3.737 | 1.586 | 2.756 |
| 4 | 40.00 | 80.00 | 150.00 | 0.267 | 0.258 | 4.682 | 0.176 |
| 5 | 70.00 | 80.00 | 150.00 | 1.889 | 1.846 | 1.357 | 1.538 |
| 6 | 55.00 | 12.96 | 275.00 | 3.400 | 3.308 | 3.600 | 3.200 |
| 7 | 29.77 | 55.00 | 275.00 | 1.419 | 1.121 | 1.857 | 1.056 |
| 8 | 80.23 | 55.00 | 275.00 | 3.077 | 3.500 | 2.200 | 3.364 |
| 9 | 55.00 | 97.04 | 275.00 | 0.535 | 0.900 | 0.939 | 0.500 |
| 10 | 40.00 | 30.00 | 400.00 | 3.571 | 3.118 | 2.167 | 2.667 |
| 11 | 70.00 | 30.00 | 400.00 | 2.500 | 2.800 | 2.273 | 2.556 |
| 12 | 40.00 | 80.00 | 400.00 | 1.842 | 1.923 | 1.750 | 1.095 |
| 13 | 70.00 | 80.00 | 400.00 | 2.333 | 2.077 | 1.692 | 1.714 |
| 14 | 55.00 | 55.00 | 485.22 | 3.833 | 2.636 | 1.700 | 1.600 |
| 15-1 | 55.00 | 55.00 | 275.00 | 3.000 | 3.231 | 2.462 | 1.895 |
| 15-2 | 55.00 | 55.00 | 275.00 | 3.412 | 3.769 | 2.667 | 2.278 |
| 15-3 | 55.00 | 55.00 | 275.00 | 3.625 | 3.462 | 2.462 | 2.000 |
| 15-4 | 55.00 | 55.00 | 275.00 | 3.688 | 3.286 | 2.385 | 2.105 |
| 15-5 | 55.00 | 55.00 | 275.00 | 3.500 | 3.143 | 2.385 | 2.167 |

Table 3.7 Observed peak symmetry of CCD for the hormones.

Table 3.8 Observed resolution factors of CCD for the hormones.

| Run Number | Mobile Phase % ACN | Standard Solution %ACN | Flow Rate µL/min | RF E2 | RF E3 | RF EE2 |
|---------------|--------------------------|------------------------------|---------------------|----------|----------|-----------|
| 1 | 55.00 | 55.00 | 64.78 | 0.191 | 1.077 | 0.407 |
| 2 | 40.00 | 30.00 | 150.00 | 0.688 | 2.806 | 0.412 |
| 3 | 70.00 | 30.00 | 150.00 | 0.066 | 0.154 | 0.167 |
| 4 | 40.00 | 80.00 | 150.00 | 0.245 | 0.744 | 0.101 |
| 5 | 70.00 | 80.00 | 150.00 | 0.000 | 0.250 | 0.134 |
| 6 | 55.00 | 12.96 | 275.00 | 0.208 | 0.714 | 0.234 |
| 7 | 29.77 | 55.00 | 275.00 | 1.000 | 2.585 | 0.283 |
| 8 | 80.23 | 55.00 | 275.00 | 0.000 | 0.156 | 0.102 |
| 9 | 55.00 | 97.04 | 275.00 | 0.066 | 0.341 | 0.133 |
| 10 | 40.00 | 30.00 | 400.00 | 0.441 | 1.698 | 0.328 |

| 11 | 70.00 | 30.00 | 400.00 | 0.027 | 0.257 | 0.171 |
|------|-------|-------|--------|-------|-------|-------|
| 12 | 40.00 | 80.00 | 400.00 | 0.282 | 1.000 | 0.167 |
| 13 | 70.00 | 80.00 | 400.00 | 0.024 | 0.257 | 0.111 |
| 14 | 55.00 | 55.00 | 485.22 | 0.154 | 0.679 | 0.214 |
| 15-1 | 55.00 | 55.00 | 275.00 | 0.180 | 0.889 | 0.259 |
| 15-2 | 55.00 | 55.00 | 275.00 | 0.179 | 0.867 | 0.241 |
| 15-3 | 55.00 | 55.00 | 275.00 | 0.203 | 0.844 | 0.222 |
| 15-4 | 55.00 | 55.00 | 275.00 | 0.185 | 0.867 | 0.214 |
| 15-5 | 55.00 | 55.00 | 275.00 | 0.177 | 0.867 | 0.236 |

Table 3.8 Observed resolution factors of CCD for the hormones (continued).

PS: Peak Symmetry

RF: Resolution Factor.

3.1.1 Optimization for Peak Symmetry

ANOVA analysis for the significance of coefficients of response equation for peak symmetry of hormones was conducted (Table 3.9). Values of "Prob > F" less than 0.0500 indicate model terms are significant. Values greater than 0.1000 indicate the model terms are not significant. Significance of quadratic coefficients indicate that response equation model is quadratic (as given in equation 3.5). Insignificant quadratic coefficients state that linear response equation can be used for diagnosis of model. The lack of fit test is desired to be insignificant which indicates that model fits and reliability of predicted responses. Reponses equation coefficients for different hormones were given in Table 3.10. R^2 >0.90 depicts a good agreement between predicted values and observed value. R^2 value was higher than 0.90 for E1, E2 and EE2 but less than 0.90 for E3. Adeq Precision" measures the signal to noise ratio. The ratio greater than 4 is desirable and states that model equation can be used to predict the reponse for any value of factors within the range of experimental design. Although R^2 value for E3 vas less than 0.90, Adeq Precision is larger than 4. Therefore, model coefficients can be used to predict response for E3.

| Source of variation | | E1 | E2 | E3 | EE2 |
|--|------------------|---------------------|---------------------|---------------------|---------------------|
| Coded | Actual | p-value Prob > F | p-value Prob > F | p-value Prob > F | p-value Prob > F |
| | | | | | |
| М | Model | 0.0012 | 0.0009 | 0.2876 | 0.0008 |
| X_1 | % ACN in | 0.2992 | 0.0039 | 0.1703 | 0.0008 |
| | mobile phase | | | | |
| X ₂ | % ACN in | < 0.0001 | < 0.0001 | 0.1791 | < 0.0001 |
| | stationary phase | | | | |
| X ₃ | Flow rate | 0.4040 | 0.5948 | 0.2342 | 0.4633 |
| X ₁ X ₂ | Interatction | 0.0039 | 0.1446 | 0.3498 | 0.0808 |
| | between mobile | | | | |
| | phase and | | | | |
| | Stationary pahse | | | | |
| X ₁ X ₃ | % ACN in | 0.8605 | 0.0983 | 0.0512 | 0.2181 |
| | mobile phase vs | | | | |
| | Flow rate | | | | |
| X ₂ X ₃ | % ACN in | 0.0194 | 0.0202 | 0.2746 | 0.2658 |
| | stationary phase | | | | |
| | vs flow rate | | | | |
| X ₁ ² | Quadratic effect | 0.0090 | 0.0101 | 0.6269 | 0.6847 |
| | of mobile phase | | | | |
| X_2^2 | Quadratic effect | 0.0029 | 0.0037 | 0.9388 | 0.3098 |
| | of stationary | | | | |
| | phase | | | | |
| X ₃ ² | Quadratic effect | 0.9025 | 0.0429 | 0.5149 | 0.1052 |
| | of flow rate | | | | |
| X ₁ X ₂ X ₃ | Three factor | 0.1526 | 0.4730 | 0.4274 | 0.7388 |
| | interaction | | | | |
| Lack of Fit | 1 | 0.0840 | 0.1091 | 0.0004 | 0.0350 |

Table 3.9 ANOVA analysis of peak symmetry for estrogenic hormones .

Table 3.10 Regression coefficients of peak symmetry response equation for estrogenic hormones.

| Coefficient of | Coefficients for | Coefficients | Coefficients for E3 | Coefficients |
|-----------------------|------------------|--------------|---------------------|--------------|
| response | E1 | for E2 | | for EE2 |
| equation | | | | |
| b ₀ | 832.838 | -102.270 | +0.061779 | 318.706 |
| b ₁ | +0.042668 | +0.17090 | +0.050065 | -0.010742 |
| b ₂ | -0.16219 | -0.058248 | +0.12648 | -0.070689 |
| b ₃ | -0.023429 | 3.23E+02 | 4.67E+02 | 5.50E+02 |
| b ₁₂ | 3.21E+02 | 1.19E+02 | -1.97E+02 | 8.12E+01 |

| b ₁₃ | 2.82E+01 | -1.56E+00 | 6.29E+00 | -3.40E+00 |
|------------------|-----------|-----------|-----------|-----------|
| b ₂₃ | 4.47E+01 | 2.47E+01 | -3.54E+01 | 8.70E+00 |
| b ₁₁ | -1.87E+02 | -1.56E+02 | -4.49E+01 | 1.58E+01 |
| b ₂₂ | -8.32E+01 | -6.77E+01 | -2.54E+00 | -1.47E+01 |
| b ₃₃ | 9.94E-02 | -1.61E+00 | -8.72E-01 | -9.88E-01 |
| b ₁₂₃ | -5.41E-01 | -2.19E-01 | 4.66E-01 | -8.13E-02 |
| \mathbb{R}^2 | 0.9326 | 0.9362 | 0.6528 | 0.9384 |
| Adequate | 13.150 | 12.773 | 4.911 | 12.822 |
| precision | | | | |

Table 3.10 Regression coefficients of peak symmetry response equation for estrogenic hormones (continued).

3.1.2 Effect of Independent Variables on Peak Symmetries of Estrogenic Hormones

The response equation developed for E1 was used to predict the any PS at different levels of independent variables. Then response surface plots were used to evaluate the effect these independent variables on the peak symmetry. The effect of flow rate and % ACN in standard solution (% ACN_s) on PS of E1 at constant ACN concentration in mobile phase (% ACN_m=40) was given in Figure 3.1. The increase in flow rate from 150 μ L/min from 400 μ L/min at the highest % ACN_s (90%) provided a slight improvement in PS value as PS=0.01 to 0.018, respectively. On the other hand, decreasing in %ACN_s from 90% to 15 % resulted in a very high PS value around PS= 4 to 5. This result indicates that low %ACN_s = 80-0 and F=380 - 390 μ L/min.

Variation of PS for E1 with % ACN_s and % ACN_m at constant flow rate, F= 300 μ L/min, is depicted in Figure 3.2. Increasing percentage of ACN_m from 40% to 70% at high level of ACN_s (90%) provided a slight increase in PS from 0.99 to 1.49, respectively. It means that the effect of %ACN_m is not substantial on PS of E1. However, peak symmetry is destructed when %ACN_s is reduced to 15% at 40% ACN_m. This result indicates that there is a significant interaction between %ACN_s and %ACN_m.

The effect of flow rate and %ACN_m on PS of E1 at constant %ACN_s is given in Figure 3.3. The predicted PS value for the studied range of independent variables varied between 0 and 2.55. The highest destruction PS can be observed when ACN_m is increased from 40% to 70%. Flow has got a slight effect on PS destruction either. The most substantial effect of flow is observed when a percentage of ACN_m is 40%. PS can reach up to 2.55 which indicate a significant tailing in chromatogram. The conditions which results in PS around 1 can be determined as %ACN_m= 45-48 and flow is between 150-275 μ L/min.

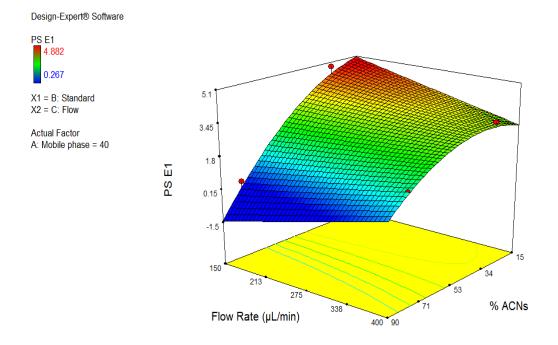


Figure 3.1 Variation of peak symmetry for E1 with flow and % ACN in standard at 40% ACN_m.

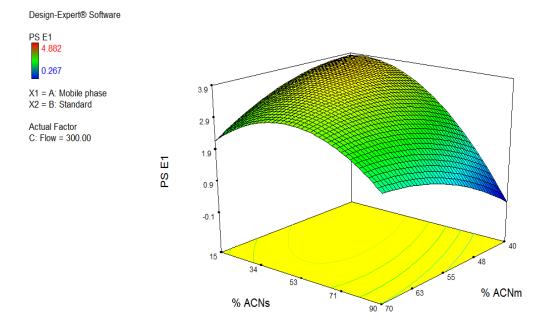


Figure 3.2 Variation of PS for E1 with % ACN standard solution and mobile phase at 300 μ L/min.

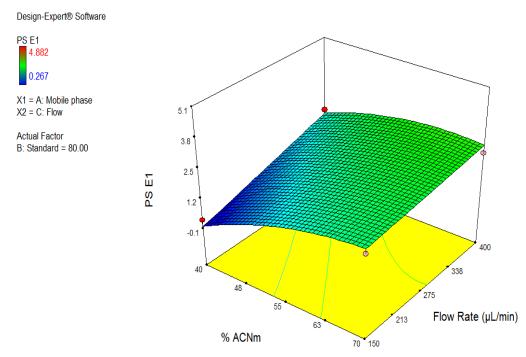


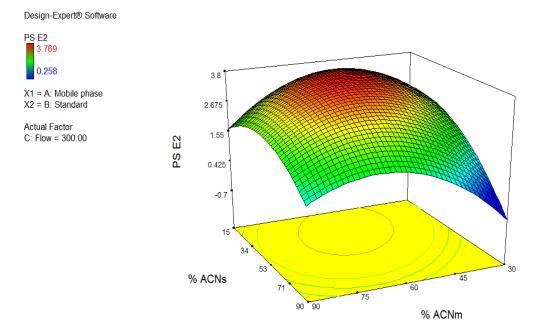
Figure 3.3 Variation of PS for E1 with % ACN_m and flow at % ACN_s = 80.

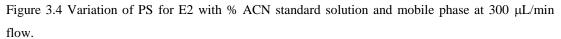
Effects of factors on PS of E2 were given through Figures 3.4 to 3.6. The first figure is about variation of PS for E2 with % ACN_s and % ACN_m at constant flow rate F= 300 µl/min. The most suitable peak symmetry value was observed when ACN_s is in the range of 90% to 70% for ACN_m between 40 - 70%. However, the

peak symmetry is substantially destructed when % ACN_s is less than 60% for any value of ACN_m . The effect of % ACN_m is not as significant as % ACN_s for E2.

Figure 3.5 indicates the effect of flow rate and %ACN_m on PS of E2 at constant %ACN_s (90%). The predicted PS values for the studied range of independent variables vary between 0 and 1.8. The highest destruction on PS can be observed when ACN_m is increased from 55% to 70%. Flow also has got a slight effect on PS structure. The most substantial effect of flow is observed when flow is higher than 325μ L/min at ACN_m = 70%. PS can reach up to 1.425 which indicates a slight tailing in chromatogram. The conditions which results in PS around 1 can be determined as %ACN_m = 45-48 and flow is between 250-300 μ L/min.

Similarly, effect of flow rate and % ACN_s on PS of E2 at constant ACN concentration in mobile phase (40%) was evaluated and 3D plot was given in Figure 3.6. At low ACN_s values between 60% - 30% for any flow rate, the peak symmetry was not acceptable. PS value range between PS = 2.0 - 3.4. However, increasing ACN in standard solution over 70% at 300μ L/min >flow rates >250 μ L/min resulted in a substantial improvement in the peak symmetry. The predicted PS values for these conditions were PS = 1.09 - 1.4. Therefore, the most suitable conditions to obtain PS values between 0.9 and 1.2 can be determined as %ACN_s > 80% and 260 μ L/min > flow > 250 μ L/min.





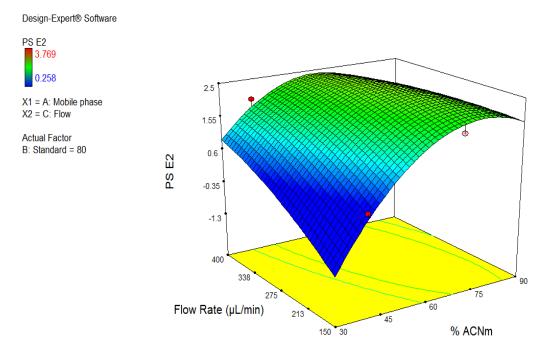


Figure 3.5 Variation of PS for E2 with % ACN_m and flow at % $ACN_s{=}\,80.$

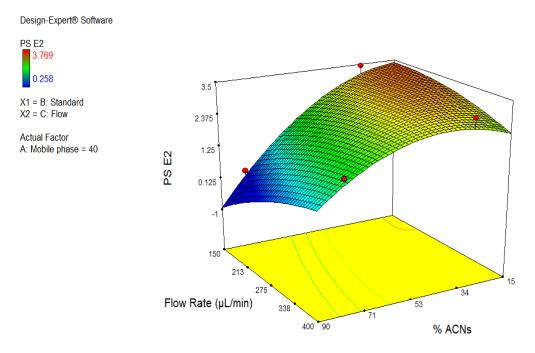


Figure 3.6 Variation of peak symmetry for E2 with flow and % ACN in standard at 40% ACN_m.

E3 is another estrogenic hormone encountered in wastewater and surface water. Peak symmetry of E3 was also considered throughout the experiments and statistical analysis of experimental results for linear response and quadratic response were conducted. Even though the highest correlation was observed for the quadratic response, observed and predicted values are not in good agreement ($R^2 = 0.65$). It means, predicted values for any values of independent variables would not be representative of the real conditions. Therefore, predictions and evaluations of peak symmetry for E3 were not made.

EE2 is the only synthetic estrogenic hormone in the mixture of hormones used. In fact, it is the major concern in the wastewater. It does not form conjugates and hardly transformed to other forms. Statistical analysis for peak symmetry of EE2 indicated that model coefficients, $\% ACN_m$ and $\% ACN_s$ are significant factors that affect peak symmetry. Correlation coefficient was R^2 =0.93 which proves a good agreement between observed and predicted values. Figure 3.7 depicts variation of PS of EE2 with flow and $\% ACN_s$ at $ACN_m = 40\%$. The relationship between independent variables and response looks like linear, but there is slight curvation in the response.

% ACN_s has got a very significant effect on peak symmetry. Decrease in %ACN_s resulted in a significant destruction in peak symmetry. PS value was around 1 when ACN_s is 90% at flow 400 μ L/min and then raised up to 3.0 when ACN_s= 15% at the same flow rate. Flow rate has not got a substantial effect on PS of EE2.

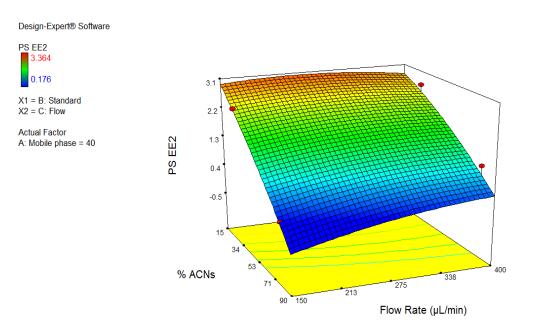


Figure 3.7 Variation of PS of EE2 with flow and $%ACN_s$ at $ACN_m = 40\%$.

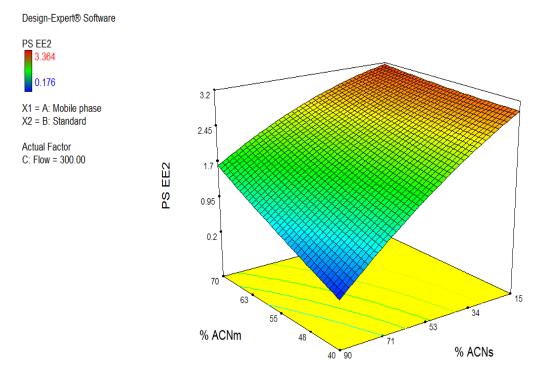


Figure 3.8 Variation of PS of EE2 with $\% ACN_m$ and $\% ACN_s$ at flow rate 300 $\mu L/min.$

Figure 3.8 shows effect of %ACN_m and %ACN_s on PS of EE2 at constant flow rate 300 µL/min. PS value increases from 0.3 to 1.7 linearly with the increase in mobile phase ACN concentration from 40% and 70% at 90% ACN_s. PS value varies between 0.77 to 1.7 for the suggested ACN_m concentrations. The most suitable ACN_m is 40% to 50% under this condition to obtain PS around 1. % ACN_s has got more significant effect on PS. The decrease in ACN_s from 90% to 15% for 40% ACN_m resulted in a significant shift in PS from 0.2 to 3.0 which indicate a considerable tailing in chromatogram for these extreme conditions. For the best PS value of EE2 chromatogram, % ACN_m should be around 70%.

3.1.3 Effect of Independent Variables on Resolution Factors

Resolution factor was the second response in CCD. In other words, resolution factor was also calculated for the same experimental conditions as conducted for peak symmetry. Table 3.11 depicts the variance analysis of peak symmetry for E2, E3 and EE2. Resolution factor of E2 was calculated with regard to E1. Therefore, no significance analysis was carried out for E1. As seen from the table, %ACN_s, % ACN_m and flow are significant factors for RF of E2 and E3. However, flow is not significant for Rf of EE2. Since retention time of EE2 is quite longer than that of other hormones. All two level interactions for E2 and E3 are significant. Only, interaction between % ACN_m and % ACN_s is significant for E2. In summary, the resolution factor should be optimized for all factors in the case of E2 and E3, but it is only necessary to conduct optimization of RF with regard to % ACN_s and %ACN_m in the case of EE2.

The following response equation 3.6 was developed and coefficients were determined by regression analysis (Table 3.12). Predicted responses for any value of studied range of factors were calculated by using these coefficients. 3D plots were used to evaluate the effect of the factors on resolution factors.

$$Y = b_0 + b_1 X_1 + b_2 X_2 + b_3 X_3 + b_{12} X_1 X_2 + b_{13} X_1 X_3 + b_{23} X_2 X_3 + b_{123} X_1 X_2 X_3 + b_{11} X_1^2 + b_{22} X_2^2 + b_{33} X_3^2$$
(3.6)

| Source of variation | | E2 | E3 | EE2 |
|--|--|---------------------|---------------------|---------------------|
| Coded | Actual | p-value Prob > F | p-value Prob > F | p-value Prob > F |
| М | Model | < 0.0001 | < 0.0001 | 0.0105 |
| X ₁ | % ACN in mobile phase | < 0.0001 | < 0.0001 | 0.0036 |
| X ₂ | % ACN in stationary phase | 0.0003 | 0.0003 | 0.0034 |
| X ₃ | Flow rate | 0.0345 | 0.0345 | 0.0777 |
| X ₁ X ₂ | Interatction between mobile phase and Stationary pahse | 0.0001 | 0.0001 | 0.0244 |
| X ₁ X ₃ | % ACN in mobile phase vs Flowrate | 0.0533 | 0.0533 | 0.9994 |
| X ₂ X ₃ | % ACN in stationary phase vs flowrate | 0.0174 | 0.0174 | 0.4016 |
| X ₁ ² | Quadratic effect of mobile phase | 0.0030 | 0.0030 | 0.1425 |
| X ₂ ² | Quadratic effect of stationary phase | 0.0141 | 0.0141 | 0.0998 |
| X_{3}^{2} | Quadratic effect of flowrate | 0.9401 | 0.9401 | 0.1548 |
| X ₁ X ₂ X ₃ | Three factor interaction | 0.0088 | 0.0088 | 0.2316 |
| Lack of Fit | 1 | 0.3656 | < 0.0001 | 0.0122 |

Table 3.11 ANOVA analysis of resolution factor for estrogenic hormones.

| Table 3.12 Regression of | coefficients of | resolution f | actor response | equation for | or estrogenic hormones. |
|--------------------------|-----------------|--------------|----------------|--------------|-------------------------|
| ruere erre regression e | | | actor response | equation is | |

| Coefficient of | f Coefficients for E2 | Coefficients for E3 | Coefficients for EE2 |
|-------------------|-----------------------|---------------------|----------------------|
| response equation | | | |
| b ₀ | +3.80738 | +13.67961 | 1.15165 |
| b ₁ | -0.086864 | -0.25848 | -7.23E+02 |
| b ₂ | -0.020127 | -0.11250 | -0.013287 |
| b ₃ | -2.86E+02 | -0.018813 | -2.63E+02 |
| b ₁₂ | 3.39E+01 | 2.02E+02 | 2.56E+01 |
| b ₂₃ | 4.53E+00 | 2.78E+01 | 2.60E+00 |
| b ₂₃ | 4.62E+00 | 2.65E+01 | 3.08E+00 |
| b ₁₁ | 4.45E+01 | 7.60E+01 | -9.47E+00 |
| b ₂₂ | -4.55E+00 | -2.03E+01 | -3.90E+00 |

| b ₃₃ | -1.01E-01 | -2.02E-02 | 1.32E-01 |
|--------------------|-----------|-----------|-----------|
| b ₁₂₃ | -5.87E-02 | -3.89E-01 | -4.73E-02 |
| R^2 | 0.9526 | 0.9819 | 0.8772 |
| Adequate precision | 14.231 | 23.622 | 9.570 |

Table 3.12 Regression coefficients of resolution factor response equation for estrogenic hormones (continued)

Figure 3.9 depicts variation of resolution factor of E2 with respect to E1 at different %ACN_s and % ACN_m concentrations (flow = $300 \mu L/min$). The higher the RF, better the resolution. Therefore, figure were plotted to obtain the highest RF values. As seen from figure, the highest RF value (0.64) is obtained at the lowest concentration of ACN in mobile phase and in standard solution. The effects of different flow rate and $%ACN_m$ on RF of E2 at $%ACN_s = 25$ is given in Figure 3.10. RF increases from 0.01 to 0.8 at the lowest flow rate of 150 μ L/min when % ACN_m was decreased from 70% to 40%. On the other hand, increasing flow rate from 150 to 400 µL/min at 40% ACN_m does not provide a substantial improvement in RF value of E2. There is an only increase from 0.4 to 0.8 in RF for the mentioned conditions. Therefore, it can be concluded that % ACN_m is more significant factor than flow in the resolution of E1 and E2 peaks. Finally, variation of RF with flow and %ACNs at 40% ACN_m was evaluated and results were given in Figure 3.11. The highest RF value was observed as 0.82 at flow= 150 μ L/min and % ACN_s= 15%. The effect of % ACN_s is more subtantial at flow rate= 150 μ L/min compared to flow= 400 μ L/min. The RF rises from 0.2 to 0.8 for the former case. In summary, the results indicate that the maximum RF value around 0.8 for E2 can be obtained at flow rate= 150 μ L/min, % ACN_m= 40 and % ACN_s= 15.

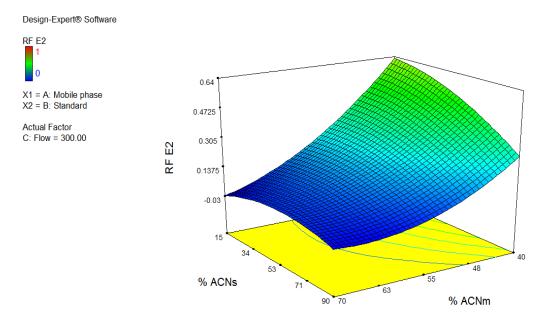
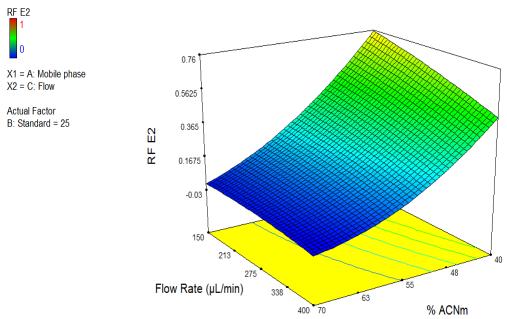


Figure 3.9 Variation of RF of E2 with $\% ACN_m$ and $\% ACN_s$ at flow rate 300 $\mu L/min.$



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Figure 3.10 Variation of RF of E2 with % ACN_m and flow rate at % ACN_s = 25.

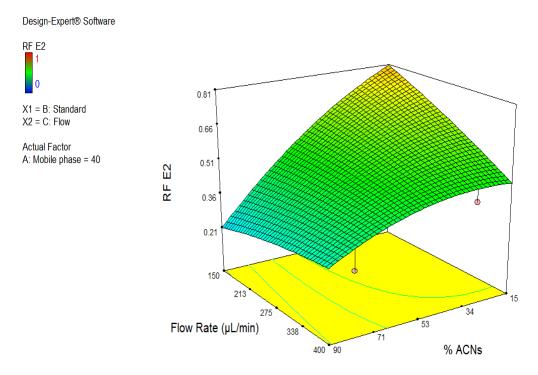


Figure 3.11 Variation of RF of E2 with flow and %ACNs at 40% ACNm.

E3 is eluted from the coloum after E2. Therefore resolution factor of E3 was calculted with regard to E2. Figure 3.12 shows of resolution factor of E2 at different $%ACN_s$ and $%ACN_m$ concentrations (flow = 300 µL/min). The highest resolution factor is obtained as RF=2.3 when ACN_m = 40% and ACN_s = 15%. However, almost no resolution can be obtained for 70% ACN_m . Similarly, resolution was too low at 90% ACN_s any value.

The effects of different flow rates and %ACN_m on RF of E3 at %ACN_s = 25 is given in Figure 3.13. RF increases from 0.00 to 3 at the lowest flow rate of 150 μ L/min when % ACN_m was decreased from 70% to 40%. On the other hand, increasing flow rate from 150 to 400 μ L/min at 40% ACN_m does not provide a substantial improvement in RF value of E3. The increase in RF value was only from 2.1 to 3.0. Therefore, it can be concluded that % ACN_m is more significant factor than flow in the resolution of E2 and E3 peaks.

Finally, the highest value of RF (3.2) of E3 was observed at conditions when flow rate and ACN_s are minimum (ACN_m= 40%) as given in Figure 3.14. The effect of %ACN_s is more subtantial at flow rate= 150 μ L/min compared to flow= 400 μ L/min.

In summary the results indicate that maximum RF value around 3 for E3 can be obtained at flow rate= $150 \mu L/min$, % ACN_m= 40 and % ACN_s= 15.

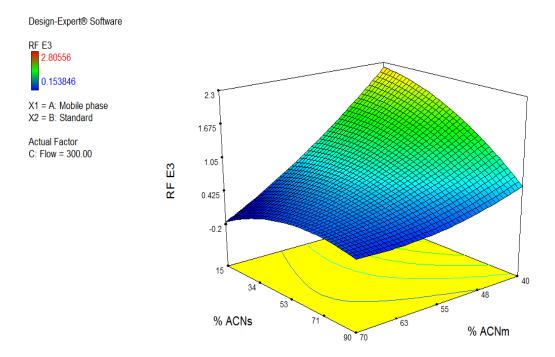


Figure 3.12 Variation of RF of E3 with % ACN_{m} and % ACN_{s} at flow rate 300 $\mu L/min.$

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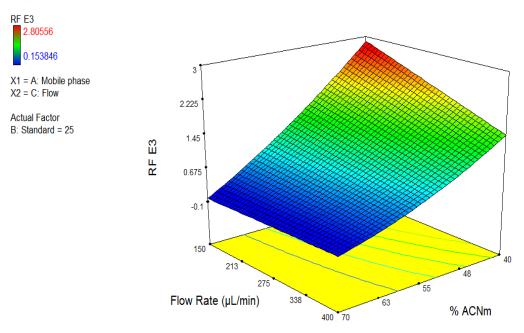


Figure 3.13 Variation of RF of E3 with % ACN_m and flow rate at 25 % ACN_s .

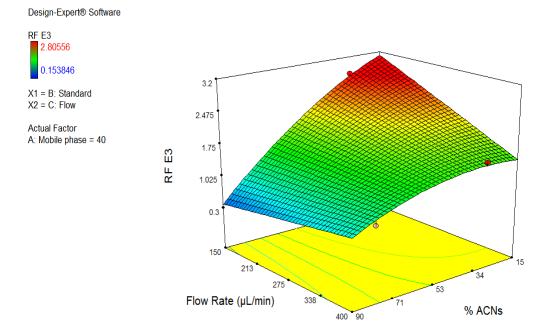


Figure 3.14 Variation of RF of E3 with % ACNs and flow rate at 40 % ACNm.

Under the different %ACN_s and % ACN_m conditions, variation of RF of EE2 was shown in figure 3.15. The flow rate was kept constat at 300 μ L/min in this figure. %ACN_s can be said insignificant factor for RF of E3 at 70 % ACN_m. However,

when ACN_m is decreased from 70% to 40%, ACN_s becomes a significant factor. Similarly, no significant variation in RF is observed for different ACN_s at 70% ACN_m . However, the combined effect of these two factor when they are at low level increases the response from 0.09 to 0.36.

Figure 3.16 depicts variation of resolution factor of EE2 with respect to E3 at different % ACN_m and flow rate when %ACN_s = 25. As seen from figure, the highest RF value (0.45) is obtained at the lowest concentration of ACN in mobile phase and lowest flow rate. Finally, variation of RF with flow and %ACN_s at 40% ACN_m was evaluated and results are given in Figure 3.17. The highest RF value was observed as 0.48 at flow = 150 μ L/min and % ACN_s= 15%. The effect of %ACN_s is more subtantial at flow rate= 150 μ L/min compared to flow= 400 μ L/min. In summary the results indicate that the maximum RF value around 0.4 for EE2 can be obtained at flow rate= 150 μ L/min, % ACN_m= 40 and % ACN_s= 15.

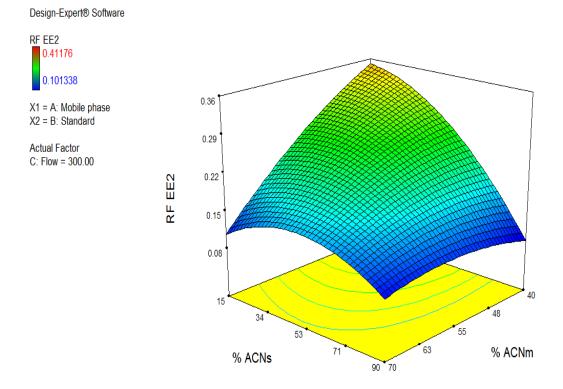


Figure 3.15 Variation of RF of EE2 with % ACN_m and % ACN_s at flow rate 300 $\mu L/min.$

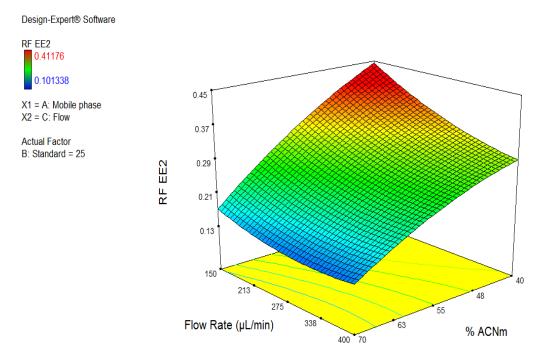


Figure 3.16 Variation of RF of EE2 with % ACN_m and flow rate at 25 % ACN_s .

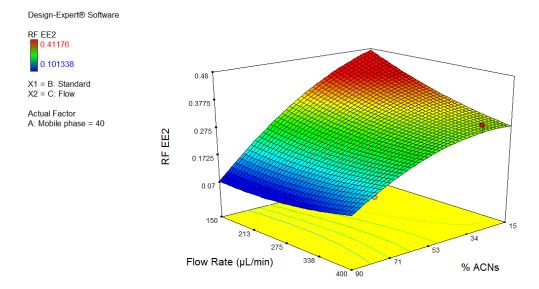


Figure 3.17 Variation of RF of EE2 with $\% ACN_s$ and flow rate at 40 $\% \ ACN_m$

Table 3.13 indicates the observed and predicted values for the experimental points which are different than the design points. This study was conducted to ensure that response equations can be used to predict the response. The observed and predicted values are very close to each other for most of the cases. This result indicates that response equations developed for RF can be used to predict RF values for any values of independent variables.

| Experimental Points | Mobile Phase % Acn | Standard Solution % ACN | Flow Rate µL/min | RF E2 (Predicted / Observed) | RF E3 (Predicted / Observed) | RF EE2 (Predicted / Observed) |
|------------------------|--------------------------|-------------------------------|------------------------|------------------------------------|------------------------------------|-------------------------------------|
| 2-1 | 45 | 25 | 250 | 0.5025 / 0.3506 | 1.8993 / 1.3571 | 0.3425 / 0.3750 |
| 6-1 | 50 | 20 | 200 | 0.4011 / 0.3150 | 1.6411 / 1.0000 | 0.3430 / 0.3442 |
| 6-2 | 55 | 15 | 400 | 0.1146 / 0.2187 | 0.5684 / 0.8214 | 0.2292 / 0.2857 |
| 10-1 | 40 | 25 | 300 | 0.615 / 0.6610 | 2.1365 / 1.7407 | 0.3406 / 0.5348 |
| 15-1 | 55 | 55 | 450 | 0.1267 / 0.1515 | 0.7171 / <mark>0.6667</mark> | 0.2391 / 0.2188 |

Table 3.13 Model verification at conditions different than design points.

In summary, the common operation conditions to get the best chromatogram in terms of peak symmetry were determined as % $ACN_m = 40$, % $ACN_s = 25$ and flow= 300 µL/min. The peak symmetry can be obtained around PS=1 under this conditions The conditions for resolution factor were as flow rate= 150 µL/min, % $ACN_m = 40$ and % $ACN_s = 15$. However, peak symmetry was selected as more imported for the chromotograms. In addition, resolution factor obtained as acceptable level around 0.6 to 1.7 depending on the hormone type for the former conditions. Figure 3.18 shows the chromatogram of 4 hormones obtained under this operation conditions.

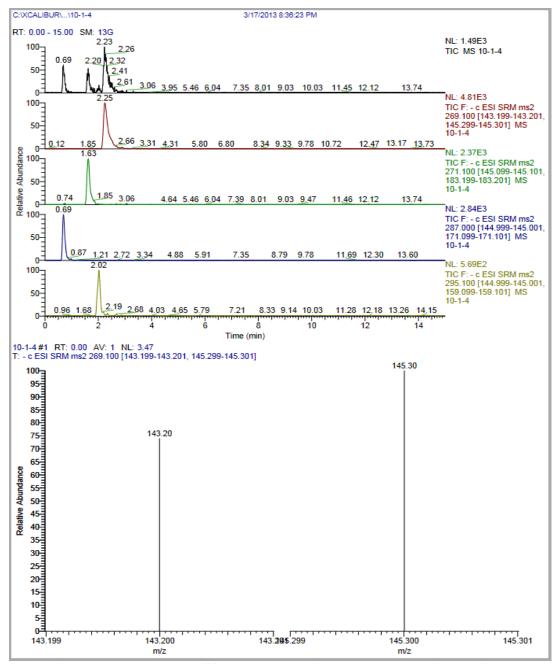


Figure 3.18 Chromatogram of four hormones obtained under this operation conditions.

3.2 The Effect of NH₄OH Concentration on Integration Area of Estrogenic Hormones

Some studies reported that addition of NH_4OH helps the ionization of hormones and increasing in integration area of hormones. In order to investigate the effect of NH_4OH concentration, the experiments were conducted at different NH_4OH (200mM in water) flow ratio between 3% and 17% in mobile phase and concentration of standard hormones solution to inject LC-MS/MS was fixed at 50 μ g/L. Control experiments without NH₄OH were conducted in parallel to the experiments with NH₄OH. NH₄OH was prepared in stock as 200 mM concentration and given to the colon from different line. % ACN in mobile phase was 40% and the flow rate was 300 μ L/min as determined in the previous section. No gradient was applied. The operation conditions for LC-MS/MS were summarized in Tables between 3.14 and 3.17.

Single factor experimental design method was used in order to evaluate if there is significant difference on integration area of the hormones for different concentrations of NH₄OH. The experiments were repeated 10 times. Variance analysis was conducted to determine if the concentration is a significant factor. Then Least Significant Difference test (LSD) was applied to the data to select the NH₄OH concentration which results in significantly higher integration area.

| Injection Volume (µL) | 25 μL |
|--|-------------|
| Needle Height from Bottom (mm) | 0.1 |
| Syringe Speed (µL/s) | 5 |
| Flush Volume (µL) | 400 |
| Flush / Wash Source | Wash Bottle |
| Wash Volume (µL) | 3000 |
| Flush Speed (µL/s) | 100 |
| Post-Injection Valve Switch Time (min) | 0 |
| Injection Mode | Full Loop |
| Tray Temperature (°C) | 25 |
| Column Oven Temperature (°C) | 25 |

Table 3.14 The auto sampler conditions for determination of %NH₄OH effect on integration area.

Table 3.15 Selected reaction mode conditions for determination of %NH₄OH effect on integration area.

| MS Acquire Time (min) | 15 |
|--|-----|
| Collision Gas Pressure (m Torr) [*] | 1.5 |
| Cycle Time (S) | 0.5 |

 $^{(*)}$ 1 mTorr = 0.000001315789473684 atm = 0.000001333223684211 bar

| | Parent | Product | SRM | Retention | Time | Tube | Polarity | Trigger | Name |
|---|--------|---------|-----------|-----------|--------|------|----------|---------|------|
| | Mass | Mass | Collision | Time | Window | Lens | | | |
| | | | Energy | | | | | | |
| 1 | 269.1 | 143.2 | 51 | 7.50 | 15.00 | 85 | - | 0 | E1 |
| 2 | 269.1 | 145.3 | 38 | 7.50 | 15.00 | 85 | - | 0 | E1 |
| 3 | 271.1 | 145.1 | 43 | 7.50 | 15.00 | 85 | - | 0 | E2 |
| 4 | 271.1 | 183.2 | 41 | 7.50 | 15.00 | 85 | - | 0 | E2 |
| 5 | 287.0 | 145.0 | 37 | 7.50 | 15.00 | 85 | - | 0 | E3 |
| 6 | 287.0 | 171.1 | 38 | 7.50 | 15.00 | 85 | - | 0 | E3 |
| 7 | 295.1 | 145.0 | 45 | 7.50 | 15.00 | 85 | - | 0 | EE2 |
| 8 | 295.1 | 159.1 | 37 | 7.50 | 15.00 | 85 | - | 0 | EE2 |

Table 3.16 SRM conditions for determination of %NH₄OH effect on integration area.

Table 3.17 The interface conditions for determination of %NH₄OH effect on integration area.

| Capillary Temperature (°C) | 280 |
|--|-----------|
| Vaporizer Temperature (°C) | 120 |
| Sheath Gas Pressure (Arb) | 25 |
| Aux Gas Pressure (Arb [*]) | 20 |
| Ion Sweep Gas Pressure (Arb) | 2.0 |
| Spray Voltage (V) (positive/negative polarity) | 2800/3500 |

^(*)Arb (arbitrary)

3.2.1 Effect of % NH₄OH on Integration Area of E1

Tables 3.18 depict the variance analysis of different NH₄OH concentrations on integration area (A) of E1. The statistical analysis indicated that concentration of NH₄OH significantly affect the response area. The expectation with the addition of NH₄OH was increase in the response area with the increase in NH₄OH concentration. Figure 3.19 shows that mean integration area of E1 for 10 replicates at different NH₄OH concentrations. It was A=369647 when no NH₄OH was added into mobile phase (See appendix Table 1). However mean area increased to A=840446 for 3% NH₄OH. A slight increase to A=851879 was observed at 5% NH₄OH. On the other hand, further increase in NH₄OH resulted in decreasing in mean integration area. The resulting mean area varied between A=756640 and A=572232 for NH₄OH concentrations 7% to 17%, respectively. These results indicate that the highest peak areas can be obtained at NH₄OH = 3%-5%. LSD test indicated that there is no

significant difference between 3% and 5% in terms of the integrating area (See appendix Table 2). Therefore, the lowest concentration of NH_4OH to get the highest integration area of E1 can be determined as 3%.

| ANOVA | | | | | | |
|---------------------|----------|----|-------------|-------------|----------|------------|
| Source of Variation | SS | df | MS | F | P-value | F crit |
| Between Groups | 1.69E+12 | 6 | 2.81086E+11 | 22.97206454 | 7.07E-14 | 2.25405301 |
| Within Groups | 7.34E+11 | 60 | 12235992113 | | | |
| | | | | | | |
| Total | 2.42E+12 | 66 | | | | |

Table 3.18 ANOVA for integration area of E1 at different NH₄OH concentrations.

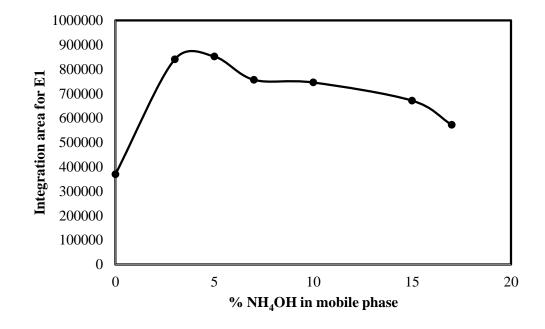


Figure 3.19 Variation of integration area of E1 with % NH₄OH concentration in mobile phase.

3.2.2 Effect of % NH₄OH on Integration Area of E2

The effect of NH₄OH concentration on ionization of E2 was almost the same as E1. The statistical analysis indicated that concentration of NH₄OH significantly affected the response area (Table 3.19). Variation of E2 integration area with NH₄OH is depicted in Figure 3.20. Mean integration area was 165799 when no NH₄OH was added into mobile phase (See appendix Table 3). A substantial increase

to A=388481 and A=408593 when NH₄OH was increased to 3% and 5%, respectively. Higher concentrations of NH₄OH adversely affected the area which varied between A=324443 and A=288114 for NH₄OH concentrations 7% to 17%, respectively. As a result of this study, the maximum area were obtained at NH₄OH= 3%-5%. LSD test indicated that there is no significant difference between 3% and 5% in terms of the integrating area (See appendix Table 4). Therefore, the lowest concentration of NH₄OH to get the highest integration area of E2 can be determined as 3%.

Table 3.19 ANOVA analysis of different NH_4OH concentration in mobile phase on integration area of E2.

| ANOVA | | | | | | |
|---------------------|------------------|----|-----------------|--------|---------|--------|
| Source of Variation | SS | df | MS | F | P-value | F crit |
| Between Groups | 348233254464.299 | 6 | 58038875744.050 | 49.711 | 0.000 | 2.275 |
| Within Groups | 61878906924.108 | 53 | 1167526545.738 | | | |
| | | | | | | |
| Total | 410112161388.407 | 59 | | | | |

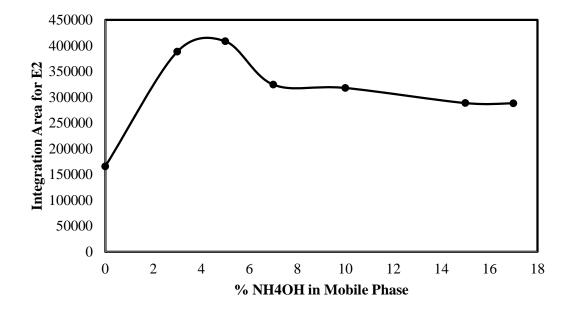


Figure 3.20 Variation of integration area of E2 with % NH₄OH concentration in mobile phase.

3.2.3 Effect of % NH₄OH on Integration Area of E3

The maximum integration area of E3 was obtained at the same NH₄OH concentrations as it was obtained for other hormones. NH₄OH concentration was significant for integration area of E3 (Table 3.20). Similar to the other hormones, the maximum area was achieved at 3% and 5% concentrations (See appendix Table 5) and response decreased for higher concentrations of NH₄OH. LSD test also proved that the integration areas for 3% or 5% were significantly different than no NH₄OH added or NH₄OH>5% conditions. The comparison between 3% and 5% resulted in that both concentrations give the same area (See appendix Table 6). For the sake of process simplicity and economy, 3% can be selected as optimal concentration for E3, too.

Table 3.20 ANOVA for integration area of E3 at different NH₄OH concentrations .

| ANOVA | | | | | | |
|---------------------|----------|----|-------------|------------|----------|---------|
| Source of Variation | SS | df | MS | F | P-value | F crit |
| Between Groups | 1.88E+11 | 6 | 31312780357 | 18.3729824 | 6.67E-12 | 2.25678 |
| Within Groups | 1.01E+11 | 59 | 1704284025 | | | |
| | | | | | | |
| Total | 2.88E+11 | 65 | | | | |

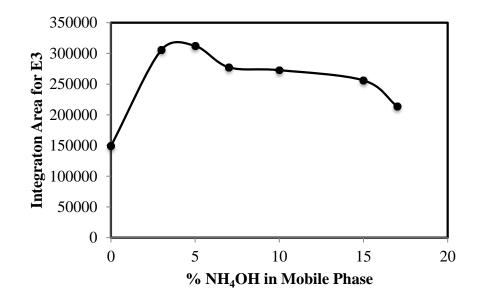


Figure 3.21 Variation of integration area of E3 with % NH₄OH concentration in mobile phase.

3.2.4 Effect of % NH₄OH on Integration Area of EE2

Variance analysis of different NH₄OH concentrations on integration area of EE2 was calculated and depicted in Table 3.21. ANOVA test results indicated that NH₄OH concentration is significant factor for EE2 ionization too. Mean integration area was maximized at NH₄OH = 3%-5% (Figure 3.22) (See appendix Table 7). LSD tests resulted in that there is no significant difference between 3% and 5% in terms of the integrating area (See appendix Table 8). Therefore, the lowest concentration of NH₄OH to get the highest integration area of EE2 was determined as 3%.

Table 3.21 ANOVA for integration area of EE2 at different NH₄OH concentrations.

| ANOVA | | | | | | |
|---------------------|----------|----|-------------|------------|----------|----------|
| Source of Variation | SS | df | MS | F | P-value | F crit |
| Between Groups | 3.79E+10 | 6 | 6313174006 | 20.1391802 | 9.67E-13 | 2.254053 |
| Within Groups | 1.88E+10 | 60 | 313477209.7 | | | |
| | | | | | | |
| Total | 5.67E+10 | 66 | | | | |

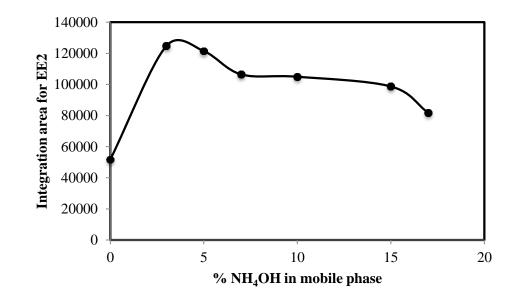


Figure 3.22 Variation of integration area of EE2 with % NH₄OH concentration in mobile phase.

In summary, addition of NH₄OH significantly improved integration area of hormones. Obtaining higher integration area for the same concentration helps

reducing LOD value. Therefore, it can be concluded that NH₄OH has got positive effect on measurement of hormones. Fortunately, 3% NH₄OH addition was optimal and common result for all hormones.

3.3 Determination of Ranges of Operation Parameters for the Measurement of Estrogenic Hormones in LC-MS/MS

The purpose of this study was to select the ranges of the independent instrumental operation variables in the analysis of estrogenic hormones in LC-MS/MS. In other words, the levels of the factors that will be used in optimization of the operating parameters were determined. The factors were sheath gas pressure, spray voltage, vaporizer temperature, aux gas pressure, capillary temperature, ion sweep gas pressure, collision gas pressure and cone position. Single factor experimental design method was used to determine the ranges of factors that significantly affect the response. ANOVA and LSD (Least Significant Difference) test were used for statistical analysis of the results. The response was Integration Area of hormones. The estrogenic hormone concentration was 500 ng/L in mix. Mobile phase was composed of acetonitrile (40%), water (57%) and NH₄OH (200 mM NH₄OH in water) (3%).

3.3.1 Determination of Sheath Gas Pressure Range

The range for sheath gas pressure was selected as SGP= 30 arb and SGP= 40 arb. Three levels; low level, center point and high level were SGP (-)= 30 arb, SPG (center)= 35 arb and SGP (+)= 40 arb, respectively. The other factors were kept constant as collision gas pressure (CGP) = 1.5 m.Torr, capillary temperature (CT) = 278 °C, vaporizer temperature (VT) = 258 °C, aux gas pressure (AGP) = 20 arb, ion sweep gas pressure (ISGP) = 2.0 arb and spray voltage (SV) = 3500 V (negative mode). The number of replicate was at least n=3 for each estrogenic. Table 3.22 shows the variance analysis for the effect of SGP on integration area of hormones. The statistical analysis clearly stated that SGP significantly affects (p<0.05) response area for E1, E2, and E3. However, sheath gas pressure was not a significant factor for the EE2. Figure 3.23 mean response of replicate at different sheath gas pressures. As seen from the Figure the highest integration area was observed at SGP= 35 arb for E1, E2 and E3.

Although it seems that there was substantial difference in terms of integration area for EE2 at different SGP (Figure 3.24), the mean of 4 replicates indicates no difference in integration area (Table 3.22).

LSD test resulted in that (Table 3.23) most significant differences for integration area for E1, E2 and E3 are between either 30 and 35 arb or 35 and 40 arb. This result means that SGP= 35 arb gives a significantly different integration area compared to that of other SGPs (See appendix Table 9). However, level of SGP does not affect the integration area of EE2. The result of LSD test is in parallel to the results of ANOVA test. In summary, the sheath gas pressure value was determined as SGP= 35 arb for the further experiments of this section.

Table 3.22 ANOVA result for the significance of sheath gas pressure on integration area of hormones in LC-MS/MS.

| Source of Variation | F | P-value | F critic | Result |
|---------------------|------------|-----------|-----------|---------------|
| SGP for E1 | 22.7332669 | 0.000867 | 4.737414 | Significant |
| SGP for E2 | 27.6472086 | 0.0004756 | 4.7374141 | Significant |
| SGP for E3 | 5.30814914 | 0.0300134 | 4.2564947 | Significant |
| SGP for EE2 | 4.13230263 | 0.0533195 | 4.2564947 | Insignificant |

| Hormone | Levels | $(\overline{Y}_i - \overline{Y}_j)$ | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
|---------|----------|-------------------------------------|----------------------------|--------------------------------|
| | 30 vs 35 | -7146 | 3453 | Significant |
| | 30 vs 40 | 2035 | 3691 | Insignificant |
| E1 | 35 vs 40 | 9181 | 3453 | Significant |
| E2 | 30 vs 35 | -3110 | 1156 | Significant |
| | 30 vs 40 | -78 | 1236 | Insignificant |
| | 35 vs 40 | 3032 | 1156 | Significant |
| E3 | 30 vs 35 | -2503 | 2650 | Insignificant |
| | 30 vs 40 | 1245 | 2650 | Insignificant |
| | 35 vs 40 | 3748 | 2650 | Significant |
| EE2 | 30 vs 35 | -985 | 1212 | Insignificant |
| | 30 vs 40 | -125 | 1212 | Insignificant |
| | 35 vs 40 | 860 | 1212 | Insignificant |

Table 3.23 LSD test for significance of sheath gas pressure levels on integration area of hormones.

*If $|t_{calculated}| > t_{critic}$, The difference between the means of the levels is significant.

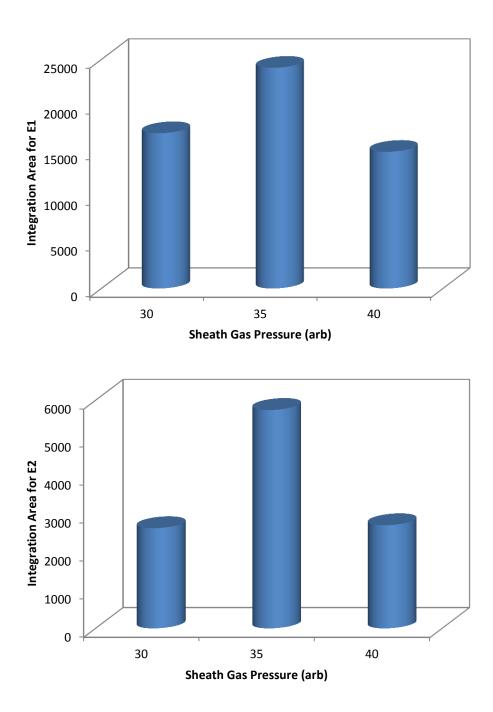


Figure 3.23 Variation of integration area of E1 and E2 with sheath gas pressure.

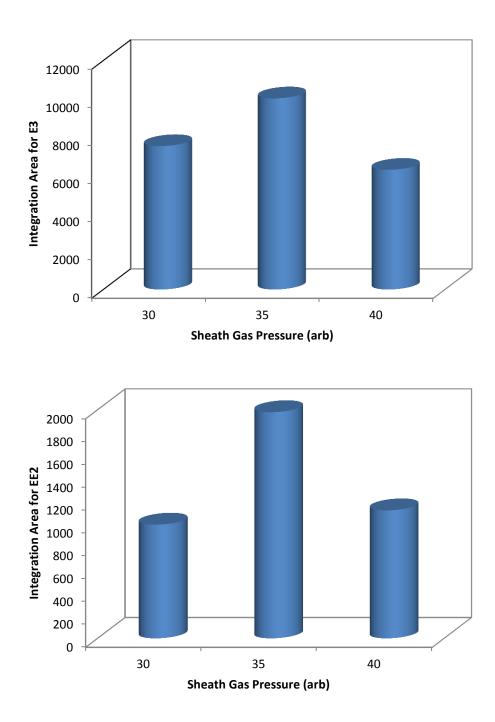


Figure 3.24 Variation of integration area of E3 and EE2 with sheath gas pressure.

3.3.2 Determination of Spray Voltage Range

A wide range spray voltage was available in LC-MS/MS. Therefore, effect of 7 different levels in the range of 2000 V to 3750 V was selected. Single factor with seven levels statistical design method was used to determine if the factor is

significant and then LSD test was applied to determine the most significantly different pairs of levels. In other words, LSD test was used to select the levels which are not significantly different from each other and result in the highest observed integration area for all estrogenic hormones.

ANOVA test showed that spray voltage is a significant factor on integration area of all hormones including EE2 (Table 3.24). Figure 3.25 depicts the variation of integration areas of E1 and E2 for different spray voltages. The high areas were observed at spray voltages between 2250 V and 3250 V for all hormones (See appendix Table 10). LSD test indicated that area obtained for E1 and E2 at SV= 2750 V is significantly higher than the area obtained at either SV= 2250 V and SV= 3250 V (Table 3.25). Similarly, Figure 3.26 depicts the effect of spray voltage on integration area of E3 and EE2. The maximum area obtained as A= 10000 for E3 at SV= 2750 V (See appendix Table 11). LSD test for this hormone gave that the response (integration area) obtained at 2750 V is significantly higher compared to the responses obtained at SV= 3500V and 3750 V. But, it was almost the same as ones observed at SV= 3000V and 3250 V. So, it is not necessary to keep the spray voltage above 2750 V for this hormone.

The highest area for EE2 was achieved at SV= 2250 V. However, LSD test indicated that the area at SV= 2250 V is not significantly different than the areas at spray voltage between SV= 2750 V and SV= 3000V. Although the maximum area was at SV= 2250 V, the spray voltage can be adjusted to SV= 2750 for EE2 (See appendix Tables 19 to 22 for LSD test).

In summary, the most suitable spray voltage was determined as SV= 2750 V for all hormones.

Table 3.24 ANOVA result for the significance of spray voltage on integration area of hormones in LC- MS/MS.

| Source of | | | | | | | |
|-----------|----------|----|-------------|------------|----------|----------|-------------|
| Variation | SS | df | MS | F | P-value | F critic | Result |
| E1 | 1.23E+09 | 6 | 205124388.6 | 11.4733787 | 1.83E-06 | 2.445259 | Significant |
| E2 | 73190514 | 6 | 12198419.02 | 7.9685823 | 4.53E-05 | 2.445259 | Significant |
| E3 | 1.62E+08 | 6 | 26977191.66 | 9.04536432 | 1.56E-05 | 2.445259 | Significant |
| EE2 | 10075369 | 6 | 1679228.181 | 4.53229833 | 0.002496 | 2.445259 | Significant |

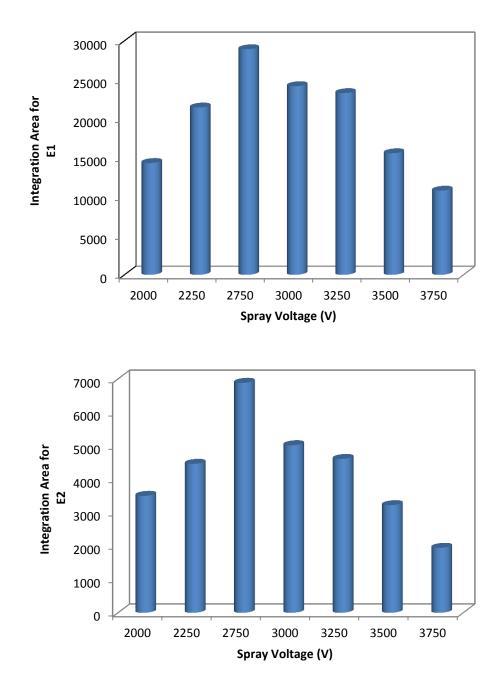
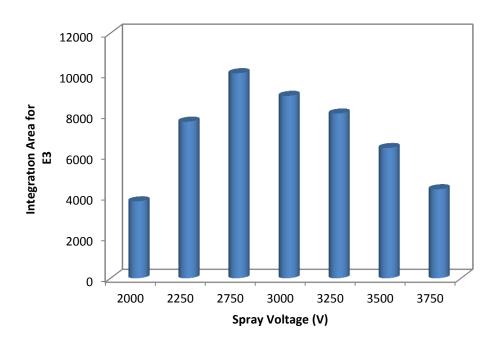


Figure 3.25 Variation of integration area of E1 and E2 with spray voltages.



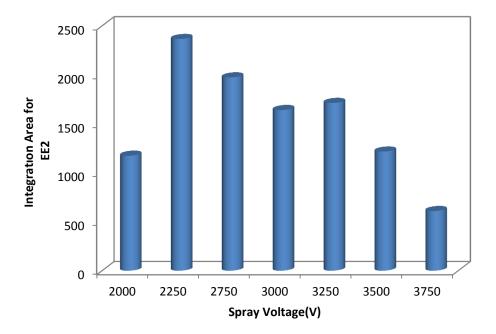


Figure 3.26 Variation of integration area of E3 and EE2 with spray voltages.

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | | |
|---------|--------------|-------------------------------------|----------------------------|--------------------------------|--|
| hormone | Levels | $t_{calculated}$ | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ | |
| | 2750 vs 3000 | 4732 | 5476.7502 | Insignificant | |
| | 2750 vs 3250 | 5624 | 5476.7502 | Significant | |
| E1 | 2750 vs 3500 | 13332 | 5476.7502 | Significant | |
| | 2750 vs 3750 | 18131 | 5476.7502 | Significant | |
| | 2750 vs 3000 | 1869 | 1603 | Significant | |
| | 2750 vs 3250 | 2280 | 1603 | Significant | |
| E2 | 2750 vs 3500 | 3664 | 1603 | Significant | |
| | 2750 vs 3750 | 4942 | 1603 | Significant | |
| | 2750 vs 3000 | 1109 | 2237 | Insignificant | |
| E3 | 2750 vs 3250 | 1973 | 2237 | Insignificant | |
| | 2750 vs 3500 | 3663 | 2237 | Significant | |
| | 2750 vs 3750 | 5682 | 2237 | Significant | |
| | 2250 vs 2750 | 392 | 788 | Insignificant | |
| | 2250 vs 3000 | 726 | 788 | Insignificant | |
| EE2 | 2250 vs 3250 | 653 | 788 | Insignificant | |
| | 2250 vs 3500 | 1150 | 788 | Significant | |
| | 2250 vs 3750 | 1757 | 788 | Significant | |

Table 3.25 LSD test results for significance of spray voltage levels on integration area of hormones.

3.3.3 Determination of Vaporizer Temperature Range

Vaporizer temperature was the third factor to be investigated. The range was between 200° C and 400° C. Number of level was 8 and the number of replicate was 5 at each level for all hormones. Spray voltage and sheath gas pressure were SV= 2750 V and SGP= 35 arb as determined in the previous experiments. The result of ANOVA test indicated that area of all hormones can change significantly as vaporizer temperature is changed (Table 3.26). In other words, levels of vaporizer temperature significantly affect the integration area.

Figure 3.27 depicts the variation of integration area of E1 and E2 at different vaporizer temperatures. The maximum area was obtained as A= 60000 at VT= 375 $^{\circ}$ C for E1 (See appendix Table 12). LSD test resulted in that this values are significantly higher than the value that can be obtained at VT= 400 $^{\circ}$ C at which the second highest area was observed (Table 3.27). In the case of E2, the area was the highest (A= 8000) at 375 $^{\circ}$ C, but the next closest area were observed at VT= 350 $^{\circ}$ C and 400 $^{\circ}$ C. However, LSD test indicated that the area obtained at 375 $^{\circ}$ C is significantly higher than that of at VT= 350 $^{\circ}$ C, but the area difference for VT= 375 $^{\circ}$ C and VT= 400 $^{\circ}$ C are not significantly different meaning that the system can be operated at VT= 375 $^{\circ}$ C for E2.

The situation was almost the same for E3. The two close integration areas were observed at VT= 375 °C and 400°C (See appendix Table 13). But, it was statistically proved that area at 375°C is significantly higher than the area obtained at 400 °C. Similarly, the highest area was achieved at VT=375°C for EE2 (Figure 3.28). Although, the values for VT= 375°C and 400°C are not statistically different, it is practical to operate the LC-MS/MS at around VT= 375 °C. As a result, VT was selected as VT= 375 °C for further optimization studies. (See appendix Tables 23 to 26 for more information about LSD test.)

| Type of hormone | SS | df | MS | F | P-value | F critic | Result |
|--------------------|-------------|----|-------------|-------------|-----------|-----------|-------------|
| E1 | 7147465552 | 7 | 1021066507 | 17 | 0 | 2 | Significant |
| E2 | 68613868.75 | 7 | 9801981.25 | 5.19 | 0.00 | 2.31 | Significant |
| E3 | 1397643157 | 7 | 199663308.1 | 26.92370718 | 1.072E-11 | 2.3127412 | Significant |
| EE2 | 32427791.15 | 7 | 4632541.593 | 9.850909004 | 1.709E-06 | 2.3127412 | Significant |

Table 3.26 ANOVA result for the significance of vaporizer temperature on integration area of hormones in LC- MS/MS.

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|---------|------------|-------------------------------------|----------------------------|--------------------------------|
| Hormone | Levels | t _{calculated} | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
| E1 | 375 vs 400 | 11342 | 9853 | Significant |
| | 375 vs 425 | 28183 | 9853 | Significant |
| | 375 vs 450 | 23018 | 9853 | Significant |
| | 375 vs 300 | -2878.64 | 1771.15 | Significant |
| E2 | 375 vs 400 | 563.16 | 1771.15 | Insignificant |
| | 375 vs 425 | 1818.42 | 1771.15 | Significant |
| | 375 vs 450 | 2704.19 | 1771.15 | Significant |
| E3 | 375 vs 400 | 3880 | 3510 | Significant |
| | 375 vs 425 | 10056 | 3510 | Significant |
| | 375 vs 450 | 10170 | 3510 | Significant |
| EE2 | 375 vs300 | -963 | 884 | Significant |
| | 375 vs 400 | 675 | 884 | Insignificant |
| | 375 vs 425 | 1335 | 884 | Significant |
| | 375 vs 450 | 1985 | 884 | Significant |

Table 3.27 LSD test results for significance of vaporizer temperature level on integration area of hormones.

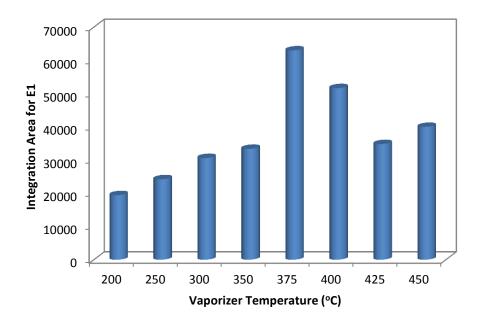


Figure 3.27 Variation of integration area of E1 and E2 with vaporizer temperature.

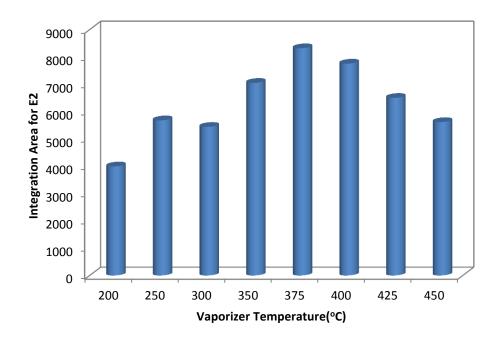


Figure 3.27 Variation of integration area of E1 and E2 with vaporizer temperature (continued).

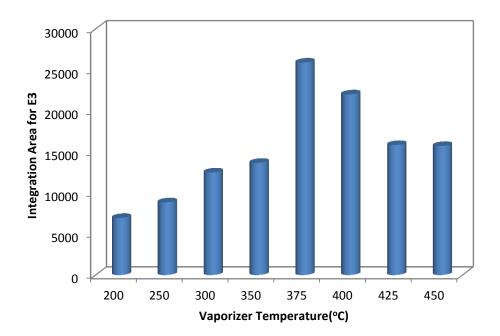


Figure 3.28 Variation of integration area of E3 and EE2 with vaporizer temperature.

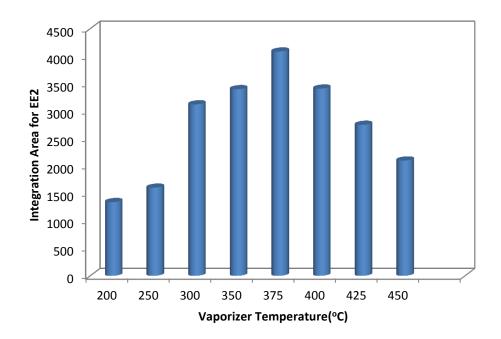


Figure 3.28 Variation of integration area of E3 and EE2 with vaporizer temperature (continued).

3.3.4 Determination of Aux Gas Pressure Range

Aux gas pressure (AGP) was varied between AGP= 5 arb to 20 arb. The number of level and replicate were 4 and 5, respectively. Spray gas voltage, vaporizer temperature and sheath gas pressure was kept constant at the value determined in the previous sections. ANOVA analysis indicated that there is no significant difference in integration area of all hormones when different aux gas pressures were used (Table 3.28), (See appendix Table 14). Integration area of hormones at different aux gas pressures were depicted in Figures from 3.29 to 3.30. Although it seems that there is some differences for different aux gas pressures, LSD test indicated that the difference between the integration areas of all hormones at different aux gas pressures is insignificant (Table 3.29). That means LC-MS/MS can be operated at any aux gas pressures and it was selected as AGP= 20 arb.

Table 3.28 ANOVA result for the significance of aux gas pressure on integration area of hormones in LC-MS/MS.

| Source of | | | | | | | |
|-----------|-------------|----|-------------|-------------|-----------|-----------|---------------|
| Variation | SS | df | MS | F | P-value | F critic | Result |
| E1 | 33102504.01 | 3 | 11034168 | 2.149427173 | 0.1340306 | 5.2922141 | Insignificant |
| E2 | 3661613.117 | 3 | 1220537.706 | 0.427232238 | 0.7362075 | 3.2388715 | Insignificant |
| E3 | 28215116.44 | 3 | 9405038.812 | 1.79175616 | 0.1892729 | 3.2388715 | Insignificant |
| EE2 | 1418437.354 | 3 | 472812.4515 | 0.298444152 | 0.8260087 | 3.2388715 | Insignificant |

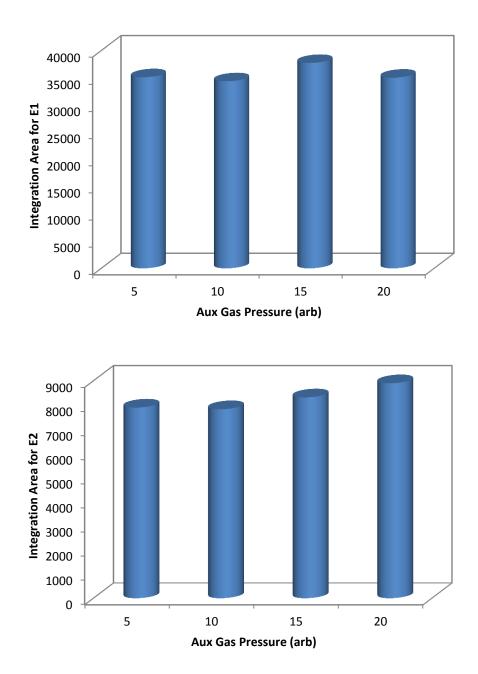


Figure 3.29 Variation of integration area of E1 and E2 with aux gas pressure.

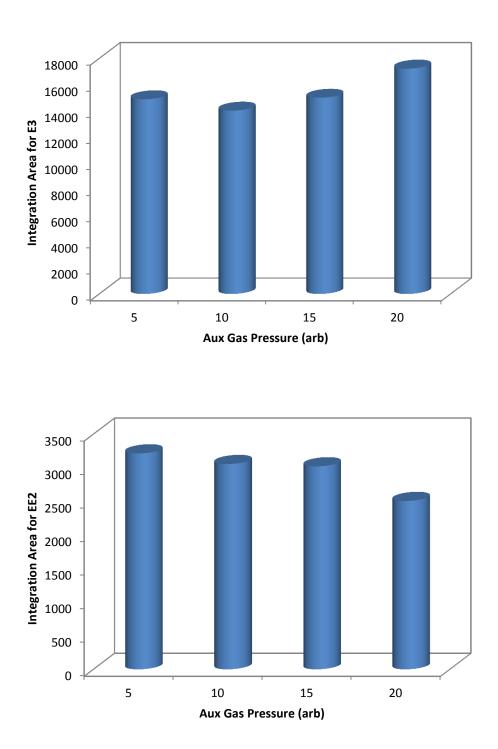


Figure 3.30 Variation of integration area of E3 and EE2 with aux gas pressure.

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|---------|----------|-------------------------------------|----------------------------|--------------------------------|
| hormone | Yi vs Yj | $t_{calculated}$ | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
| E1 | 5 vs 10 | 736 | 4186 | Insignificant |
| | 5 vs 15 | -2625 | 4186 | Insignificant |
| | 5 vs 20 | 81 | 4186 | Insignificant |
| | 10 vs 15 | -3361 | 4186 | Insignificant |
| | 10 vs 20 | -655 | 4186 | Insignificant |
| | 15 vs 20 | 2706 | 4186 | Insignificant |
| E2 | 5 vs 10 | 68 | 2266 | Insignificant |
| | 5 vs 15 | -422 | 2266 | Insignificant |
| | 5 vs 20 | -1006 | 2266 | Insignificant |
| | 10 vs 15 | -490 | 2266 | Insignificant |
| | 10 vs 20 | -1074 | 2266 | Insignificant |
| | 15 vs 20 | -584 | 2266 | Insignificant |
| E3 | 5 vs 10 | 871 | 4233 | Insignificant |
| | 5 vs 15 | -115 | 4233 | Insignificant |
| | 5 vs 20 | -2346 | 4233 | Insignificant |
| | 10 vs 15 | -986 | 4233 | Insignificant |
| | 10 vs 20 | -3217 | 4233 | Insignificant |
| | 15 vs 20 | -2231 | 4233 | Insignificant |
| EE3 | 5 vs 10 | 158 | 1688 | Insignificant |
| | 5 vs 15 | 192 | 1688 | Insignificant |
| | 5 vs 20 | 709 | 1688 | Insignificant |
| | 10 vs 15 | 34 | 1688 | Insignificant |
| | 10 vs 20 | 551 | 1688 | Insignificant |
| | 15 vs 20 | 516 | 1688 | Insignificant |

Table 3.29 LSD test results for significance of aux gas pressure levels on integration area of hormones.

3.3.5 Determination of Capillary Temperature Range

A narrow range was selected for capillary temperature (CT). It was between CT=300 °C and 350 °C. ANOVA test indicated that capillary temperature levels haven't got significant effect on integration area of E1, E3 and EE2. But it is significant for E2 (Table 3.30). Integration area for E1 was A= 45000 at CT= 300 °C but slightly decreased to around A= 35000 at CT= 350 °C (Figure 3.31). According to this result, it can be concluded increasing temperature adversely affect the

integration area (See appendix Table 15). However, LSD test statistically proof that the decrease in the area with the increase in temperature is not significant (Table 3.31). The similar effect can be observed for E3 and EE2 (Figure 3.32). But LSD test results indicated that no significant difference for the integration area of these hormones. Finally, E2 is affected by the levels of capillary temperature (Table 3.30), the highest area was obtained at CT= 300° C and that area was significantly different than ones obtained at CT= 325° C and 350° C. Capillary temperature was selected as CT= 300° C for the benefit of E2.

Table 3.30 ANOVA result for the significance of capillary temperature on integration area of hormones in LC-MS/MS.

| Source of | | | | | | | |
|-----------|-------------|----|-------------|-------------|-----------|-----------|---------------|
| Variation | SS | df | MS | F | P-value | F critic | Result |
| E1 | 187633558 | 2 | 93816778.98 | 3.132859771 | 0,0927606 | 4,2564947 | Insignificant |
| E2 | 27995798.9 | 2 | 13997899.45 | 5.077129113 | 0.0334116 | 4.2564947 | Significant |
| E3 | 18298921.33 | 2 | 9149460.664 | 1.110225863 | 0.3707189 | 4.2564947 | Insignificant |
| EE2 | 3414233.999 | 2 | 1707117 | 2.895340953 | 0.106941 | 4.2564947 | Insignificant |

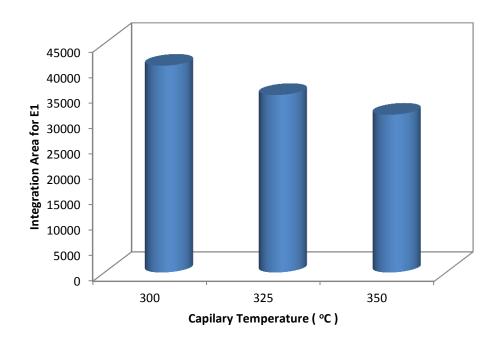


Figure 3.31 Variation of integration area of E1 and E2 with capillary temperature.

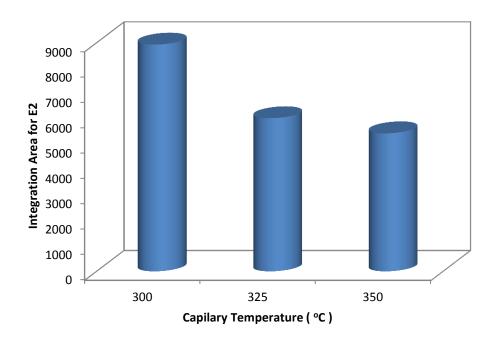


Figure 3.31 Variation of integration area of E1 and E2 with capillary temperature (continued).

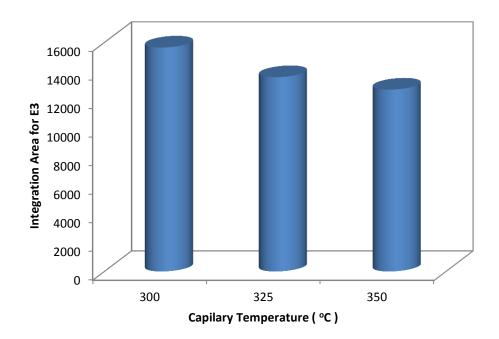


Figure 3.32 Variation of integration area of E3and EE2 with capillary temperature.

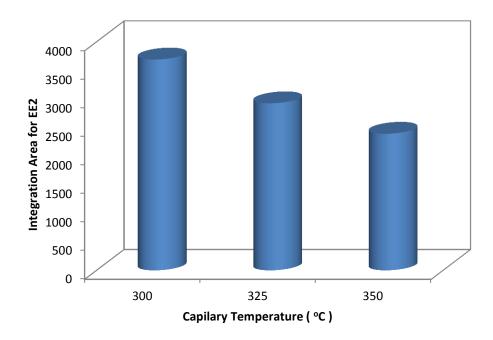


Figure 3.32 Variation of integration area of E3and EE2 with capillary temperature (continued).

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|---------|------------|-------------------------------------|----------------------------|--------------------------------|
| hormone | Levels | t _{calculated} | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| E1 | 300 vs 325 | 5756 | 12963 | Insignificant |
| | 300 vs 350 | 9624 | 12963 | Insignificant |
| | 325 vs 350 | 3869 | 12963 | Insignificant |
| E2 | 300 vs 325 | 2902 | 2656 | Significant |
| | 300 vs 350 | 3496 | 2656 | Significant |
| | 325 vs 350 | 594 | 2656 | Insignificant |
| E3 | 300 vs 325 | 2074 | 4592 | Insignificant |
| | 300 vs 350 | 2944 | 4592 | Insignificant |
| | 325 vs 350 | 869 | 4592 | Insignificant |
| EE2 | 300 vs 325 | 767 | 1765 | Insignificant |
| | 300 vs 350 | 1300 | 1765 | Insignificant |
| | 325 vs 350 | 533 | 1765 | Insignificant |

Table 3.31 LSD test results for significance of capillary temperature levels on integration area of hormones.

 $|\mathbf{F}|$ $|\mathbf{t}_{calculated}| > t_{critic}$, The difference between the means of the levels is significant.

3.3.6 Determination of Ion Sweep Gas Pressure Range

The experiments at different ion sweep gas pressures (ISGP) resulted in that this factor is not significant (Table 3.32). Even at different levels of these factors no substantial difference was observed for integration area (See appendix Table 16). As seen from Figures 3.33 and 3.34, the areas are very close to each other. LSD test statistically proves that changing sweep gas pressure does not affect the integration area (Table 3.33). Therefore, SGP was selected as SGP= 0 arb for the further experiments.

Table 3.32 ANOVA result for the significance of ion sweep gas pressure on integration area of hormones in LC-MS/MS.

| Source of | | | | | | | |
|-----------|-------------|----|-------------|-------------|-----------|-----------|---------------|
| Variation | SS | df | MS | F | P-value | F critic | Result |
| E1 | 7173249.081 | 2 | 3586624.541 | 0.498534537 | 0.6232527 | 4.2564947 | Insignificant |
| E2 | 5268792.042 | 2 | 2634396.021 | 1.881017459 | 0.2077072 | 4.2564947 | Insignificant |
| E3 | 1625143.081 | 2 | 812571.5405 | 0.174265694 | 0.8428417 | 4.2564947 | Insignificant |
| EE2 | 3611353.8 | 2 | 1805676.9 | 3.586679528 | 0.0715303 | 4.2564947 | Insignificant |

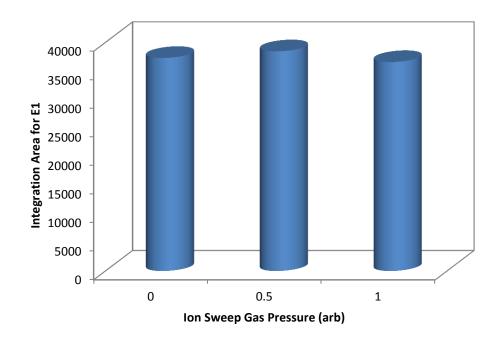


Figure 3.33 Variation of integration area of E1 and E2 with variable ion sweep gas pressure.

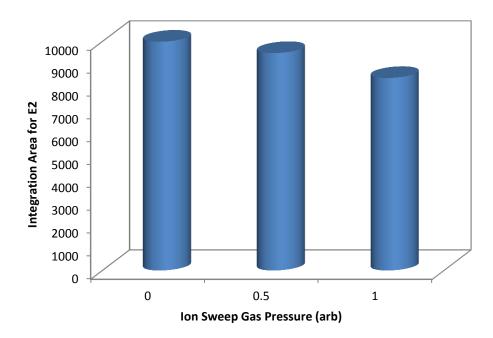


Figure 3.33 Variation of integration area of E1 and E2 with variable ion sweep gas pressure (continued).

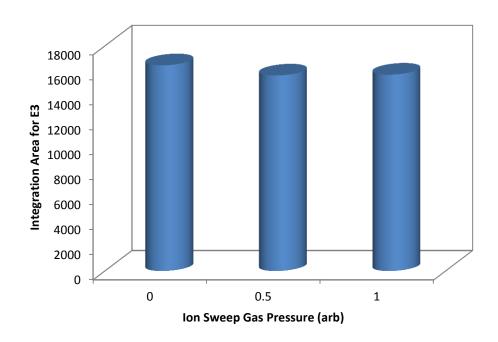


Figure 3.34 Variation of integration area of E3 and EE2 with variable ion sweep gas pressure.

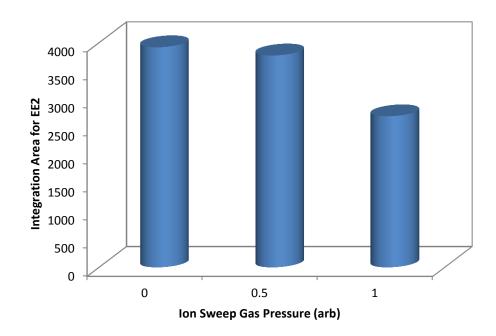


Figure 3.34 Variation of integration area of E3 and EE2 with variable ion sweep gas pressure (continued).

| Table 3.33 LSD test r | esults for significanc | e of ion sweep ga | s pressure levels on | integration area of |
|-----------------------|------------------------|-------------------|----------------------|---------------------|
| hormones. | | | | |

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|---------|----------|-------------------------------------|----------------------------|--------------------------------|
| hormone | Levels | $t_{calculated}$ | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| E1 | 0.5 vs 0 | 1166 | 4290 | Insignificant |
| | 0.5 vs 1 | 1875 | 4290 | Insignificant |
| | 0 vs 1 | 709 | 4290 | Insignificant |
| E2 | 0.5 vs 0 | -497 | 1893 | Insignificant |
| | 0.5 vs 1 | 1089 | 1893 | Insignificant |
| | 0 vs 1 | 1587 | 1893 | Insignificant |
| E3 | 0.5 vs 0 | -812 | 3454 | Insignificant |
| | 0.5 vs 1 | -67 | 3454 | Insignificant |
| | 0 vs 1 | 745 | 3454 | Insignificant |
| EE2 | 0.5 vs 0 | -147 | 1631 | Insignificant |
| | 0.5 vs 1 | 1083 | 1631 | Insignificant |
| | 0 vs 1 | 1230 | 1631 | Insignificant |

3.3.7 Range Determination for Cone Position

There are 3 positions on the cone. These are B, C and D. B position increases the distance between ionization point and sample injection point to ionization chamber. This distance can sometimes affect the amount of sample that enters to the ionization chamber. Therefore, this factor was considered as important to get better integration area. ANOVA test results indicated that cone position is a significant factor for integration area of E1, E2 and E3 (Table 3.34). The general trend of integration area for the different cone position is the increase in area as cone position was changed from B to D for these hormones (Figures 3.35 and 3.36). In other words, the highest area was observed at D position (See appendix Table 17). LSD test results depicts that there are significant differences between B position with respect to C and D positions. But, the difference is not significant for C and D positions.

The situation is quite different for EE2. Cone position is not significant and although there is a slight increase in the area as position was changed from B to D (Figure 3.36), this increase is not statistically significant (Table 3.35). In summary, D position was determined as the best.

Table 3.34 ANOVA result for the significance of cone position on integration area of hormones in LC-MS/MS.

| Source of | | | | | | | |
|-----------|-------------|----|-------------|-------------|-----------|-----------|---------------|
| Variation | SS | df | MS | F | P-value | F critic | Result |
| E1 | 526328775.2 | 2 | 263164387.6 | 28.28421128 | 0.0001315 | 4.2564947 | Significant |
| E2 | 30813020.48 | 2 | 15406510.24 | 17.18222307 | 0.0008453 | 4.2564947 | Significant |
| E3 | 170141837.9 | 2 | 85070918.93 | 47.2213957 | 1.69E-05 | 4.2564947 | Significant |
| EE2 | 2269094.62 | 2 | 1134547.31 | 1.913252066 | 0.2030504 | 4.2564947 | Insignificant |

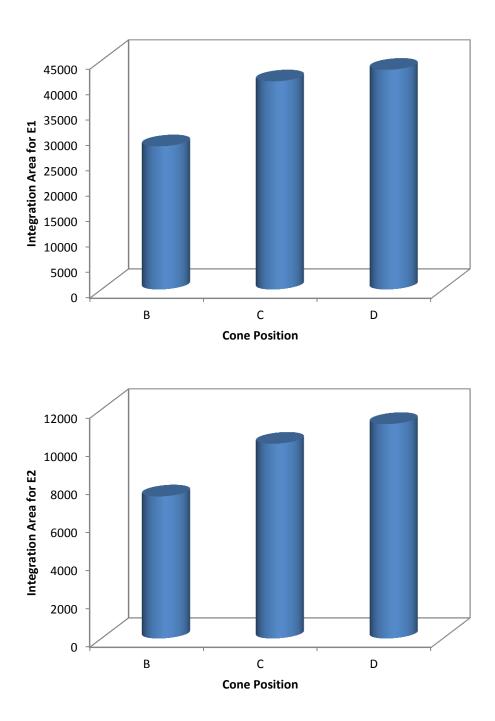
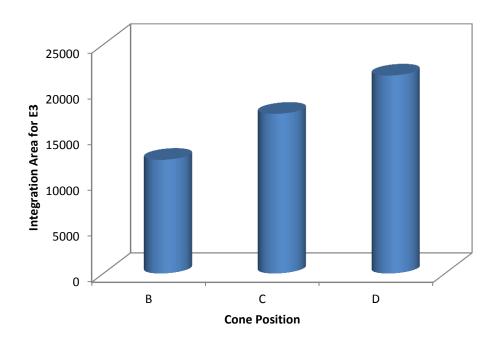


Figure 3.35 Variation of integration area of E1 and E2with cone position.



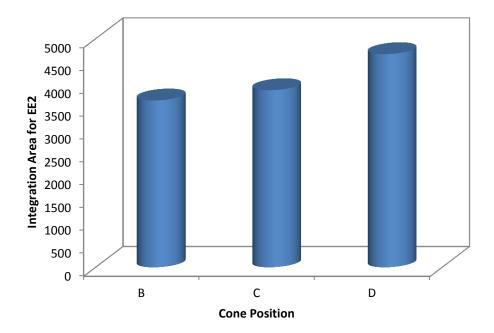


Figure 3.36 Variation of integration area of E3 and EE2 with cone position.

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|---------|--------|-------------------------------------|----------------------------|--------------------------------|
| hormone | Levels | t _{calculated} | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| E1 | B vs C | -12770 | 4879 | Significant |
| | B vs D | -15049 | 4879 | Significant |
| | C vs D | -2279 | 4879 | Insignificant |
| E2 | B vs C | -2764 | 1515 | Significant |
| | B vs D | -3795 | 1515 | Significant |
| | C vs D | -1031 | 1515 | Insignificant |
| E3 | B vs C | -5025 | 2147 | Significant |
| | B vs D | -9211 | 2147 | Significant |
| | C vs D | -4186 | 2147 | Significant |
| EE2 | B vs C | -225 | 1232 | Insignificant |
| | B vs D | -1014 | 1232 | Insignificant |
| | C vs D | -789 | 1232 | Insignificant |

Table 3.35 LSD test results for significance of cone position levels on integration area of hormones.

3.3.8 Determination of Collision Gas Pressure Range

The final instrumental operation parameter was collision gas pressure (CGP). The values for the other factor were adjusted to the values determined in the previous sections. ANOVA analysis resulted in that this factor has got a significant effect on integration area of all hormones including EE2 (Table 3.36). However, there are significant differences in areas obtained at different levels of collision gas pressure. For example, area obtained for E1 was A= 20000 at CGP= 1 arb and increased to A= 44000 at CGP= 1.5 arb and remained almost constant when CGP was 2 arb (See appendix Table 18). Statistical analysis of these results showed that the difference between CGP= 1 arb and CGP= 1.5 arb is significant but there is no significant difference between CGP= 1.5 arb and CGP= 2 arb (Figure 3.37). The situation was the same for EE2 (Figure 3.37). However, the most significant differences for E2 and E3 were observed at CGP= 1.5 arb and CGP= 2 arb. The highest integration area was obtained at CGP= 2 for these hormones (Figure 3.38 and Table 3.37). Therefore,

range for CGP value can be selected as 1.5 arb and 2 arb for optimization of these parameters in the further experiments.

| Source of Variation | SS | df | MS | F | P-value | F critic | Result |
|---------------------|-------------|----|-------------|-------------|-----------|-----------|-------------|
| E1 | 1364387505 | 2 | 682193752.6 | 285.9900283 | 7.167E-09 | 4.2564947 | Significant |
| E2 | 69260191.89 | 2 | 34630095.94 | 16.8914011 | 0.0008982 | 4.2564947 | Significant |
| E3 | 159126244.6 | 2 | 79563122.32 | 34.72619049 | 5.866E-05 | 4.2564947 | Significant |
| EE2 | 7920604.597 | 2 | 3960302.298 | 5.500366381 | 0.0275033 | 4.2564947 | Significant |

Table 3.36 ANOVA result for the significance of collision gas pressure on integration area of hormones in LC-MS/MS.

Table 3.37 LSD test results for significance of collision gas pressure levels on integration area of hormones.

| Type of | | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|---------|----------|-------------------------------------|----------------------------|--------------------------------|
| hormone | Levels | t _{calculated} | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
| E1 | 1 vs 1.5 | -21877 | 2470 | Significant |
| | 1 vs 2 | -23295 | 2470 | Significant |
| | 1.5vs 2 | -1418 | 2470 | Insignificant |
| E2 | 1.5 vs 1 | 3789 | 2290 | Significant |
| | 1.5 vs 2 | -2005 | 2290 | Insignificant |
| | 1 vs 2 | -5794 | 2290 | Significant |
| E3 | 1.5 vs 1 | 7266 | 2421 | Significant |
| | 1.5 vs 2 | -848 | 2421 | Insignificant |
| | 1 vs 2 | -8114 | 2421 | Significant |
| EE2 | 1.5 vs 1 | 1.5 vs 1 | 1916 | Significant |
| | 1.5 vs 2 | 1.5 vs 2 | 493 | Insignificant |
| | 1 vs 2 | 1 vs 2 | -1423 | Significant |

*If $\mid t_{calculated} \mid$ > t_{critic} , The difference between the means of the levels is significant.

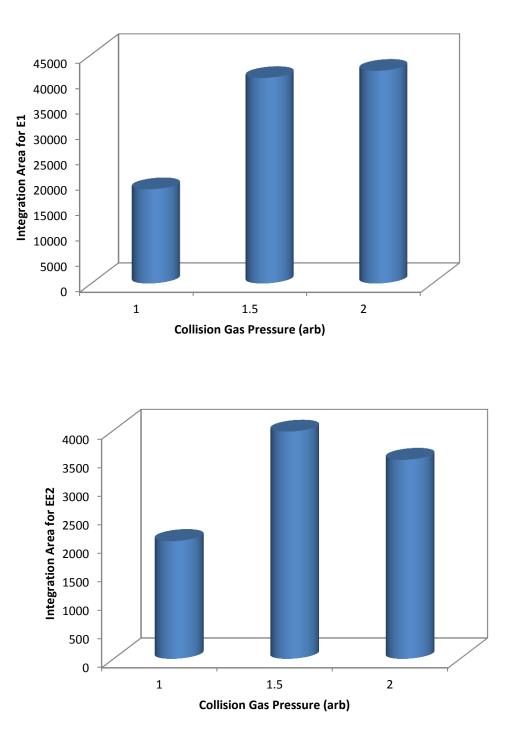


Figure 3.37 Variation of integration area of E1and EE2 with collision gas pressure.

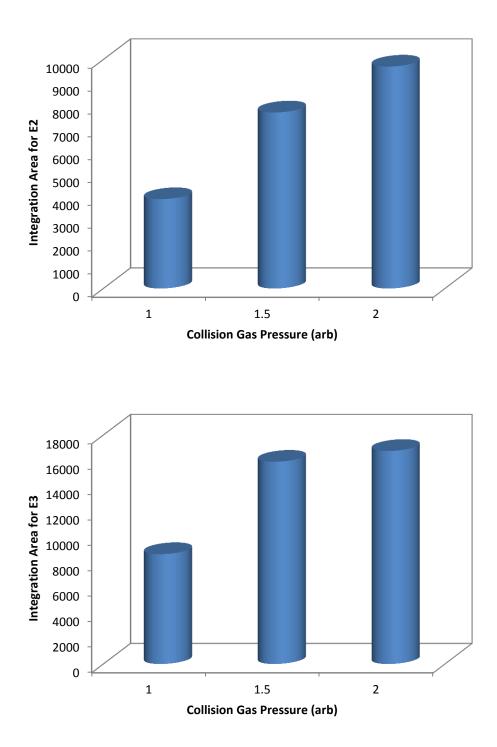


Figure 3.38 Variation of integration area of E2 and E3 with collision gas pressure.

Table 3.38 summarizes the instrument operation conditions which significantly affect the integration area of hormones. As seen from table, the significant factors are sheath gas pressure, spray voltage, vaporizer temperature, cone position and collision

gas pressure. On the other hand, capillary temperature, ion sweep gas pressure and aux gas pressure do not significantly affect the response area (Table 3.39).

| Hormones | Sheath Gas | Spray Voltage | Vaporizer | Cone Position | Collision Gas |
|----------|-----------------------------|------------------------------------|------------------|---------------|---------------|
| | Pressures (arb) | (V) | Temperature (°C) | Range Max | Pressure Max |
| | | | | | |
| E1 | 35 | 2750 | 375 | D | 2 |
| E2 | 35 | 2750 | 375 | D | 2 |
| E3 | 35 | 2750 | 375 | D | 2 |
| EE2 | Not effect between 30-40 | No effect between 2250- 2750 | 375 | D | 2 |

Table 3.38 The values of significant LC-MS/MS operation factor to obtain high integration area of hormones.

Table 3.39 The insignificant LC-MS/MS operation factor for integration area of hormones.

| Hormones | mones Capillary Temperature °C | | Aux Gas Pressure, (arb) | |
|----------|--------------------------------|---------------|-------------------------|--|
| | | (arb) | | |
| E1 | No effect 300-350 | No effect 0-1 | No effect 10-20 | |
| E2 | 300 | No effect 0-1 | No effect 10-20 | |
| E3 | No effect 300-350 | No effect 0-1 | No effect 10-20 | |
| EE2 | No effect 300-350 | No effect 0-1 | No effect 10-20 | |

3.4 Improvement of Optimization Conditions for LC Elution: Composition of Mobile Phase, Standard Solution and Flow Rate

Optimizations of these parameters were already done in the beginning of the study. However, the operation conditions of the instrument were selected arbitrarily. Since, significant and insignificant parameters were selected and the conditions to obtain the highest integration area were determined in section 3.3, the optimization was repeated in this stage of thesis. The aim of this section was to optimize flow rate through the column, composition of mobile phase and standard solution for the best peak symmetry and resolution factor in LC-MS/MS with regard to the best instrumental conditions.

Box-Behnken experimental design method was used. The Box-Behnken design is an independent quadratic design in that it does not contain an embedded factorial or fractional factorial design. The treatment combinations are at the midpoints of edges of the process space and at the center. These designs are rotatable (or near rotatable) and require 3 levels of each factor. The designs have limited capability for orthogonal blocking compared to the central composite designs. The three independent variables in this study were % ACN in standard solution (1000 ng/L) (X₁), % ACN concentration in mobile phase (X₂), and flow rate (X₃). The ranges for the factors were determined based on the results of first optimization study. % ACN in standard solution (ACN_s) X_1 = 22%-28%, % ACN in mobile phase (ACN_m) X_2 = 44%-50% and flow rate X_3 = 100 – 200 µL/min. The dependent variables were peak symmetry (PS) and resolution factor (RF). Table 3.40 summarizes the coded and actual experimental points of Box-Behnken experimental design. Center point was repeated 5 times.

The experiments were conducted at isocratic conditions, no gradient was applied. The parent and product masses, LC-MS/MS running conditions and selected reaction mode (SRM) conditions were given in Table 3.41. The interface conditions given in Table 3.42 represent the conditions at which the highest integration areas of the hormones were obtained in section 3.3.

| Run | Coded | | | Actual | | | | |
|--------|-----------|----|----|------------------------|-----------------------|--------|--|--|
| Number | Variables | | | Variables | | | | |
| STD | X1 | X2 | X3 | Standard Solution %ACN | Flow Rate $\mu L/min$ | | | |
| 1 | +1 | -1 | 0 | 28.00 | 44.00 | 150.00 | | |
| 2 | 0 | -1 | -1 | 25.00 | 44.00 | 100.00 | | |
| 3 | -1 | -1 | 0 | 22.00 | 44.00 | 150.00 | | |
| 4 | 0 | -1 | +1 | 25.00 | 44.00 | 200.00 | | |
| 5 | +1 | 0 | +1 | 28.00 | 47.00 | 200.00 | | |
| 6 | -1 | 0 | +1 | 22.00 | 47.00 | 200.00 | | |
| 7 | -1 | 0 | -1 | 22.00 | 47.00 | 100.00 | | |
| 8 | +1 | 0 | -1 | 28.00 | 47.00 | 100.00 | | |
| 9 | 0 | +1 | 0 | 22.00 | 50.00 | 150.00 | | |
| 10 | 0 | +1 | +1 | 25.00 | 50.00 | 200.00 | | |
| 11 | +1 | +1 | 0 | 28.00 | 50.00 | 150.00 | | |
| 12 | 0 | +1 | -1 | 25.00 | 50.00 | 100.00 | | |

Table 3.40 The coded and experimental points of Box-Behnken design.

| C-1 | 0 | 0 | 0 | 25.00 | 47.00 | 150.00 |
|------|---|---|---|-------|-------|--------|
| C -2 | 0 | 0 | 0 | 25.00 | 47.00 | 150.00 |
| C -3 | 0 | 0 | 0 | 25.00 | 47.00 | 150.00 |
| C -4 | 0 | 0 | 0 | 25.00 | 47.00 | 150.00 |
| C -5 | 0 | 0 | 0 | 25.00 | 47.00 | 150.00 |

Table 3.40 The coded and experimental points of Box-Behnken design (continued).

Table 3.41 The SRM conditions in LC-MS/MS for measurement of hormones.

| | Parent | Product | SRM | Retention | Time | Tube | Polarity | Trigger | Name |
|---|--------|---------|-----------|-----------|--------|------|----------|---------|------|
| | Mass | Mass | Collision | Time | Window | Lens | | | |
| | | | Energy | | | | | | |
| 1 | 269.1 | 143.2 | 51 | 7.50 | 15.00 | 85 | - | 0 | E1 |
| 2 | 269.1 | 145.3 | 36 | 7.50 | 15.00 | 85 | - | 0 | E1 |
| 3 | 271.1 | 145.1 | 56 | 7.50 | 15.00 | 85 | - | 0 | E2 |
| 4 | 271.1 | 183.2 | 44 | 7.50 | 15.00 | 85 | - | 0 | E2 |
| 5 | 287.0 | 145.0 | 48 | 7.50 | 15.00 | 85 | - | 0 | E3 |
| 6 | 287.0 | 171.1 | 41 | 7.50 | 15.00 | 85 | - | 0 | E3 |
| 7 | 295.1 | 145.0 | 49 | 7.50 | 15.00 | 85 | - | 0 | EE2 |
| 8 | 295.1 | 159.1 | 44 | 7.50 | 15.00 | 85 | - | 0 | EE2 |

Table 3.42 Interface conditions in LC-MS/MS for optimization of composition of mobile phase, standard solution and flow rate.

| Capillary Temperature (°C) | 300 |
|--|-----------|
| Vaporizer Temperature (°C) | 375 |
| Sheath Gas Pressure (Arb) | 35 |
| Aux Gas Pressure (Arb) | 20 |
| Ion Sweep Gas Pressure (Arb) | 0 |
| Spray Voltage (V) (positive/negative polarity) | 3000/2750 |

The experiments were conducted randomly. Responses obtained at these experimental conditions were presented at Table 3.43. The peak symmetry obtained for E1 varied between PS= 1.58 and 2.71 after improvement of instrument running conditions. However this range was considerably wider as PS= 0.5 to 3.8 obtained before this improvement. This improvement is also valid for PS values of all hormones. For example, PS value for E3 reached to 4.652 which indicate that peak is

not symmetric. But improvement in operating conditions and addition of NH_4OH decreased maximum PS of E3 to around PS=2.0 which is acceptable.

Similarly, a substantial improvement in resolution factor was observed. The desired condition for RF is to get high value which indicate that there is a good separation of substances and hence a good chromatogram. The highest RF for E3 was RF= 2.8 before instrument operating condition was improved. That improvement provided a RF value of E3= 4.5 which means an acceptable separation between E2 and E3. Similar increases in the RF values of peak pairs of other hormones were observed. These results indicated that determination of best instrumental conditions and addition of NH_4OH into mobile phase provided significantly better chromatograms.

| Run Number | Standard Solution %ACN | Mobile Phase % ACN | Flow Rate μL/min | RF-E3 | RF-E2 | RF-EE2 | PS-E1 | PS-E2 | PS-E3 | PS-EE2 |
|---------------|---------------------------|-----------------------|---------------------|-------|-------|--------|-------|-------|-------|--------|
| 1 | 22 | 44 | 150 | 3.95 | 1.09 | 0.39 | 2.24 | 2.00 | 2.10 | 2.00 |
| 2 | 28 | 44 | 150 | 3.73 | 1.29 | 0.59 | 1.91 | 1.41 | 1.79 | 2.00 |
| 3 | 22 | 50 | 150 | 2.70 | 0.62 | 0.48 | 2.41 | 3.00 | 1.62 | 1.61 |
| 4 | 28 | 50 | 150 | 2.05 | 0.57 | 0.54 | 1.78 | 2.38 | 2.25 | 1.75 |
| 5 | 22 | 47 | 100 | 4.05 | 1.08 | 0.59 | 1.82 | 1.65 | 1.64 | 1.36 |
| 6 | 28 | 47 | 100 | 3.07 | 0.93 | 0.45 | 2.32 | 1.69 | 2.46 | 1.42 |
| 7 | 22 | 47 | 200 | 2.50 | 0.74 | 0.51 | 2.71 | 1.75 | 2.00 | 2.33 |
| 8 | 28 | 47 | 200 | 3.10 | 0.78 | 0.39 | 2.22 | 1.92 | 1.60 | 2.06 |
| 9 | 25 | 44 | 100 | 4.50 | 1.25 | 0.75 | 1.86 | 1.86 | 2.00 | 2.50 |
| 10 | 25 | 50 | 100 | 3.05 | 0.79 | 0.65 | 1.58 | 1.19 | 1.44 | 2.00 |
| 11 | 25 | 44 | 200 | 2.90 | 0.91 | 0.49 | 2.14 | 2.62 | 2.36 | 2.67 |
| 12 | 25 | 50 | 200 | 2.11 | 0.47 | 0.53 | 1.79 | 2.70 | 1.06 | 2.00 |
| C1 | 25 | 47 | 150 | 3.93 | 0.88 | 0.46 | 1.64 | 1.85 | 1.74 | 1.80 |
| C2 | 25 | 47 | 150 | 3.70 | 1.03 | 0.57 | 2.59 | 1.71 | 1.82 | 1.93 |
| C3 | 25 | 47 | 150 | 3.21 | 0.72 | 0.54 | 1.92 | 1.94 | 1.86 | 1.32 |
| C4 | 25 | 47 | 150 | 3.47 | 1.08 | 0.52 | 1.92 | 1.94 | 1.57 | 1.69 |
| C5 | 25 | 47 | 150 | 3.33 | 0.89 | 0.63 | 2.21 | 1.59 | 1.73 | 1.68 |

Table 3.43 Observed peak symmetry and resolution factors of Box-Behnken experimental design.

3.4.1 Optimization of Peak Symmetry

ANOVA analysis for the significance of coefficients of response equation for peak symmetry (Table 3.44 – Table 3.45, respectively) was conducted. Values of "Prob > F" less than 0.0500 indicate model terms are significant. Values greater than 0.1000 indicate the model terms are not significant. Significance of quadratic coefficients indicates that response equation model is quadratic (as given in equation 3.7). Insignificant quadratic coefficients state that linear response equation can be used for diagnosis of model. The lack of fit test is desired to be insignificant which indicates reproducibility of the results. Reponses equation coefficients for different hormones were given in Table 3.45 $R^2 > 0.90$ depicts a good agreement between predicted values by using response equation coefficients and observed value. R^2 value was higher than 0.90 for E2, E3and EE2. Adeq Precision" measures the signal to noise ratio. A ratio greater than 4 is desirable and states that model equation can be used to predict the reponse for any value of factors within tha range of experimental design. Although R^2 value for E1 vas less than 0.90, Adeq Precison is larger than 4. Therefore, model coefficient can be used to predict response for E1. The coefficients were used to predicted the reposes for the experimental points. As seen from the tables, the difference between observed and predicted values is very low or at acceptable level (Table 3.46). This result proves that model coefficients are reliable to predict response at any experimental point within the studied ranges of factors.

$$Y = b_0 + b_1 X_1 + b_2 X_2 + b_3 X_3 + b_{12} X_1 X_2 + b_{13} X_1 X_3 + b_{23} X_2 X_3 + b_{123} X_1 X_2 X_3 + b_{11} X_1^2 + b_{22} X_2^2 + b_{33} X_3^2$$
(3.7)

| Source | of variation | E1 | E2 | E3 | EE2 | |
|----------------|-----------------------|----------|----------|----------|----------|--|
| Coded | Actual | p-value | p-value | p-value | p-value | |
| | Actual | Prob > F | Prob > F | Prob > F | Prob > F | |
| М | Model | 0.6747 | 0.0614 | 0.0030 | 0.0629 | |
| X ₁ | % ACN in standard | 0.3890 | 0.2411 | 0.0480 | 0.9115 | |
| X ₂ | % ACN in mobile phase | 0.4098 | 0.3137 | 0.0003 | 0.0395 | |

Table 3.44 ANOVA analysis of peak symmetry of hormones for improved instrumental running conditions.

| X ₃ | Flow rate | 0.5246 | 0.0077 | 0.9440 | 0.7089 |
|--------------------------------|--|--------|--------|--------|--------|
| X ₁ X ₂ | Interatction between mobile phase and stationary phase | 0.6893 | 0.9608 | 0.0058 | 0.7552 |
| X ₁ X ₃ | % ACN in mobile phase vs flow rate | 0.2265 | 0.8134 | 0.0019 | 0.4654 |
| X ₂ X ₃ | % ACN in stationary phase vs flow rate | 0.9244 | 0.2090 | 0.0148 | 0.7089 |
| X ₁ ² | Quadratic effect of mobile phase | 0.2477 | 0.8396 | 0.0092 | 0.1557 |
| X_{2}^{2} | Quadratic effect of stationary phase | 0.3067 | 0.0356 | 0.8908 | 0.0245 |
| X_{3}^{2} | Quadratic effect of flowrate | 0.9363 | 0.5624 | 0.7155 | 0.0416 |
| $X_1^2 X_2$ | | 0.5292 | 0.0183 | 0.0014 | 0.4166 |
| X ₁ 2X ₃ | | 0.7776 | 0.0484 | 0.1499 | 0.0589 |
| Lack of | Fit | 0.3928 | 0.0305 | 0.7970 | 0.6179 |

Table 3.44 ANOVA analysis of peak symmetry of hormones for improved instrumental running conditions (continued).

Table 3.45 Regression coefficients of peak symmetry for estrogenic hormones.

| Coefficient of | Coefficients | Coefficients | Coefficients | Coefficients |
|--------------------------------|--------------|--------------|--------------|--------------|
| response equation | for E1 | for E2 | for E3 | for EE2 |
| b ₀ | -246.26 | -492.878 | -441.752 | -141.667 |
| b ₁ | 15.46322 | 47.50023 | 36.10214 | 18.38937 |
| b ₂ | 6.201013 | 10.7824 | 10.13496 | -0.5126 |
| b ₃ | 0.155584 | -0.71428 | -0.05877 | 0.498594 |
| b ₁₂ | -0.32482 | -1.18659 | -0.82847 | -0.24048 |
| b ₁₃ | -0.01002 | 0.053843 | 0.011562 | -0.04091 |
| b ₂₃ | -0.00012 | 0.001263 | -0.00124 | -0.00028 |
| b ₁₁ | -0.29722 | -0.95077 | -0.73982 | -0.36981 |
| b ₂₂ | -0.02204 | 0.040647 | -0.0008 | 0.036328 |
| b ₃₃ | -5.9E-06 | -3.2E-05 | -7.7E-06 | 0.000112 |
| b ₁₁ b ₂ | 0.006328 | 0.023717 | 0.017091 | 0.004887 |
| b ₁₁ b ₃ | 0.000168 | -0.00107 | -0.00027 | 0.000807 |
| R ² | 0.625287 | 0.903189 | 0.973602 | 0.902112 |
| Adequate precision | 4.176596 | 7.391553 | 16.27569 | 7.638518 |

| Run | X1 | X2 | X3 | E1 | | E2 | | E3 | | EE2 | |
|-----|----|----|-----|--------|-----------|--------|-----------|--------|-----------|--------|-----------|
| No: | | | | Actual | Predicted | Actual | Predicted | Actual | Predicted | Actual | Predicted |
| 1 | 22 | 44 | 150 | 2.24 | 2.12 | 2.00 | 1.82 | 2.10 | 2.08 | 2.00 | 2.04 |
| 2 | 28 | 44 | 150 | 1.91 | 2.03 | 1.41 | 1.59 | 1.79 | 1.80 | 2.00 | 1.96 |
| 3 | 22 | 50 | 150 | 2.41 | 2.29 | 3.00 | 2.82 | 1.62 | 1.60 | 1.61 | 1.65 |
| 4 | 28 | 50 | 150 | 1.78 | 1.90 | 2.38 | 2.56 | 2.25 | 2.26 | 1.75 | 1.71 |
| 5 | 22 | 47 | 100 | 1.82 | 1.94 | 1.65 | 1.83 | 1.64 | 1.65 | 1.36 | 1.31 |
| 6 | 28 | 47 | 100 | 2.32 | 2.20 | 1.69 | 1.51 | 2.46 | 2.45 | 1.42 | 1.46 |
| 7 | 22 | 47 | 200 | 2.71 | 2.83 | 1.75 | 1.93 | 2.00 | 2.01 | 2.33 | 2.29 |
| 8 | 28 | 47 | 200 | 2.22 | 2.10 | 1.92 | 1.75 | 1.60 | 1.59 | 2.06 | 2.11 |
| 9 | 25 | 44 | 100 | 1.86 | 1.86 | 1.86 | 1.86 | 2.00 | 2.00 | 2.50 | 2.50 |
| 10 | 25 | 50 | 100 | 1.58 | 1.58 | 1.19 | 1.19 | 1.44 | 1.44 | 2.00 | 2.00 |
| 11 | 25 | 44 | 200 | 2.14 | 2.14 | 2.62 | 2.62 | 2.36 | 2.36 | 2.67 | 2.67 |
| 12 | 25 | 50 | 200 | 1.79 | 1.79 | 2.70 | 2.70 | 1.06 | 1.06 | 2.00 | 2.00 |
| C1 | 25 | 47 | 150 | 1.64 | 2.06 | 1.85 | 1.81 | 1.74 | 1.74 | 1.80 | 1.68 |
| C2 | 25 | 47 | 150 | 2.59 | 2.06 | 1.71 | 1.81 | 1.82 | 1.74 | 1.93 | 1.68 |
| C3 | 25 | 47 | 150 | 1.92 | 2.06 | 1.94 | 1.81 | 1.86 | 1.74 | 1.32 | 1.68 |
| C4 | 25 | 47 | 150 | 1.92 | 2.06 | 1.94 | 1.81 | 1.57 | 1.74 | 1.69 | 1.68 |
| C5 | 25 | 47 | 150 | 2.21 | 2.06 | 1.59 | 1.81 | 1.73 | 1.74 | 1.68 | 1.68 |

Table 3.46 Actual and predicted values of peak symmetries of hormones.

Table 3.47 Optimum predicted conditions for the best peak symmetry.

| %ACNs | %ACN _m | Flow rate | PS E1 | PS E2 | PS E3 | PS EE2 | Desirability |
|-------|-------------------|-----------|-------|-------|-------|--------|--------------|
| 25 | 50 | 105 | 1,60 | 1,27 | 1,46 | 1,95 | 1 |
| 25 | 50 | 100 | 1,60 | 1,18 | 1,46 | 1,99 | 1 |
| 24 | 50 | 100 | 1,59 | 1,26 | 1,35 | 1,95 | 1 |
| 24 | 50 | 100 | 1,60 | 1,36 | 1,32 | 1,92 | 1 |
| 25 | 50 | 103 | 1,59 | 1,24 | 1,42 | 1,96 | 1 |
| 25 | 50 | 105 | 1,60 | 1,27 | 1,46 | 1,95 | 1 |

Two level interactions of the factors for different hormones at constant ACN_s concentration of 25%, which was determine according to results of optimization, were evaluated (Table 3.47). Figure 3.39 depicts the variation of PS value of E1 at different %ACN_m and flow rates. Increasing flow rate adversely affects the peak symmetry. It was PS= 1.57 at 100 μ L/min flow rate and increased to PS= 2.10 when flow rate was F= 200 μ L/min at ACN_m = 44%. The PS value was higher for % ACN_m=44% - 47% at any flow rate, but showed a substantial decrease at

ACN_m>47%. The minimum PS value was obtained as PS= 1.5 at ACN_m= 50 % and flow rate = $100 \mu L/min$.

Variation of PS of E2 at different flow rate and %ACN_m concentration is shown in Figure 3.40. The lowest PS value around PS= 1.0 was observed at ACN_m>48% and flow rate= 100 μ L/min. The effect of flow rate was adverse on the PS and more significant than that of ACN_m on PS for E2. Increasing flow rate from 100 μ L/min to 200 μ L/min at 50% ACN_m resulted in increasing PS value from PS= 1.1 to PS= 2.3. However, increasing ACN_m concentration provided better PS values. It was PS= 1.4 at 44% ACN_m but decreased to around PS= 1.0 at 50% ACN_m (flow rate = 100 μ L/min).

The most significant factor in the case of PS value of E3 was ACN_m concentration. As seen from Figure 3.41 increasing ACN_m from 44% to 50% resulted in a substantial improvement peak symmetry with decreasing in the value from PS= 2.3 to PS=1.1 at flow rate= 100 µL/min. The effect of flow rate on PS was not as strong as ACN_m . Decrease in PS from PS= 1.4 to PS= 1.2 when flow rate was increased from 100 µL/min to 200 µL/min at ACN_m = 50%. The best peak symmetry around PS= 1 for E3 can be obtained at flow rate= 200µL/min and ACN_m = 50%.

Finally, variation of PS for EE2 with ACN_m and flow rate at ACN_s= 25 % is depicted in Figure 3.42 the main factor that affects the PS value of EE2 is ACN_m rather than flow rate. PS value most significantly increases from PS= 1.9 to PS= 2.5 when ACN_m was decreased from 50% to 44% at minimum flow rate of 100 μ L/min. However, PS value varies between 1.8 and 1.9 for flow rate between 100 μ L/min and 200 μ L/min at ACN_m= 50%. This slight variation in PS value for different values of flow rate can be observed even at lowest concentration of ACN_m= 44%. It was 2.7 at 200 μ L/min and decreased to only 2.4 at 100 μ L/min flow rate. In summary the best acceptable peak symmetry for EE2 can be obtained at flow rate= 100 μ L/min, ACN_m= 50%.

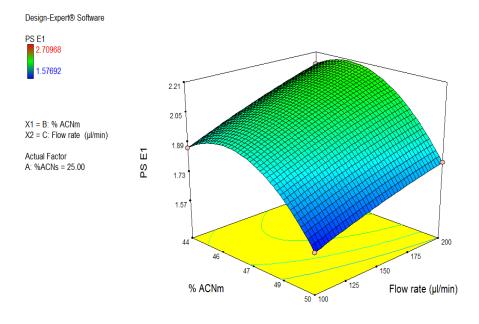


Figure 3.39 Variation of peak symmetry of E1 with % ACN $_{\rm m}$ and flow rate at ACN $_{\rm s}$ = 25%.

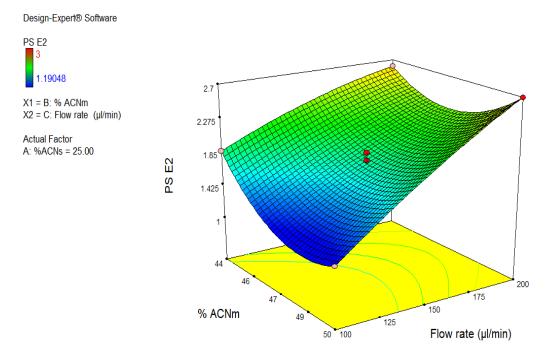


Figure 3.40 Variation of peak symmetry of E2 with % ACN $_{\rm m}$ and flow rate at ACN $_{\rm s}{=}~25\%.$

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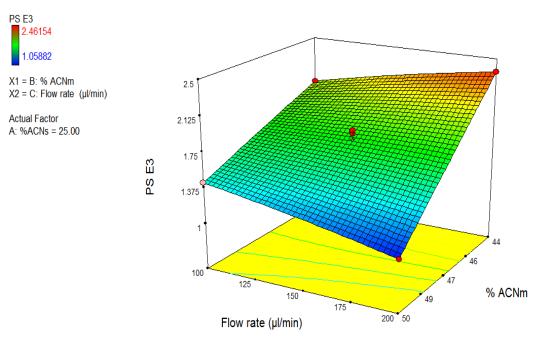


Figure 3.41 Variation of peak symmetry of E3 with % ACN_m and flow rate at $ACN_s = 25\%$.

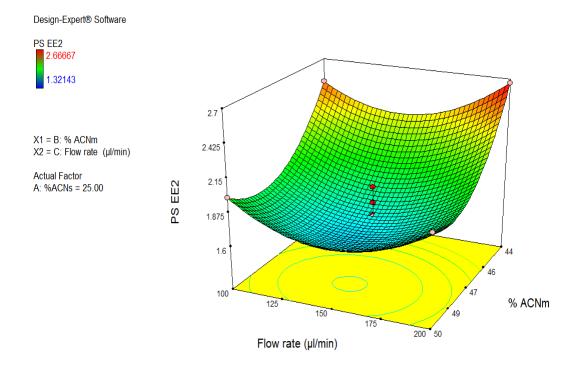


Figure 3.42 Variation of peak symmetry of EE2 with % ACN_m and flow rate at $ACN_s = 25\%$.

3.4.2 Optimization of Resolution Factor

Variance analysis of Box-Behnken design for resolution factor response is given in Table 3.48 similar to peak symmetry, variance analysis for the significance of coefficients of resolution factor response equation (Table 3.49) was carried out. Response equation for E2 and EE2 were quadratic but it was linear for E3. Therefore no significance of the quadratic terms of this hormone was conducted. ANOVA results indicated that the most significant linear effect corresponds to the flow rate for all hormones. The lack of fit for all hormones was insignificant which indicates reproducibility of the results. Response equation coefficients for different hormones were given in Table 3.49. Regression coefficients between observed and predicted values were higher than 0.85 for E3 and E2 but it was 0.57 for EE2. However, Adeq Precision for this hormone was greater than 4 which means that model equation can be used to predict the reponse for any value of factors within tha range of experimental design. Moreover, the difference between observed and predicted values were very low or at acceptable level too (Table 3.50). This result prooves that model coefficients are reliable to predict response at any experimental point within the studied ranges of factors.

Optimization of condition by using response equation of resolution factor was done. The high resolution factor indicates that there is a good separation of peaks relative to each other. Therefore, the main aim in the optimization of RF was to select the conditions to obtain the highest RF values for each hormone. In other words, the target in the optimization was to maximization of RF value. Table 3.51 depicts the optimum conditions with 95% guarantee target aim. As seen from table, $%ACN_s= 25$, $%ACN_m= 44$ and flow rate= 100 µL/min are the optimal conditions to get the best RF values.

| Source | of variation | E2 | E3 | EE2 |
|-------------------------------|--|-----------------------------------|---------------------|---------------------|
| Coded | Actual | p-value Prob > F | p-value Prob > F | p-value Prob > F |
| М | Model | 0.0006 | 0.0035 | 0.4857 |
| \mathbf{X}_1 | % ACN in standard | 0.9010 | 0.1632 | 0.9853 |
| X ₂ | % ACN in mobile phase | < 0.0001 | 0.0003 | 0.9493 |
| X ₃ | Flow rate | 0.0031 | 0.0014 | 0.0812 |
| X ₁ X ₂ | Interatction between mobile phase and Stationary phase | 0.2733 | 0.4713 | 0.4978 |
| X ₁ X ₃ | %ACN in mobile phase vs flowrate | 0.3835 | 0.0265 | 0.8815 |
| X ₂ X ₃ | %ACN in stationary phase vs flowrate | 0.9221 | 0.2779 | 0.4793 |
| X ₁ ² | Quadratic effect of mobile phase | Not included to response equation | 0.2105 | 0.1073 |
| X2 ² | Quadratic effect of stationary phase | Not included to response equation | 0.1358 | 0.4182 |
| X ₃ ² | Quadratic effect of flowrate | Not included to response equation | 0.2877 | 0.6229 |
| Lack of | Fit | 0.9308 | 0.5253 | 0.1296 |

Table 3.48 ANOVA analysis of resolution factor of hormones for improved instrumental running conditions.

Values of "Prob > F" less than 0.0500 indicate model terms are significant. Values greater than 0.1000 indicate the model terms are not significant.

| Coefficient | Coefficients | Coefficients for | Coefficients | |
|-----------------------|--------------|------------------|--------------|--|
| of response | for E2 | E3 | for EE2 | |
| equation | | | | |
| b ₀ | -1.07978 | -51.3902 | 2.170366 | |
| b ₁ | 0.26869 | 1.167873 | 0.616001 | |
| b ₂ | 0.075353 | 2.339036 | -0.34164 | |
| b ₃ | -0.01237 | -0.10904 | -0.01582 | |
| b ₁₂ | -0.00669 | -0.01194 | -0.0036 | |
| b ₁₃ | 0.000316 | 0.002635 | 4.67E-05 | |
| b ₂₃ | 3.47E-05 | 0.001107 | 0.000226 | |

Table 3.49 Regression coefficients of resolution factor response equation for estrogenic hormones.

Table 3.49 Regression coefficients of resolution factor response equation for estrogenic hormones (continued).

| b ₁₁ | | -0.02107 | -0.00907 |
|-----------------|--------|----------|----------|
| b ₂₂ | | -0.02577 | 0.004225 |
| b ₃₃ | | -6.3E-05 | 9.09E-06 |
| \mathbb{R}^2 | 0.8708 | 0.9253 | 0.5744 |
| Adequate | 12.079 | 10.648 | 4.224 |
| precision | | | |

| Run | | | | E3 | | E2 | | EE2 | |
|--------|----|----|-----|--------|-----------|--------|-----------|--------|-----------|
| Number | X1 | X2 | X3 | Actual | Predicted | Actual | Predicted | Actual | Predicted |
| 1 | 22 | 44 | 150 | 3.95 | 3.80 | 1.09 | 1.08 | 0.39 | 0.47 |
| 2 | 28 | 44 | 150 | 3.73 | 3.70 | 1.29 | 1.21 | 0.59 | 0.53 |
| 3 | 22 | 50 | 150 | 2.70 | 2.72 | 0.62 | 0.69 | 0.48 | 0.53 |
| 4 | 28 | 50 | 150 | 2.05 | 2.20 | 0.57 | 0.57 | 0.54 | 0.47 |
| 5 | 22 | 47 | 100 | 4.05 | 4.24 | 1.08 | 1.07 | 0.59 | 0.56 |
| 6 | 28 | 47 | 100 | 3.07 | 3.14 | 0.93 | 0.99 | 0.45 | 0.54 |
| 7 | 22 | 47 | 200 | 2.50 | 2.43 | 0.74 | 0.70 | 0.51 | 0.41 |
| 8 | 28 | 47 | 200 | 3.10 | 2.91 | 0.78 | 0.80 | 0.39 | 0.43 |
| 9 | 25 | 44 | 100 | 4.50 | 4.46 | 1.25 | 1.30 | 0.75 | 0.71 |
| 10 | 25 | 50 | 100 | 3.05 | 2.83 | 0.79 | 0.77 | 0.65 | 0.63 |
| 11 | 25 | 44 | 200 | 2.90 | 3.11 | 0.91 | 1.00 | 0.49 | 0.51 |
| 12 | 25 | 50 | 200 | 2.11 | 2.15 | 0.47 | 0.49 | 0.53 | 0.57 |
| C1 | 25 | 47 | 150 | 3.93 | 3.53 | 0.88 | 0.89 | 0.46 | 0.54 |
| C2 | 25 | 47 | 150 | 3.70 | 3.53 | 1.03 | 0.89 | 0.57 | 0.54 |
| C3 | 25 | 47 | 150 | 3.21 | 3.53 | 0.72 | 0.89 | 0.54 | 0.54 |
| C4 | 25 | 47 | 150 | 3.47 | 3.53 | 1.08 | 0.89 | 0.52 | 0.54 |
| C5 | 25 | 47 | 150 | 3.33 | 3.53 | 0.89 | 0.89 | 0.63 | 0.54 |

Table 3.50 Actual and predicted values of resolution factor for hormones.

Table 3.51 Optimum predicted conditions to obtain the maximum resolution factor values.

| X1 | X2 | X3 | E3 | E2 | EE2 | Desirability |
|-------|----|--------|------|------|------|--------------|
| 24.69 | 44 | 100 | 4.50 | 1.30 | 0.70 | 0.95 |
| 24.74 | 44 | 100 | 4.49 | 1.30 | 0.70 | 0.95 |
| 24.98 | 44 | 100 | 4.46 | 1.30 | 0.71 | 0.95 |
| 24.63 | 44 | 101.02 | 4.50 | 1.29 | 0.70 | 0.95 |

Variation of RF values with two level interactions of factors was evaluated. % ACN_s was kept constant at 25% which is the optimal concentration obtained after

optimization. Figure 3.43 depicts effect of % ACN_m and flow rate on RF value of E3. Both factors significantly affect the RF value. For example, decreasing flow rate from 200 μ L/min to 100 μ L/min at 50 % ACN_m resulted in increasing in RF value from RF=2.1 to RF= 2.8. Similarly, there was an increase from 2.1 to around 3.2 for ACN_m concentration 50% to 44%, respectively. However, the interaction effects of these factors are more significant than the main factor effects. Since, decreasing both factors provide a substantial increase in the RF value. The maximum resolution factor value with regard to E3 can be obtained as RF=4.5 at the low levels of factor as ACN_m= 44% and flow rate= 100 μ L/min.

The relationship between factors for E2 was linear and curvation was insignificant (Table 3.48). Similar to RF value of E3, the combined effect of factors are more significant than the main effects of factors (Figure 3.44). As a results, maximum RF value can be obtained as RF= 1.3 at ACN_m= 44% and flow rate= 100 μ L/min. In the case of EE2, the main increase in the response can be obtained with the decrease in flow rate from 200 μ L/min to 100 μ L/min (Figure 3.45). The interaction effects of these two factors provide a substantial improvement in the response as well.

Although statistically proved that the model equations can be used to predict the responses at any values of factor within the studied range, the best approach is to run an experiment at the point which is different than design points. In other words, model verification was conducted to be sure about the model. Table 3.52 depicts the observed and predicted values of two different values of investigated factors. The results indicated that there is no substantial difference between observed and predicted values. The chromatograms of these two conditions were given in Figure 3.46 and Figure 3.47.

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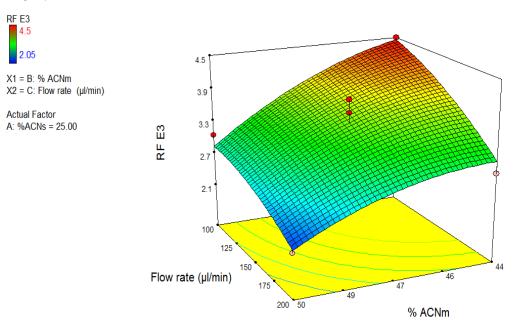


Figure 3.43 Variation of RF value of E3 with % ACN_m and flow rate at $ACN_s\!=\!25\%.$

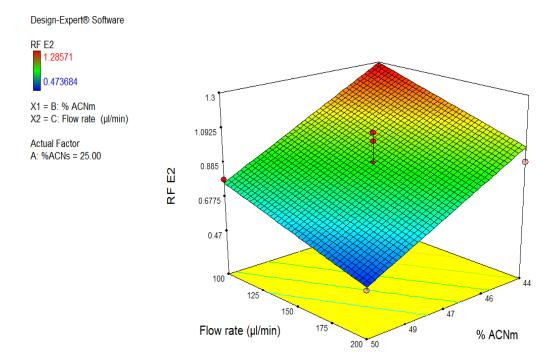


Figure 3.44 Variation of RF value of E2 with % ACN $_{\rm m}$ and flow rate at ACN $_{\rm s}$ = 22%.

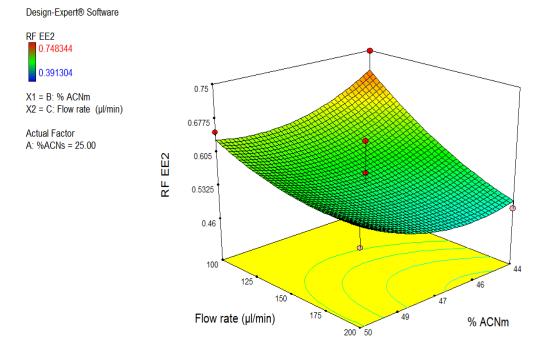


Figure 3.45 Variation of RF value of EE2 with % ACN_m and flow rate at $ACN_s = 25\%$.

| | %ACN _s | %AC | %ACN _m | | %ACN _s | %ACN _m | | Flow | |
|----------|-------------------|-----------------|-------------------|------|-------------------|-------------------|-------|-----------|--|
| Response | 25 | 25 48 | | 145 | 25 44 | | | 175 | |
| | Observed | Observed | | cted | Observed | Observed | | Predicted | |
| RF E3 | 3.16 | | 3.33 | | 3.05 | | 3.57 | | |
| RF E2 | 0.717 | 0.717 | | | 1.00 | | 1.08 | | |
| RF EE2 | 0.521 | | 0.552 | | 0.588 | | 0.540 | | |
| PS E1 | 1.94 | | 1.97 | | 2.06 | | 2.084 | | |
| PS E2 | 1.85 | | 1.73 | | 1.93 | | 2.49 | | |
| PS E3 | 1.62 | 1.62 | | | 2.67 | | 2.29 | | |
| PS EE2 | 1.45 | 1.45 | | | 2.36 | | 2.41 | | |

Table 3.52 Observed and predicted values of RF and PS at the experimental points which are different than design points.

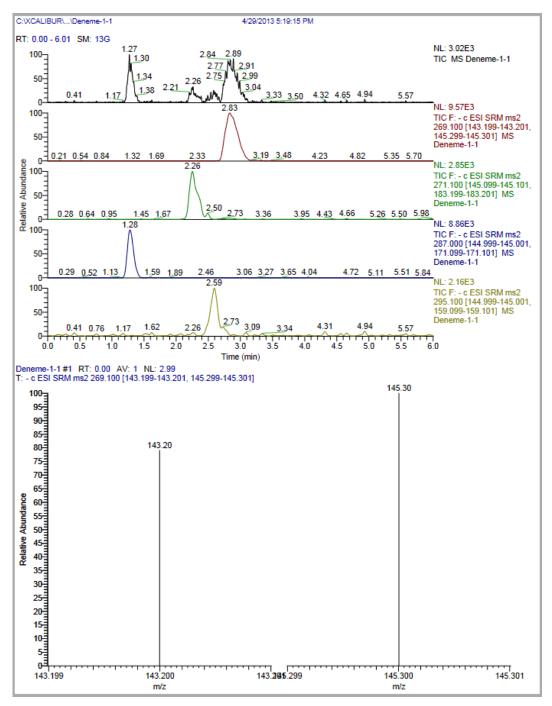


Figure 3.46 Chromatograms of hormones at ACN_s= 25%, ACN_m= 48% and flow rate = 145 μ L/min.

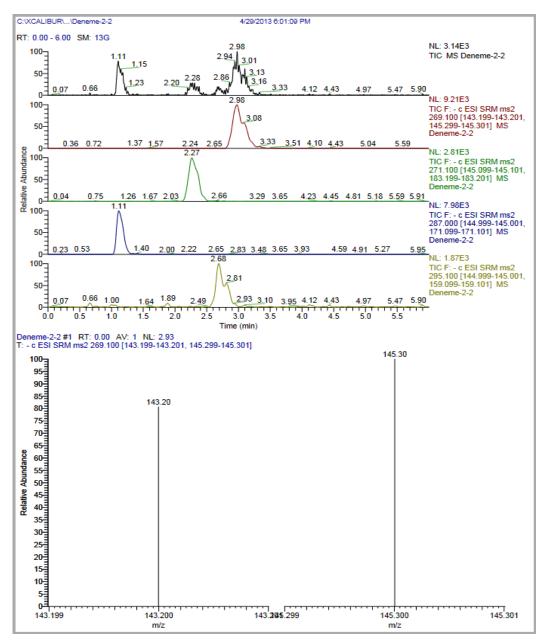


Figure 3.47Chromatograms of hormones at ACN_s= 25%, ACN_m= 44% and flow rate = 175 μ L/min.

The optimization of conditions was carried out for two different responses so far in order to observe that if there are considerable differences for the optimized conditions. Fortunately, these two conditions were not substantially different. Since, LC-MS/MS cannot be operated at different conditions to obtain the best RF and PS values. Therefore, the optimization process were run again to get the maximum RF value and target PS value between PS=1 and PS=2. The results were given in Table 3.53 indicated the conditions were very close to the values obtained from individual optimization of responses. However, EE2 is the most difficult hormone to measure. In addition there is no need to have RF=4 for E3. Therefore, the conditions needed further improvement in terms of peak symmetry of EE2 and RF of E3. The second optimization (Table 3.54) resulted in a slight variations from the Table 3.53 for the responses but acceptable.

Table 3.53 Predicted optimum conditions for peak symmetry and resolution factor.

| Number | %ACNs | %ACN _m | Flow rate | RF E3 | RF E2 | RF EE2 | PS E1 | PS E2 | PS E3 | PS EE2 | Desirability |
|--------|-------|-------------------|-----------|-------|-------|--------|-------|-------|-------|--------|--------------|
| 1 | 22.49 | 44 | 100 | 4.69 | 1.28 | 0.63 | 1.68 | 1.90 | 1.77 | 2.00 | 0.869 |
| 2 | 22.51 | 44.03 | 100 | 4.69 | 1.28 | 0.63 | 1.69 | 1.89 | 1.77 | 2.00 | 0.869 |
| 3 | 22.57 | 44.14 | 100 | 4.68 | 1.27 | 0.63 | 1.71 | 1.87 | 1.77 | 1.99 | 0.866 |
| 4 | 22.5 | 44 | 101.09 | 4.68 | 1.28 | 0.62 | 1.69 | 1.90 | 1.78 | 2.00 | 0.864 |
| 5 | 22.45 | 44.04 | 100 | 4.69 | 1.28 | 0.62 | 1.68 | 1.89 | 1.76 | 1.97 | 0.864 |

Table 3.54 Predicted optimum conditions and determined conditions.

| | | | | | | RF | | | | PS |
|--------------------------|-------|-------------------|-----------|-------|-------|------|-------|-------|-------|------|
| | %ACNs | %ACN _m | Flow rate | RF E3 | RF E2 | EE2 | PS E1 | PS E2 | PS E3 | EE2 |
| Determined Conditions | 28 | 44 | 136.9 | 3.76 | 1.25 | 0.56 | 2.04 | 1.60 | 1.86 | 1.88 |

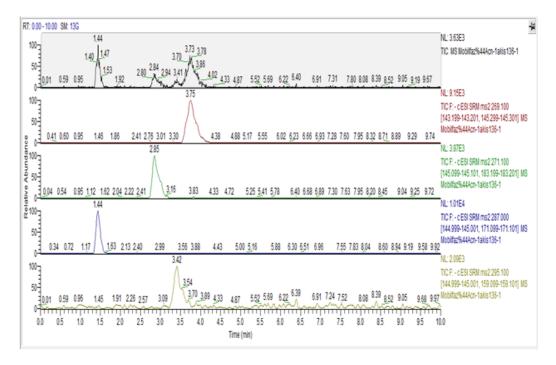


Figure 3.48 Chromatograms of hormones at ACN_s= 28%, ACN_m= 44% and flow rate = 136.9 μ L/min.

3.5 Improvement of Optimized Conditions for LC-MS/MS Operation

Box-Behnken Experimental Design method was used for optimization of instrument operating conditions for the new elution conditions as determined in section 3.4. The factors were sheath gas pressure (SGP), ion sweep gas pressure (ISGP), aux gas pressure (AGP), spray voltage (SV), capillary temperature (CT), vaporizer temperature (VT) and collision gas pressure (CGP). Cone position was kept at D. The ranges of these factors were determined according to the results obtained at section 3.3 and given in Table 3.55. Table 3.56 indicates the experimental points (62). Center point repeated 6 times (run number 11, 15, 27, 40, 50, 61) times. The response was the integration area of the hormones. The observed responses for four hormones were given in Table 3.57. ANOVA analysis (Table 3.58) for the significance of coefficients (Table 3.59) of response equation for integration area of hormones was conducted. Values of "Prob > F" less than 0.0500 indicate model terms are significant. Values greater than 0.1000 indicate the model terms are not significant. The response equation included main effects, two level interactions and quadratic effects of the factors. The responses for the same experimental points were predicted by using model coefficients. The regression coefficient and Adeq Precision values were R>0.90 and AP>4, respectively, indicate that model can be used to predict the integration area of hormones for the studied ranges of factors. Finaly, optimization process was run for all hormones (1000 ng/L). The results were presented in Table 3.60. The target was to maximize the integration area. There was 14 different possible optimized conditions of the factors.

| | Low level (-1) | High Level (+1) | Center point (0) |
|-------------|----------------|-----------------|------------------|
| SGP (arb) | 32 | 38 | 35 |
| ISGP (arb) | 0 | 2 | 1 |
| AGP (arb) | 10 | 20 | 15 |
| CT (°C) | 250 | 350 | 300 |
| VT (°C) | 325 | 425 | 375 |
| CGP (mTorr) | 1.5 | 2.5 | 2 |
| SV (V) | 2500 | 3000 | 2750 |

Table 3.55 Determined high levels, low levels and center points of the factors.

| Run Number | SGP | ISGP | AGP | СТ | VT | CGP | SV |
|---------------|-----|------|-----|-----|------------|-----|------|
| 1 | 35 | 1 | 10 | 350 | 375 | 2 | 2500 |
| 2 | 32 | 2 | 15 | 350 | 375 | 2 | 2750 |
| 3 | 35 | 1 | 10 | 350 | 375 | 2 | 3000 |
| 4 | 35 | 1 | 15 | 250 | 325 | 1.5 | 2750 |
| 5 | 35 | 1 | 20 | 250 | 375 | 2 | 3000 |
| 6 | 35 | 0 | 20 | 300 | 375 | 2.5 | 2750 |
| 7 | 35 | 1 | 15 | 250 | 325 | 2.5 | 2750 |
| 8 | 35 | 0 | 10 | 300 | 375 | 2.5 | 2750 |
| 9 | 38 | 1 | 15 | 300 | 375 | 2.5 | 3000 |
| 10 | 32 | 1 | 15 | 300 | 375 | 2.5 | 3000 |
| | 35 | | 15 | 300 | | 2.3 | 2750 |
| 11 12 | 35 | 1 | 15 | 300 | 375 425 | 2 | 3000 |
| | | 0 | | | | | |
| 13 | 38 | 1 | 20 | 300 | 325 | 2 | 2750 |
| 14 | 35 | 1 | 20 | 350 | 375 | 2 | 3000 |
| 15 | 35 | 1 | 15 | 300 | 375 | 2 | 2750 |
| 16 | 35 | 0 | 20 | 300 | 375 | 1.5 | 2750 |
| 17 | 32 | 1 | 10 | 300 | 325 | 2 | 2750 |
| 18 | 32 | 0 | 15 | 250 | 375 | 2 | 2750 |
| 19 | 32 | 2 | 15 | 250 | 375 | 2 | 2750 |
| 20 | 35 | 1 | 15 | 250 | 425 | 2.5 | 2750 |
| 21 | 32 | 1 | 20 | 300 | 325 | 2 | 2750 |
| 22 | 38 | 2 | 15 | 250 | 375 | 2 | 2750 |
| 23 | 38 | 1 | 15 | 300 | 375 | 1.5 | 3000 |
| 24 | 35 | 0 | 10 | 300 | 375 | 1.5 | 2750 |
| 25 | 35 | 1 | 20 | 250 | 375 | 2 | 2500 |
| 26 | 35 | 1 | 10 | 250 | 375 | 2 | 3000 |
| 27 | 35 | 1 | 15 | 300 | 375 | 2 | 2750 |
| 28 | 35 | 1 | 15 | 250 | 425 | 1.5 | 2750 |
| 29 | 35 | 1 | 15 | 350 | 325 | 1.5 | 2750 |
| 30 | 32 | 1 | 15 | 300 | 375 | 2.5 | 2500 |
| 31 | 32 | 0 | 15 | 350 | 375 | 2 | 2750 |
| 32 | 38 | 1 | 10 | 300 | 425 | 2 | 2750 |
| 33 | 35 | 2 | 15 | 300 | 325 | 2 | 2500 |
| 34 | 32 | 1 | 20 | 300 | 425 | 2 | 2750 |
| 35 | 38 | 1 | 10 | 300 | 325 | 2 | 2750 |
| 36 | 35 | 1 | 15 | 350 | 425 | 1.5 | 2750 |
| 37 | 38 | 0 | 15 | 350 | 375 | 2 | 2750 |
| 38 | 38 | 1 | 15 | 300 | 375 | 1.5 | 2500 |

Table 3.56 Box Behnken Experimental Design for optimization of LC-MS/MS operating conditions.

| 39 | 35 | 2 | 10 | 300 | 375 | 1.5 | 2750 |
|----|----|---|----|-----|-----|-----|------|
| 40 | 35 | 1 | 15 | 300 | 375 | 2 | 2750 |
| 41 | 35 | 1 | 15 | 350 | 325 | 2.5 | 2750 |
| 42 | 35 | 1 | 20 | 350 | 375 | 2 | 2500 |
| 43 | 38 | 1 | 15 | 300 | 375 | 2.5 | 2500 |
| 44 | 35 | 2 | 15 | 300 | 425 | 2 | 3000 |
| 45 | 35 | 2 | 15 | 300 | 325 | 2 | 3000 |
| 46 | 38 | 1 | 20 | 300 | 425 | 2 | 2750 |
| 47 | 35 | 2 | 15 | 300 | 425 | 2 | 2500 |
| 48 | 35 | 2 | 20 | 300 | 375 | 2.5 | 2750 |
| 49 | 38 | 2 | 15 | 350 | 375 | 2 | 2750 |
| 50 | 35 | 1 | 15 | 300 | 375 | 2 | 2750 |
| 51 | 32 | 1 | 10 | 300 | 425 | 2 | 2750 |
| 52 | 32 | 1 | 15 | 300 | 375 | 1.5 | 3000 |
| 53 | 35 | 0 | 15 | 300 | 325 | 2 | 3000 |
| 54 | 32 | 1 | 15 | 300 | 375 | 1.5 | 2500 |
| 55 | 38 | 0 | 15 | 250 | 375 | 2 | 2750 |
| 56 | 35 | 2 | 10 | 300 | 375 | 2.5 | 2750 |
| 57 | 35 | 0 | 15 | 300 | 325 | 2 | 2500 |
| 58 | 35 | 1 | 10 | 250 | 375 | 2 | 2500 |
| 59 | 35 | 0 | 15 | 300 | 425 | 2 | 2500 |
| 60 | 35 | 2 | 20 | 300 | 375 | 1.5 | 2750 |
| 61 | 35 | 1 | 15 | 300 | 375 | 2 | 2750 |
| 62 | 35 | 1 | 15 | 350 | 425 | 2.5 | 2750 |

Table 3.56 Box Behnken Experimental Design for optimization of LC-MS/MS operating conditions (continued).

Table 3.57 Coefficients of model terms for different hormones.

| Coefficients | E1 | E2 | E3 | EE2 | |
|-----------------------|----------|----------|----------|----------|--|
| b ₀ | 172463.6 | 42673.08 | 75588.75 | 26534.69 | |
| b ₁ | 2696.783 | 1496.183 | 1969.335 | 370.2664 | |
| b ₂ | -5943.64 | -3189.39 | -3706 | -2019.15 | |
| b ₃ | 1313.332 | -279.06 | 289.9176 | -98.3677 | |
| b_4 | -20611.1 | -9877.67 | -5215.27 | -4739.28 | |
| b ₅ | -63301.3 | -17206.5 | -27668.8 | -10228 | |
| b ₆ | -1278.89 | -1851.56 | -1267.68 | -787.092 | |
| b ₇ | -10495 | -3949.05 | -5276.8 | -2635.8 | |
| b ₁₂ | 3123.884 | 367.206 | 265.28 | 2527.171 | |
| b ₁₃ | 22051.21 | 4768.905 | 8073.63 | 1524.091 | |
| b ₁₄ | 252.3905 | 386.5508 | 2165.158 | -310.661 | |

| b ₁₅ | 18513.91 | 4094.343 | 6921.138 | 4104.024 |
|-----------------|----------|----------|----------|----------|
| b ₁₆ | -535.769 | 308.2959 | 1576.173 | 526.8978 |
| b ₁₇ | 1921.665 | -704.53 | 3019.263 | 1095.008 |
| b ₂₃ | -324.297 | -813.049 | -2415.97 | -52.0269 |
| b ₂₄ | -4448.24 | -616.791 | -1449.26 | 148.2908 |
| b ₂₅ | 2913.445 | 2146.758 | -722.698 | 1573.113 |
| b ₂₆ | -1160.33 | 1336.474 | 2584.524 | -578.253 |
| b ₂₇ | 2342.146 | 543.0506 | 1860.682 | 1985.744 |
| b ₃₄ | 2240.425 | -129.756 | 725.704 | 407.2529 |
| b ₃₅ | 15702.7 | 5787.002 | 5086.341 | 2979.356 |
| b ₃₆ | -3881.99 | -31.0186 | -297.02 | -1492.05 |
| b ₃₇ | -2076.36 | -723.366 | 363.4076 | 495.9503 |
| b ₄₅ | 12118.37 | 5664.571 | 2492.89 | 2598.758 |
| b ₄₆ | 3311.824 | -1.3249 | 63.20756 | 297.5233 |
| b ₄₇ | 8374.847 | 3739.379 | 2718.584 | 1212.984 |
| b ₅₆ | 1435.664 | 687.1358 | 1705.947 | 1072.538 |
| b ₅₇ | -2806 | 1122.957 | -789.546 | 814.9745 |
| b ₆₇ | 2618.567 | 1278.819 | 430.395 | -779.864 |
| b ₁₁ | 6011.336 | 974.9913 | 3019.214 | 450.7009 |
| b ₂₂ | -971.644 | 854.6614 | -176.116 | 1199.041 |
| b ₃₃ | -93.3027 | 309.9898 | -383.987 | -577.002 |
| b ₄₄ | -13418 | -3054.52 | -5945.89 | -2007.78 |
| b ₅₅ | -64789.2 | -16137.7 | -28368.1 | -10214.5 |
| b ₆₆ | -12216.1 | -2746.48 | -5241.74 | -2774.85 |
| b ₇₇ | -25650.7 | -6714.02 | -12386.7 | -5172.58 |

Table 3.57 Coefficients of model terms for different hormones (continued).

Table 3.58 Variance analysis (ANOVA) of model terms for different hormones.

| | | Prob > F | | | | | | | | |
|---------------------|----------|----------|----------|----------|--|--|--|--|--|--|
| Source of Variation | E1 | E2 | E3 | EE2 | | | | | | |
| Model | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | | | | | | |
| А | 0.4618 | 0.2192 | 0.3137 | 0.6202 | | | | | | |
| В | 0.1118 | 0.0125 | 0.0641 | 0.0111 | | | | | | |
| С | 0.7190 | 0.8162 | 0.8809 | 0.8950 | | | | | | |
| D | < 0.0001 | < 0.0001 | 0.0115 | < 0.0001 | | | | | | |
| E | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | | | | | | |
| F | 0.7260 | 0.1313 | 0.5142 | 0.2961 | | | | | | |
| G | 0.0074 | 0.0026 | 0.0106 | 0.0014 | | | | | | |
| AB | 0.6216 | 0.8598 | 0.9369 | 0.0588 | | | | | | |

| | - | | | |
|----------------|----------|----------|----------|----------|
| AC | 0.0016 | 0.0286 | 0.0222 | 0.2440 |
| AD | 0.9681 | 0.8525 | 0.5200 | 0.8099 |
| AE | 0.0065 | 0.0573 | 0.0471 | 0.0035 |
| AF | 0.9324 | 0.8821 | 0.6389 | 0.6836 |
| AG | 0.7611 | 0.7349 | 0.3715 | 0.3996 |
| BC | 0.9590 | 0.6960 | 0.4733 | 0.9679 |
| BD | 0.4832 | 0.7668 | 0.6661 | 0.9086 |
| BE | 0.6452 | 0.3065 | 0.8294 | 0.2296 |
| BF | 0.8542 | 0.5218 | 0.4433 | 0.6548 |
| BG | 0.7110 | 0.7940 | 0.5800 | 0.1325 |
| CD | 0.7230 | 0.9502 | 0.8287 | 0.7526 |
| CE | 0.0186 | 0.0092 | 0.1376 | 0.0278 |
| CF | 0.5402 | 0.9881 | 0.9294 | 0.2538 |
| CG | 0.7425 | 0.7281 | 0.9137 | 0.7012 |
| DE | 0.0636 | 0.0106 | 0.4595 | 0.0524 |
| DF | 0.6009 | 0.9995 | 0.9850 | 0.8178 |
| DG | 0.1921 | 0.0808 | 0.4203 | 0.3515 |
| EF | 0.8202 | 0.7412 | 0.6117 | 0.4092 |
| EG | 0.6574 | 0.5900 | 0.8139 | 0.5294 |
| FG | 0.6788 | 0.5398 | 0.8979 | 0.5472 |
| A ² | 0.2229 | 0.5437 | 0.2482 | 0.6508 |
| B ² | 0.8416 | 0.5942 | 0.9456 | 0.2341 |
| C^2 | 0.9847 | 0.8464 | 0.8817 | 0.5628 |
| D^2 | 0.0098 | 0.0649 | 0.0281 | 0.0516 |
| E ² | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 |
| F^2 | 0.0175 | 0.0949 | 0.0505 | 0.0091 |
| G2 | < 0.0001 | 0.0003 | < 0.0001 | < 0.0001 |
| Lack of Fit | 0.0212 | 0.0551 | 0.5082 | 0.1522 |

Table 3.58 Variance analysis (ANOVA) of model terms for different hormones (continued).

A-Sheath Gas pressure, B-Ion sweep gas pressure, C-Aux gas pressure, D-Capillary temperature,

E-Vaporizer temperature, F-Collision gas pressure, G-Spray voltage.

Table 3.59 Observed and predicted integration areas of hormones at several experimental conditions.

| | EE2 | | E2 | | E3 | | E1 | | |
|---|----------|-----------|----------|-----------|----------|-----------|----------|-----------|--|
| | Observed | Predicted | Observed | Predicted | Observed | Predicted | Observed | Predicted | |
| 1 | 13588.77 | 11810.39 | 25162.33 | 24259.36 | 47411.46 | 47719.62 | 112476.4 | 109093.1 | |
| 2 | 30343.71 | 31260.73 | 53520.67 | 56020.48 | 74880.79 | 74446.85 | 187925 | 184097.5 | |

| 2 | a (aca a) | | 10000 50 | 44 50 5 50 | | | | 4 49 7 49 9 | |
|----------------|-----------|----------|----------|------------|----------|----------|----------|-------------|--|
| 3 | 24233.51 | 24653.79 | 40832.53 | 41595.58 | 66486.81 | 72049.57 | 157771.2 | 162763.3 | |
| 4 | 24439.69 | 26946.42 | 47506.97 | 50945.74 | 68900.91 | 68373.19 | 166362.3 | 172044.8 | |
| 5 | 12965.73 | 12843.02 | 27712.36 | 28565.82 | 50585.06 | 48300.64 | 129583.8 | 127370.2 | |
| 6 | 26112.1 | 28055.57 | 43691.18 | 48033.68 | 78284.43 | 80348.01 | 162332.9 | 170764.4 | |
| 7 | 17891.08 | 18907.48 | 27059.54 | 31294.61 | 53724.18 | 59952.39 | 127724 | 133927.7 | |
| 8 | 19112.77 | 20447.41 | 37481.69 | 37075.31 | 64106.86 | 61969.92 | 140459.5 | 140843.2 | |
| 9 | 16333.18 | 15273.8 | 22479.6 | 23861.07 | 56766.19 | 54867.3 | 120123.8 | 120440.8 | |
| 10 | 18563.3 | 19354.93 | 35049.38 | 36263.64 | 62234.49 | 64974.67 | 147764.2 | 147906.7 | |
| \mathbb{R}^2 | 0.958713 | | 0.946327 | | 0.938551 | | 0.943031 | | |
| Adeq | | | | | | | | | |
| Precision | 16.72297 | | 13.59588 | 13.59588 | | 13.55452 | | 13.18931 | |

Table 3.59 Observed and predicted integration areas of hormones at several experimental conditions (continued).

Table 3.60 Possible optimized conditions to maximize integration area of hormones.

| | SGP | ISGP | AGP | CT | VT | CGP | SV | | | | |
|----|-------|-------|-------|--------|--------|---------|------|-------|--------|-------|-------|
| SN | (arb) | (arb) | (arb) | (°C) | (°C) | (mTorr) | (V) | EE2 | E1 | E2 | E3 |
| 1 | 32.52 | 0.41 | 16.91 | 253.9 | 351.88 | 1.9 | 2740 | 36838 | 204298 | 58498 | 87257 |
| 2 | 32.13 | 1.23 | 13.18 | 261.72 | 334.75 | 2.04 | 2650 | 36429 | 226297 | 62043 | 94747 |
| 3 | 33.52 | 1.15 | 11.25 | 252.28 | 336.1 | 1.65 | 2612 | 36345 | 220982 | 66104 | 91498 |
| 4 | 32.05 | 1.03 | 10.02 | 268.51 | 344.17 | 2.5 | 2589 | 35818 | 229343 | 59933 | 93251 |

The model equation can be used to evaluate variation of response with different factors. For three factors, it is necessary to keep one of the factors at constant value to be able plot 3D surface plots. In this case there are 7 factors and numerous numbers of plots can be obtained. In order to keep the process simple, only variation of integration area of hormones with ISGP and SGP were plotted. The other factors were kept constant at the optimized values. Figure 3.49 depicts the integration area of E1 for different values of ISGP and SGP. SGP has got more significant effect than ISGP on the response. The response significantly increases from around 180000 to over 210000 when SGP was decreased from SGP= 38 arb to SGP= 32 arb for ISGP between 0 arb and 2 arb. However, response varies around 170000 or 210000 for different ISGP at SGP= 38 arb and SGP= 32 arb, respectively. Almost the same effects of these factors can be obtained when ISGP was decreased from 2 arb to 0 arb for any values of SGPs. But, decreasing SGP provides a substantial increase in the response.

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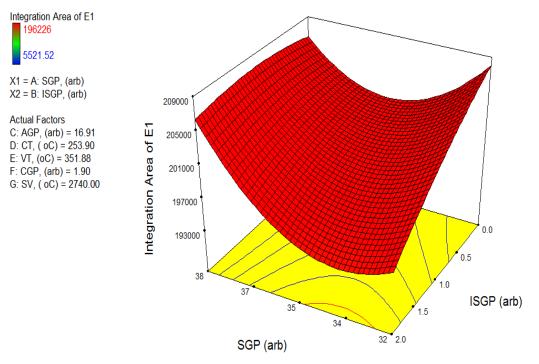


Figure 3.49 Surface plot of integration area of E1 at optimized condition (solution 1).

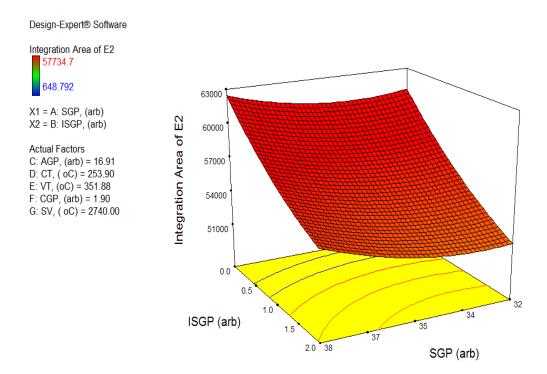


Figure 3.50 Surface plot of integration area of E2 at optimized condition (solution1).

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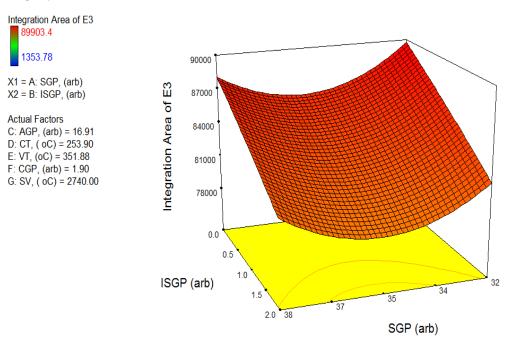


Figure 3.51 Surface plot of integration area of E3 at optimized condition (solution 1).

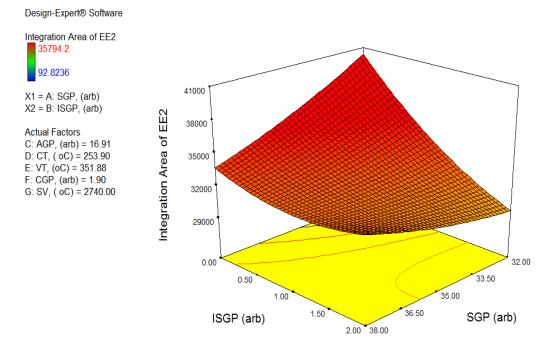


Figure 3.52 Surface plot of integration area of EE2 at optimized condition (solution 1).

The results were quite different for EE2. ISGP resulted in more significant effect on EE2 integration area than that of SGP. But, the interaction between factors was substantial as well, especially at low values of factors. The highest response area was obtained as 40000 when SGP= 32 arb and ISGP= 0. However, it was around 30000 at SGP= 38 arb and ISGP= 2 arb. Table 3.61 depicts that verification point of Box-Behnken design and figure 3.53 depicts that chromatogram of prediction point of 3.

| Dum | SGP | ISGP | AGP | CT | VT | CGP | SV | Area (EE2) |
|--------------|-------|-------|-------|------|------|---------|------|---------------------------|
| Run | (arb) | (arb) | (arb) | (°C) | (°C) | (mTorr) | (V) | Predicted / Observed |
| prediction-1 | 38 | 1.5 | 12 | 325 | 350 | 1.5 | 2750 | 20375/ 22623 |
| prediction-2 | 34 | 0.5 | 19 | 340 | 400 | 2.2 | 3000 | 4941/ 3769 |
| prediction-3 | 33 | 0.4 | 17 | 254 | 352 | 1.9 | 2740 | 38023/ <mark>39840</mark> |

Table 3.61 Verification studies for Box-Behnken design.

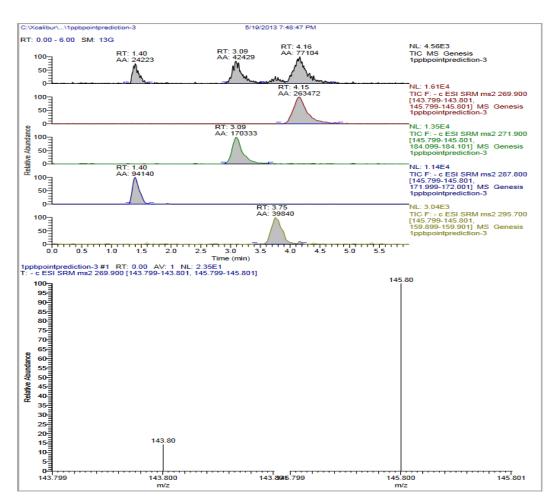


Figure 3.53 Depicts that chromatogram of verification point of 3.

3.6 Calibration Curve Studies

Calibration curves were constructed and shown in Figure 3.54(E1 and E2) and Figure 3.55 (E3 and EE2). Concentration ranges were fixed at 5 ng/L - 30 ng/L for E1, 75 ng/L - 1000 ng/L for E2, 10 ng/L - 75 ng/L for E3 and 75 ng/L - 250 ng/L for EE2. Regression coefficients were determined and these values are greater than acceptable value (0.97). This result indicated that there are linear relationship between concentrations and responses.

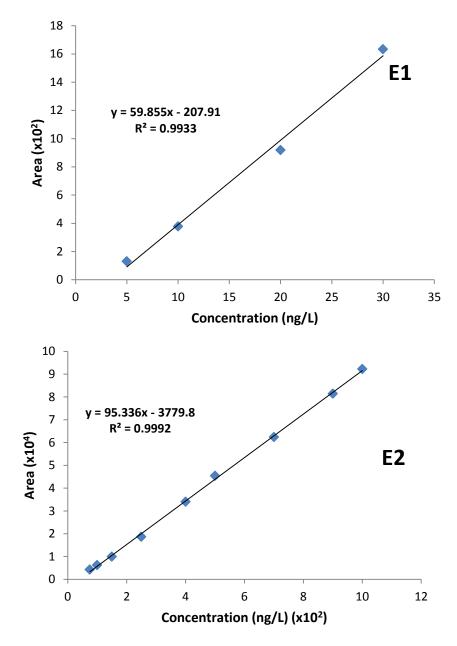


Figure 3.54 Calibration curves of E1 and E2.

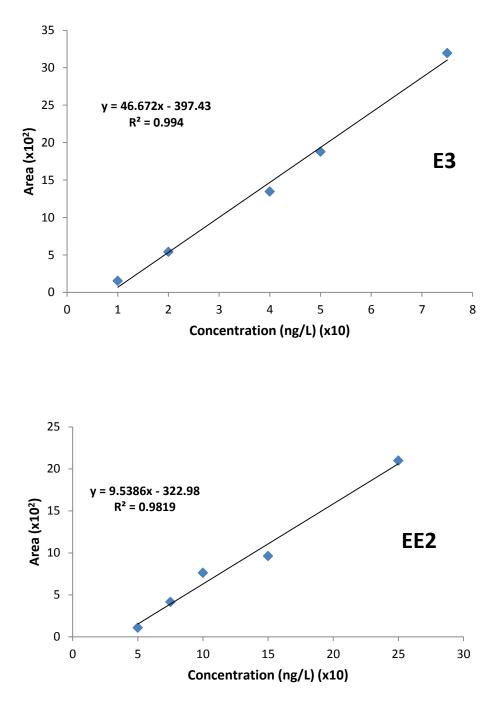


Figure 3.55 Calibration curves of E3 and EE2.

CHAPTER FOUR CONCLUSIONS

Biological development of human being depends on closely related hormones reactions in the body. The interferences in hormone secretion and functions by different factors will lead to abnormalities in metabolism, reproduction and morphology of organisms. One of these factors is the chemicals called as Endocrine Disrupting Chemical (EDC). EDC's can exist in water, air, soil and wastes. They are one of the important environmental pollutants which extremely threaten the normal development of plants, animals and human being. The EDC's in domestic wastewater and generated by waste incineration, agricultural and industrial activities can be taken into the body through breathing, food chain and ingestion of water. These disruptors are perceived by the body as genuine hormones because they elicit the same chemical reactions as natural hormones, prevent naturally occurring hormones from affecting cells in the usual way by blocking the cell receptors; elicit unusual or abnormal reactions in cells. The synthetic EDCs are persistent, toxic and bio accumulative substances (persistent organic pollutants (POPs). Pesticides (aldrin, dieldrin, endrin, heptachlor etc), industrial chemicals (PCBs) and others chemicals such as dioxin, furan and PAH are within the group of synthetic EDC. The natural EDCs are known as estrogenic hormones as E1, E2, E3 and EE2 are generated by through body function of human or consumption of estrogen hormone for birth control. The existence of synthetic or natural ECDs chemical in air, soil and water has been detected and some adverse effects of them on the organisms even at nano gram level have been reported. Development of methods for measurement of very low concentration in water, wastewater and even in soil will be very helpful to advance the knowledge about their adverse health effect on human and animals. Moreover, it will also be helpful for the establishment of national or international control standards of these chemicals.

By considering these facts, the thesis aimed to develop an instrumental method for the measurement of estrogenic hormones as E1, E2, E3 and EE2 in LC-MS/MS. The pre-optimization of mobile phase, injection solution compositions and flow for peak symmetry and resolution factor by using central composite design was conducted as initial stage of thesis. The optimized conditions were determined as % ACN_m= 40, %ACN_s= 25 and flow= 300 μ L/min. The peak symmetry was at acceptable level around PS=1 but resolution factors were low around 0.6 to 1.7 depending on the hormone type. Low RF could have caused insufficient separation of peaks. In addition, integration area under these conditions were low as well. Ionization of hormones needed improvement. Alkaline addition as NH₄OH significantly improved integration area. Alkaline media support to increase ionization rate of hormones, because acidity constant of target analytes (pK_a) are around 10. This means that increasing alkalinity will have positive effect on ionization. The effect of %NH₄OH on ionization was studied between 0 to 17 %. Statistical analysis of results indicated that 3% NH₄OH was the optimum concentration to get highest integration area for all hormones.

The optimization studies should be carried out for narrow ranges of significant factors. There are 10 different LC-MS/MS running factors that could affect integration area of analyte. Factor selection was conducted by Single Factor Experimental Design method. The significant factors were sheath gas pressure, spray voltage, vaporizer temperature, cone position and collision gas pressure. On the other hand, capillary temperature, ion sweep gas pressure and aux gas pressure did not significantly affect the response area of all hormones. The pre-selected running conditions were SGP= 35 arb, SV= 2750 V, VT= 375 °C, cone position= D, CGP= 2 arb for significant factors. The maximum integration area achieved for E1 and E3, for example, by this experimental study were around A= 45000 and A= 18000, respectively.

Optimization of elution conditions for the new mobile phase with NH₄OH and pre-selected running conditions resulted in a substantial improvement in resolution factor although peak symmetry was at acceptable level. The final elution conditions were determined as % ACN_s= 28, % ACN_m=44, Flow=136.9 μ L/min with corresponding RF values of hormones as E3=3.76, E2=1.25, EE2= 0.58. The most substantial improvement was achieved between E1 and E3. In addition EE2

separation in the chromatogram was sufficient compared to the pre-optimization studies. Total instrumental analysis time was achieved as 5 minutes by this second optimization.

MS/MS conditions were further optimized using response surface method. The interface conditions were determined as sheath gas= 33 arb, ion sweep gas= 0.4 arb, aux gas pressure= 17 arb, capillary temperature= 254 °C, vaporizer temperature= 352 °C, collision gas= 1.9 mTorr, spray voltage= 2740 V and cone position set at D. Substantial improvement in integration areas of hormones were achieved by this final optimization. The area for E1 and E3 increased up to E1= 200000 and for E3= 85000.

Calibration studies were performed and regression values coefficients were obtained at around 0.98 - 0.99. Linear range of calibration curve developed at the optimal conditions. It was revealed that even 1.6 ng/L of E1, 49 ng/L of E2, 3.2 ng/L of E3 and 23.2 ng/L of EE2 can be detected by the developed optimized conditions.

The measurement of these hormones still needs further studies as given below,

- Method development about preconcentration and purification techniques for measuring hormone concentrations, e.g., in wastewater, surface water and drinking water can be conducted. This study is being carried out by MSc. student Can Aftafa from Chemistry Department of EGE University.
- The method can be applied to water, wastewater and drinking water to investigate the matrix effect.
- Hormones are transformed to their conjugates through biochemical reactions in the body or in the water. Methods for the measurement of conjugates can be developed.
- Biological treatment of these hormones, process optimization and determination of alteration products after treatment can be studied.

- The concentrations of these hormones and their conjugates in the surface waters or in the effluent of domestic wastewater treatment plant can be monitored.
- The lowest concentration of hormones that could cause shift in the population from male to female of an aquatic animal can be investigated.

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APPENDICES

| Replicate Number | | % NH ₄ OH Concentration in Mobile Phase (200mM) | | | | | | | |
|---------------------|----------|--|----------|----------|----------|----------|----------|--|--|
| | 0 | 3 | 5 | 7 | 10 | 15 | 17 | | |
| 1 | 464999 | 757254 | 939542 | 742302 | 726983 | 710048 | 741178 | | |
| 2 | 378566 | 935188 | 435712 | 745196 | 729584 | 710533 | 744770 | | |
| 3 | 281782 | 682782 | 1028236 | 788230 | 767019 | 624417 | 716172 | | |
| 4 | 330897 | 690926 | 707873 | 768337 | 744723 | 611596 | 551245 | | |
| 5 | 372140 | 833536 | 1030780 | 747322 | 739401 | 642404 | 468470 | | |
| 6 | 381325 | 944411 | 1034792 | 757614 | 754575 | 660802 | 379633 | | |
| 7 | 378720 | 862915 | 1012192 | 756179 | 745538 | 699565 | 404157 | | |
| 8 | 410189 | 942813 | 1017491 | 749613 | 754882 | 710710 | | | |
| 9 | 409581 | 903930 | 732459 | 766516 | 753804 | 740855 | | | |
| 10 | 288265 | 850704 | 579708 | 745091 | 739183 | 722992 | | | |
| Mean | 369647 | 840446 | 851879 | 756640 | 745569 | 671259 | 572232 | | |
| n | 10 | 10 | 10 | 10 | 10 | 10 | 7 | | |
| SD | 56253.13 | 99491.41 | 221019.6 | 14296.66 | 12365.96 | 41576.93 | 161028.8 | | |

Table 1 Variation of integration area of E1 with NH₄OH concentration in mobile phase.

| Table 2 LSD Comparison test for the different levels of NH ₄ OH concentration on integration | 1 area of |
|---|-----------|
| E1. | |

| Levels | $(\overline{Y}_i - \overline{Y}_j) t_{calculated}$ | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ | |
|---|--|----------------------------|--------------------------------|--|
| LSD test for comparing 0% NH ₄ O | H with the other levels | | | |
| 0%-3% | -470799 | 98938 | Significant | |
| 0%-5% | -482232 | 98938 | Significant | |
| 0%-7% | -386993 | 98938 | Significant | |
| %0-%10 | -375923 | 98938 | Significant | |
| %0-%15 | -301613 | 98938 | Significant | |
| %0-%17 | -202585 | 109025 | Significant | |
| LSD test for comparing 3% NH ₄ O | H with the other levels | | | |
| %3-%5 | -11433 | 98938 | Insignificant | |
| %3-%7 | 83806 | 98938 | Insignificant | |
| %3-%10 | 94877 | 98938 | Insignificant | |
| %3-%15 | 169186 | 98938 | Significant | |
| %3-%17 | 268214 | 109025 | Significant | |
| LSD test for comparing 5% NH ₄ O | H with the other levels | | | |
| %5-%7 | 95239 | 98938 | Insignificant | |
| %5-%10 | 106309 | 98938 | Significant | |
| %5-%15 | 180619 | 98938 | Significant | |
| %5-%17 | 279647 | 109025 | Significant | |
| LSD test for comparing 7% NH ₄ O | H with the other levels | · | | |
| %7-%10 | 11071 | 98938 | Insignificant | |
| %7-%15 | 85381 | 98938 | Insignificant | |
| %7-%17 | 184408 | 109025 | Significant | |
| LSD test for comparing 10% NH40 | DH with the other levels | · | | |
| %10-%15 | 74310 | 98938 | Insignificant | |
| %10-%17 | 173337 | 109025 | Significant | |
| LSD test for comparing 15% NH40 | DH with the other levels | | | |
| %15-%17 | 99027 | 109025 | Insignificant | |

*If $|t_{calculated}| > t_{critic}$, The difference between the means of the levels is significant.

| Replicate Number | | 9 | 6 NH4OH Conce | ntration in Mobile | e Phase (200mM) | | |
|---------------------|------------|------------|---------------|--------------------|-----------------|------------|------------|
| | 0 | 3 | 5 | 7 | 10 | 15 | 17 |
| 1 | 266650.840 | 411942.271 | 414113.979 | 320831.881 | 305505.317 | 307150.116 | 310285.504 |
| 2 | 168255.512 | 307459.444 | | 322877.637 | 317210.249 | 291923.002 | 310463.614 |
| 3 | 118764.560 | 305894.520 | 443356.976 | 334186.291 | 332901.398 | 261892.330 | 302782.276 |
| 4 | 144413.972 | 375774.274 | 321448.457 | 325699.139 | 326141.045 | | 228925.831 |
| 5 | 155605.691 | 420033.011 | 448199.974 | 321537.523 | 311308.957 | 280692.856 | |
| 6 | 162581.663 | 416335.176 | 443136.043 | 326608.944 | 323937.107 | 283792.294 | |
| 7 | 171067.130 | 417939.639 | 435317.324 | 321080.121 | 317943.951 | 288987.180 | |
| 8 | 175158.490 | 426993.897 | 438959.723 | 321607.672 | 316103.617 | 306339.221 | |
| 9 | 172909.606 | 413963.786 | 324212.595 | 324303.991 | 320231.306 | 313115.389 | |
| 10 | 122585.231 | | | 325697.990 | 308831.900 | 306733.123 | |
| Mean | 165799.270 | 388481.780 | 408593.134 | 324443.119 | 318011.485 | 288682.428 | 288114.306 |
| n | 10 | 9 | 8 | 10 | 10 | 9 | 4 |
| SD | 40817.051 | 48565.320 | 53919.915 | 4028.725 | 8284.653 | 15646.448 | 39621.032 |

Table 3 Variation of integration area of E2 with NH₄OH concentration in mobile phase.

Table 4 LSD Comparison test for the different levels of NH_4OH concentration on integration area of E2.

| Levels | $(\overline{Y}_i - \overline{Y}_j)$ $t_{calculated}$ | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
|---|---|----------------------------|--------------------------------|
| LSD test for comparing 0% NH4OF | I with the other levels | | |
| 0%-3% | -222682.510 | 42002.743 | Significant |
| | | | 0 |
| 0%-5% | -242793.864 | 43362.405 | Significant |
| 0%-7% | -158643.849 | 30674.075 | Significant |
| %0-%10 | -152212.215 | 30674.075 | Significant |
| %0-%15 | -122883.159 | 42002.743 | Significant |
| %0-%17 | -122315.037 | 54082.421 | Significant |
| LSD test for comparing 3% NH ₄ OH with | h the other levels | | |
| %3-%5 | -20111.354 | 33328.418 | Insignificant |
| %3-%7 | 64038.661 | 42002.743 | Significant |
| %3-%10 | 70470.295 | 42002.743 | Significant |
| %3-%15 | 99799.352 | 32333.315 | Significant |
| %3-%17 | 100367.473 | 41217.050 | Significant |
| LSD test for comparing 5% NH4OH with | h the other levels | | L |
| %5-%7 | 84150.015 | 43362.405 | Significant |
| %5-%10 | 90581.649 | 43362.405 | Significant |
| %5-%15 | 119910.706 | 33328.418 | Significant |
| %5-%17 | 120478.828 | 54934.165 | Significant |
| LSD test for comparing 7% NH4OH with | n the other levels | | 1 |
| %7-%10 | 6431.634 | 30674.075 | Insignificant |
| %7-%15 | 35760.691 | 42002.743 | Insignificant |
| %7-%17 | 36328.813 | 54082.421 | Insignificant |
| LSD test for comparing 10% NH ₄ OH wi | th the other levels | 1 | 1 |
| %10-%15 | 29329.056 | 42002.743 | Insignificant |
| %10-%17 | 29897.178 | 54082.421 | Insignificant |
| LSD test for comparing 15% NH ₄ OH wi | th the other levels | 1 | 1 |
| %15-%17 | 568.122 | 41217.050 | Insignificant |
| | | | |

| Replicate Number | | (| % NH4OH Conc | entration in Mob | ile Phase (200m) | M) | |
|---------------------|--------|--------|--------------|------------------|------------------|--------|--------|
| | 0 | 3 | 5 | 7 | 10 | 15 | 17 |
| 1 | 250281 | 317984 | 347125 | 272197 | 257338 | 263263 | 270264 |
| 2 | 151572 | 255561 | 158297 | 273394 | 284495 | 264940 | 281593 |
| 3 | 107319 | 240930 | 380690 | 290793 | 283600 | 243928 | 260871 |
| 4 | 121330 | 292819 | 273567 | 279695 | 274287 | 238106 | 204341 |
| 5 | 138499 | 330085 | 362274 | 272469 | 274123 | 251780 | 180364 |
| 6 | 145962 | 327532 | 376062 | 281617 | 280401 | 261800 | 141514 |
| 7 | 148170 | 338619 | 359806 | 270016 | 264525 | 251574 | 156592 |
| 8 | 159472 | 329155 | 369843 | 274102 | 268919 | 272591 | |
| 9 | 159759 | 319720 | 280067 | 279617 | 273481 | 274747 | |
| 10 | 109762 | | 213984 | 279851 | 265972 | 264484 | |
| Mean | 149213 | 305823 | 312171 | 277375 | 272714 | 255998 | 213648 |
| n | 10 | 9 | 10 | 10 | 10 | 10 | 7 |
| SD | 40349 | 35227 | 77419 | 6202 | 8723 | 11618 | 57307 |

Table 5 Variation of integration area of E3 with NH₄OH concentration in mobile phase.

Table 6 LSD Comparison test for the different levels of NH_4OH concentration on integration area of E3.

| Levels | $(\overline{Y}_i - \overline{Y}_j)$ $t_{calculated}$ | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
|---|---|----------------------------|--------------------------------|
| LSD test for comparing 0% NH4OH with the oth | ner levels | | |
| 0%-3% | -156610 | 37956 | Significant |
| 0%-5% | -162959 | 36944 | Significant |
| 0%-7% | -128162 | 36944 | Significant |
| %0-%10 | -123502 | 36944 | Significant |
| %0-%15 | -106785 | 36944 | Significant |
| %0-%17 | -64436 | 40710 | Significant |
| LSD test for comparing 3% NH4OH with the oth | ner levels | L. | I |
| %3-%5 | -6349 | 37956 | Insignificant |
| %3-%7 | 28448 | 37956 | Insignificant |
| %3-%10 | 33109 | 37956 | Insignificant |
| %3-%15 | 49825 | 37956 | Significant |
| %3-%17 | 92175 | 41631 | Significant |
| LSD test for comparing 5% NH_4OH with the other | ner levels | I. | L |
| %5-%7 | 34796 | 36944 | Insignificant |
| %5-%10 | 39457 | 36944 | Significant |
| %5-%15 | 56174 | 36944 | Significant |
| %5-%17 | 98523 | 40710 | Significant |
| LSD test for comparing 7% $\rm NH_4OH$ with the other than the other than the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of the test of t | ner levels | | |
| %7-%10 | 4661 | 36944 | Insignificant |
| %7-%15 | 21377 | 36944 | Insignificant |
| %7-%17 | 63727 | 40710 | Significant |
| LSD test for comparing 10% NH ₄ OH with the o | ther levels | | 1 |
| %10-%15 | 16716 | 36944 | Insignificant |
| %10-%17 | 59066 | 40710 | Significant |
| LSD test for comparing 15% $\rm NH_4OH$ with the o | ther levels | | 1 |
| %15-%17 | 42349 | 40710 | Significant |

| Replicate Number | | (| % NH4OH Conc | entration in Mob | ile Phase (200m | M) | |
|---------------------|----------|----------|--------------|------------------|-----------------|----------|----------|
| | 0 | 3 | 5 | 7 | 10 | 15 | 17 |
| 1 | 73813 | 104960 | 142431 | 106881 | 99606 | 104318 | 112743 |
| 2 | 52407 | 134386 | 55029 | 103299 | 103731 | 107809 | 104133 |
| 3 | 37542 | 105472 | 151069 | 111530 | 108315 | 90161 | 99297 |
| 4 | 46319 | 99793 | 105304 | 106455 | 106735 | 89838 | 82633 |
| 5 | 49863 | 121360 | 144908 | 106691 | 102667 | 90614 | 62811 |
| 6 | 53093 | 136748 | 145557 | 110556 | 101796 | 100766 | 52055 |
| 7 | 55107 | 137495 | 143760 | 107513 | 106153 | 99696 | 58714 |
| 8 | 55587 | 137349 | 149070 | 102847 | 106536 | 106394 | |
| 9 | 53071 | 144934 | 102924 | 104537 | 109605 | 113022 | |
| 10 | 39757 | 140571 | 74080 | 104209 | 104427 | 109372 | |
| Mean | 51656 | 124722 | 121413 | 106452 | 104957 | 98699 | 81769 |
| n | 10 | 10 | 10 | 10 | 10 | 10 | 7 |
| SD | 9974.542 | 17186,64 | 34911,07 | 2898,947 | 3084,494 | 7519,808 | 24294,64 |

Table 7 Variation of integration area of EE2 with NH₄OH concentration in mobile phase.

Table 8 LSD Comparison test for the different levels of NH_4OH concentration on integration area of EE2.

| Levels | $(\overline{Y}_i - \overline{Y}_j)$ $t_{calculated}$ | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
|--|---|----------------------------|--------------------------------|
| LSD test for comparing 0% NH4OH v | with the other levels | | 1 |
| 0%-3% | -73066 | 15836 | Significant |
| 0%-5% | -69757 | 15836 | Significant |
| 0%-7% | -54796 | 15836 | Significant |
| %0-%10 | -53301 | 15836 | Significant |
| %0-%15 | -47043 | 15836 | Significant |
| %0-%17 | -30113 | 17451 | Significant |
| LSD test for comparing 3% NH ₄ OH v | with the other levels | | |
| %3-%5 | 3308 | 15836 | Insignificant |
| %3-%7 | 18270 | 15836 | Significant |
| %3-%10 | 19765 | 15836 | Significant |
| %3-%15 | 26023 | 15836 | Significant |
| %3-%17 | 42952 | 17451 | Significant |
| LSD test for comparing 5% NH ₄ OH v | with the other levels | 1 | L |
| %5-%7 | 14962 | 15836 | Insignificant |
| %5-%10 | 16456 | 15836 | Significant |
| %5-%15 | 22714 | 15836 | Significant |
| %5-%17 | 39644 | 17451 | Significant |
| LSD test for comparing 7% NH ₄ OH v | with the other levels | | |
| %7-%10 | 1495 | 15836 | Insignificant |
| %7-%15 | 7753 | 15836 | Insignificant |
| %7-%17 | 24682 | 17451 | Significant |
| LSD test for comparing 10% NH4OH | with the other levels | • | • |
| %10-%15 | 6258 | 15836 | Insignificant |
| %10-%17 | 23188 | 17451 | Significant |
| LSD test for comparing 15% NH ₄ OH | with the other levels | | 1 |
| %15-%17 | 16930 | 17451 | Insignificant |

| | El | | | E2 | | | E3 | | | EE2 | | |
|-----------|----------------------|----------|----------|----------------------|-----------|----------|----------------------|-----------|-----------|----------------------|-----------|-----------|
| Number of | Levels of Sheath Gas | ath Gas | | Levels of Sheath Gas | th Gas | | Levels of Sheath Gas | h Gas | | Levels of Sheath Gas | eath Gas | |
| Replicate | sg -30 | sg-35 | sg-40 | sg -30 | sg-35 | sg-40 | sg -30 | sg-35 | sg-40 | sg -30 | sg-35 | sg-40 |
| 1 | 14320 | 24833 | 15665 | 2522 | 5772 | 2649 | 11137 | 10187 | 8042 | 1645 | 1690 | 726 |
| 2 | 19279 | 22781 | 12450 | 2357 | 4811 | 2477 | 5601 | 10021 | 5016 | 1405 | 2444 | 916 |
| 3 | 17253 | 25135 | 16633 | 3028 | 5431 | 3016 | 6209 | 9898 | 6768 | 363 | 1620 | 1915 |
| 4 | | 23639 | | | 6969 | | 7106 | 9958 | 5248 | 565 | 2164 | 923 |
| 5 | | | | | | | | | | | | |
| Mean | 16951 | 24097 | 14916 | 2636 | 5746 | 2714 | 7513 | 10016 | 6268 | 994 | 1979 | 1120 |
| u | 3 | 4 | 3 | 3 | 4 | 3 | 4 | 4 | 4 | 4 | 4 | 4 |
| SD | 2493.247 | 1089.474 | 2189.492 | 349.90498 | 907.44842 | 275.4727 | 2493.6437 | 124.44888 | 1415.0393 | 625.4645 | 393.10808 | 537.82612 |
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Table 10 Raw data for the effect of spray voltage on integration area of E1 and E2.

| | E1 | | | | | | | E2 | | | | | | |
|-----------|-----------|-------------------------|---------|---------|---------|---------|---------|-------------|-------------------------|----------|----------|----------|----------|----------|
| Replicate | Levels of | cevels of Spray Voltage | ge | | | | | Levels of S | Levels of Spray Voltage | | | | | |
| number | sv-2000 | sv-2250 | sv-2750 | sv-3000 | sv-3250 | sv-3500 | sv-3750 | sv-2000 | sv-2250 | sv-2750 | sv-3000 | sv-3250 | sv-3500 | sv-3750 |
| 1 | 10062 | 21625 | 25394 | 26250 | 22500 | 12586 | 13713 | 3060 | 3965 | 4961 | 4549 | 6060 | 2456 | 1187 |
| 2 | 14999 | 27366 | 18460 | 28956 | 23110 | 14475 | 10668 | 4389 | 4734 | 4077 | 5679 | 5437 | 3052 | 1325 |
| 3 | 10847 | 15404 | 33758 | 27530 | 22866 | 12282 | 9387 | 3114 | 3189 | 8124 | 4894 | 4217 | 2998 | 3161 |
| 4 | 19360 | 21287 | 33833 | 21096 | 26930 | 17876 | 10164 | 2919 | 5548 | 8690 | 6358 | 4589 | 2963 | 3129 |
| 5 | 16447 | 21595 | 33181 | 17134 | 21102 | 20745 | 10041 | 4032 | 4869 | 8583 | 3609 | 2730 | 4644 | 925 |
| Mean | 14343 | 21455 | 28925 | 24193 | 23302 | 15593 | 10795 | 3503 | 4461 | 6887 | 5018 | 4607 | 3223 | 1946 |
| u | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| SD | 3891.48 | 4231.87 | 6847.46 | 4936.46 | 2172.19 | 3640.27 | 1693.94 | 661.9919 | 906.2476 | 2194.473 | 1054.902 | 1272.302 | 829.8406 | 1104.655 |

| | E3 | | | | | | | EE2 | | | | | | |
|-----------|-------------|-------------------------|---------|---------|---------|---------|---------|-------------|-------------------------|---------|---------|---------|---------|---------|
| Replicate | Levels of 5 | Levels of Spray Voltage | | | | | | Levels of 5 | Levels of Spray Voltage | | | | | |
| number | sv-2000 | sv-2250 | sv-2750 | sv-3000 | sv-3250 | sv-3500 | sv-3750 | sv-2000 | sv-2250 | sv-2750 | sv-3000 | sv-3250 | sv-3500 | sv-3750 |
| | 3654 | 9360 | 10116 | 7070 | 7123 | 5572 | 5543 | 752 | 3344 | 1104 | 1419 | 1706 | 686 | 796 |
| 2 | 2791 | 7640 | 7212 | 9517 | 8606 | 5749 | 5200 | 1333 | 2124 | 1805 | 814 | 1759 | 1421 | 67 |
| 3 | 3502 | 5699 | 10064 | 9037 | 9829 | 5413 | 4137 | 1596 | 2440 | 2669 | 2154 | 2196 | 390 | 1080 |
| 4 | 4722 | 8578 | 12002 | 13989 | 7186 | 6472 | 3271 | 1174 | 1845 | 3159 | 2200 | 784 | 966 | 415 |
| 10 | 4150 | 7041 | 10796 | 5030 | 7581 | 8669 | 3628 | 1009 | 2073 | 1128 | 1611 | 2115 | 2310 | 684 |
| Mean | 3764 | 7664 | 10038 | 8928 | 8065 | 6375 | 4356 | 1173 | 2365 | 1973 | 1640 | 1712 | 1215 | 608 |
| | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| SD | 723.52 | 1410.82 | 1762.57 | 3339.81 | 1151.05 | 1344.54 | 984.61 | 319.88 | 586.96 | 920.23 | 572.21 | 561.43 | 713.41 | 385.06 |

Table 11 Raw data for the effect of spray voltage on integration area of E3 and EE2.

Table 12 Raw data for the effect of vaporizer temperature on integration area of E1 and E2.

| | E1 | | | | | | | | E2 | | | | | | | |
|-----------|-----------|-----------|---------------------------------|--------|--------|--------|--------|--------|--------------|---------------------------------|---------|---------|----------|---------|---------|---------|
| Replicate | Levels of | Vaporizer | Levels of Vaporizer Temperature | e | | | | | Levels of Vi | Levels of Vaporizer Temperature | erature | | | | | |
| number | vt-200 | vt-250 | vt-300 | vt-350 | vt-375 | vt-400 | vt-425 | vt-450 | vt-200 | vt-250 | vt-300 | vt-350 | vt-375 | vt-400 | vt-425 | vt-450 |
| 1 | 18062 | 19526 | 33581 | 32366 | 62048 | 60431 | 35786 | 31495 | 4495.50 | 6624.88 | 4797.43 | 8444.76 | 7123.48 | 4902.16 | 6786.38 | 4860.19 |
| 2 | 22416 | 22770 | 28965 | 32434 | 64086 | 64699 | 35014 | 31850 | 4119.82 | 5035.52 | 4204.16 | 6753.23 | 7519.25 | 7430.91 | 6841.89 | 5030.81 |
| 3 | 19982 | 20104 | 26174 | 32871 | 64747 | 67035 | 31629 | 33825 | 5397.34 | 3164.08 | 5128.32 | 6033.56 | 10278.39 | 7821.64 | 5994.42 | 7851.17 |
| 4 | 17245 | 35181 | 33062 | 35872 | 60649 | 31560 | 36127 | 53237 | 3044.12 | 8213.61 | 6070.81 | 6327.78 | 8966.36 | 8894.19 | 7020.30 | 3508.22 |
| 5 | 19456 | 23524 | 31295 | 33350 | 63428 | 34525 | 35486 | 49463 | 2894.44 | 5348.81 | 6995.19 | 7685.89 | 7701.63 | 9724.43 | 5854.00 | 6817.76 |
| Mean | 19432 | 24221 | 30616 | 33379 | 62992 | 51650 | 34808 | 39974 | 3990.25 | 5677.38 | 5439.18 | 7049.04 | 8317.82 | 7754.66 | 6499.40 | 5613.63 |
| u | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| SD | 1992 | 6358 | 3070 | 1449 | 1647 | 17183 | 1824 | 10508 | 1042.58 | 1881.94 | 1101.58 | 90.06 | 1295.02 | 1831.98 | 534.45 | 1717.31 |

| Replicate | | | | | | | | | | | | | | | | |
|-----------|-----------|---------------------------------|------------|--------|--------|--------|--------|--------|-----------|---------------------------------|------------|--------|--------|--------|--------|--------|
| number | E3 | | | | | | | | EE2 | | | | | | | |
| | Levels of | Levels of Vaporizer Temperature | emperature | | | | | | Levels of | Levels of Vaporizer Temperature | emperature | | | | | |
| | vt-200 | vt-250 | vt-300 | vt-350 | vt-375 | vt-400 | vt-425 | vt-450 | vt-200 | vt-250 | vt-300 | vt-350 | vt-375 | vt-400 | vt-425 | vt-450 |
| 1 | 9191 | 6486 | 11843 | 14625 | 25444 | 25272 | 16938 | 14442 | 1710 | 1653 | 2930 | 2511 | 2680 | 3911 | 3086 | 2578 |
| 2 | 6958 | 8326 | 11433 | 13510 | 26041 | 26723 | 16479 | 11091 | 1226 | 1419 | 3764 | 3711 | 4324 | 2345 | 3103 | 2850 |
| 3 | 5993 | 8548 | 12689 | 14485 | 26632 | 23555 | 16402 | 11386 | 616 | 1898 | 2734 | 3100 | 4233 | 4458 | 2935 | 1611 |
| 4 | 7521 | 11704 | 13526 | 11545 | 22936 | 17634 | 12634 | 20901 | 2147 | 1375 | 4006 | 3228 | 4388 | 2311 | 1872 | 1743 |
| 5 | 5102 | 9208 | 12983 | 14162 | 28431 | 16898 | 16750 | 20814 | 1012 | 1678 | 2173 | 4440 | 4797 | 4020 | 2752 | 1712 |
| Mean | 6953 | 8854 | 12495 | 13665 | 25897 | 22017 | 15841 | 15727 | 1342 | 1605 | 3121 | 3398 | 4084 | 3409 | 2750 | 2099 |
| u | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| SD | 1555 | 1886 | 850 | 1261 | 1997 | 4487 | 1805 | 4864 | 599 | 213 | 755 | 723 | 814 | 1008 | 510 | 572 |
| | | | | | | | | | | | | | | | | |

Table 13 Raw data for the effect of vaporizer temperature on integration area of E3 and EE2.

Table 14 Raw data for the effect of aux gas pressure on integration area of all hormones.

| | El | | | | E2 | | | | E3 | | | | EE2 | | | |
|-----------|--------------------|----------------------------|-------|-------|-----------|----------------------------|----------|-------|-------------|----------------------------|-------|-------|-------------|----------------------------|-------|-------|
| Replicate | Levels of <i>i</i> | Levels of Aux Gas Pressure | ssure | | Levels of | Levels of Aux Gas Pressure | Pressure | | Levels of / | Levels of Aux Gas Pressure | ssure | | Levels of , | Levels of Aux Gas Pressure | ssure | |
| number | ag-5 | ag-10 | ag-15 | ag-20 | ag-5 | ag-10 | ag-15 | ag-20 | ag-5 | ag-10 | ag-15 | ag-20 | ag-5 | ag-10 | ag-15 | ag-20 |
| 1 | 36113 | 34794 | 39657 | 34409 | 6535 | 7218 | 10806 | 10026 | 13638 | 12903 | 14378 | 13486 | 4905 | 2311 | 1852 | 606 |
| 2 | 33844 | 34913 | 38701 | 34280 | 8690 | 7114 | 9213 | 7180 | 15768 | 12661 | 16993 | 19744 | 1843 | 3506 | 3303 | 3967 |
| 3 | 35548 | 29862 | 35905 | 36682 | 7452 | 10269 | 5793 | 10148 | 14748 | 15619 | 15159 | 22962 | 2311 | 2263 | 2731 | 4682 |
| 4 | 33671 | 34684 | 40776 | 33067 | 9289 | 6518 | 6637 | 6392 | 16759 | 14956 | 14262 | 15347 | 4838 | 3236 | 3823 | 1517 |
| 5 | 36332 | 37577 | 33593 | 36667 | 7499 | 8007 | 9125 | 10751 | 13456 | 13873 | 14153 | 14558 | 2172 | 3964 | 3400 | 1452 |
| Mean | 35102 | 34366 | 37727 | 35021 | 7893 | 7825 | 8315 | 8899 | 14874 | 14003 | 14989 | 17219 | 3214 | 3056 | 3022 | 2505 |
| u | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| SD | 1261 | 2792 | 2932 | 1598 | 1093 | 1465 | 2052 | 1968 | 1406 | 1279 | 1188 | 3996 | 1523 | 749 | 761 | 1696 |

| | e. | c.tem 350 | 2049 | 2896 | 3118 | 1497 | | 2390 | 4 | 753 |
|-----|---------------------------------|-----------|-------|-------|-------|-------|---|-------|---|------|
| | Levels of Capillary Temperature | c.tem 325 | 2995 | 1898 | 2912 | 3887 | | 2923 | 4 | 814 |
| EE2 | Levels of Capil | c.tem 300 | 2939 | 4543 | 3236 | 4041 | | 3690 | 4 | 735 |
| | ure | c.tem 350 | 15077 | 12457 | 11122 | 12168 | | 12706 | 4 | 1682 |
| | Levels of Capillary Temperature | c.tem 325 | 14395 | 11623 | 14671 | 13612 | | 13575 | 4 | 1376 |
| E3 | Levels of Cap | c.tem 300 | 14556 | 14243 | 11718 | 22082 | | 15650 | 4 | 4472 |
| | e | c.tem 350 | 4882 | 5707 | 5169 | 5984 | | 5436 | 4 | 500 |
| | Levels of Capillary Temperature | c.tem 325 | 5921 | 6970 | 4994 | 6235 | | 6030 | 4 | 819 |
| E2 | Levels of Capil | c.tem 300 | 5112 | 9318 | 11490 | 9808 | | 8932 | 4 | 2711 |
| | ture | c.tem 350 | 31521 | 29341 | 31577 | 31584 | | 31006 | 4 | 1110 |
| | Levels of Capillary Temperature | c.tem 325 | 34167 | 38582 | 33995 | 32753 | | 34874 | 4 | 2551 |
| El | Levels of Ca _l | c.tem 300 | 35583 | 32600 | 41218 | 53120 | | 40630 | 4 | 9061 |
| | Number of | Replicate | 1 | 2 | 3 | 4 | 5 | Mean | u | SD |

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Table 16 Raw data for the effect of ion sweep gas pressure on integration area of all hormones.

| | EI | | | E2 | | | E3 | | | EE2 | | |
|-----------|------------------------|----------|-------|------------------------|------------|------|------------------------|------------|-------|------------------------|-------------|------|
| | Ion sweep gas pressure | pressure | | Ion sweep gas pressure | s pressure | | Ion sweep gas pressure | s pressure | | Ion sweep gas pressure | ts pressure | |
| Number of | (arb) | | _ | (arb) | | | (arb) | | | (arb) | | |
| Replicate | is-0.5 | is-0 | is-1 | is-0.5 | is-0 | is-1 | is-0.5 | is-0 | is-1 | is-0.5 | is-0 | is-1 |
| 1 | 36871 | 41205 | 38335 | 11352 | 10286 | 8019 | 17059 | 12694 | 13553 | 3936 | 5027 | 3070 |
| 2 | 41203 | 34777 | 39322 | 9936 | 9353 | 9052 | 16420 | 106/1 | 15037 | 3967 | 2997 | 2546 |
| 3 | 37113 | 35299 | 36081 | 9476 | 9142 | 8785 | 16618 | 17238 | 16977 | 3216 | 4658 | 3049 |
| 4 | 38624 | 37866 | 32571 | 7217 | 11189 | 7767 | 12455 | 17969 | 17256 | 3976 | 2999 | 2095 |
| 5 | | | | | | | | | | | | |
| Mean | 38453 | 37287 | 36577 | 9495 | 9992 | 8406 | 15638 | 16450 | 15706 | 3774 | 3920 | 2690 |
| u | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| SD | 1991 | 2941 | 2996 | 1716 | 940 | 611 | 2139 | 2526 | 1742 | 372 | 1075 | 465 |
| | | | | | | | | | | | | |

| B C C C C C C C C C C C C C C C C C C C | C 9550 9938 10888 | B 7494 6842 7821 | D 41380 42701 43994 | | B C C B C C C C C C C C C C C C C C C C |
|---|----------------------------|---------------------------|------------------------------|--------------------------------------|--|
| 12860 9890 | 10368 12651 9624 | | 9550 9938 10888 | 7494 9550 6842 9938 7821 10888 | 41380 7494 9550 42701 6842 9938 43994 7821 10888 |
| | 2651 624 | ~ | 9938 10888 | 6842 9938 7821 10888 2212 0088 | 42701 6842 9938 43994 7821 10888 |
| | 24 | | 10888 | 7821 10888 | 43994 7821 10888 |
| 13288 17327 | | | | | |
| 13568 18340 | 60 | 10451 12309 | | 10451 | 10451 |
| | | | | | |
| 12402 17426 | 11238 | 10207 112 | | 10207 | 7442 10207 |
| 4 | | 4 | 4 4 | 4 4 4 | 4 |
| 1699 626 | 33 | 585 1473 | | 585 | 423 585 |

Table 17 Raw data for the effect of cone position on integration area of all hormones.

Table 18 Raw data for the effect of collision gas pressure (m Torr) on integration area of all hormones.

| | E1 | | | E2 | | | E3 | | | EE2 | | |
|-----------|------------------------|--------|-------|------------------------|--------|-------|------------------------|--------|-------|------------------------|--------|------|
| | Collision gas pressure | essure | | Collision gas pressure | essure | | Collision gas pressure | essure | | Collision gas pressure | essure | |
| Number of | (m Torr) | | | (m Torr) | | | (m Torr) | | | (m Torr) | | |
| Replicate | cg-1 | cg-1.5 | cg-2 | cg-1.5 | cg-1 | cg-2 | cg-1.5 | cg-1 | cg-2 | cg-1.5 | cg-1 | cg-2 |
| 1 | 18184 | 39624 | 43147 | 6246 | 2796 | 10375 | 15501 | 8456 | 17531 | 3246 | 1796 | 4903 |
| 2 | 18054 | 42797 | 43681 | 7225 | 2996 | 9722 | 14093 | 8203 | 16429 | 3913 | 1806 | 1772 |
| 3 | 18006 | 40233 | 40385 | 6449 | 4884 | 9377 | 18651 | 9390 | 18476 | 4793 | 2244 | 3677 |
| 4 | 19786 | 38884 | 39998 | 10828 | 4918 | 9295 | 15351 | 8484 | 14553 | 3959 | 2400 | 3585 |
| 5 | | | | | | | | | | | | |
| Mean | 18507 | 40384 | 41803 | 7687 | 3898 | 9692 | 15899 | 8633 | 16747 | 3978 | 2061 | 3484 |
| n | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| SD | 856 | 1700 | 1880 | 2136 | 1161 | 491 | 1940 | 520 | 1685 | 633 | 307 | 1290 |

| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|--------------|-------------------------------------|----------------------------|--------------------------------|
| $Y_i vs Y_j$ | t _{calculated} | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
| 2000 vs 2250 | -7112 | 5476.7502 | Significant |
| 2000 vs 2750 | -14582 | 5476.7502 | Significant |
| 2000 vs 3000 | -9850 | 5476.7502 | Significant |
| 2000 vs 3250 | -8959 | 5476.7502 | Significant |
| 2000 vs 3500 | -1250 | 5476.7502 | Insignificant |
| 2000 vs 3750 | 3548 | 5476.7502 | Insignificant |
| 2250 vs 2750 | -7470 | 5476.7502 | Significant |
| 2250 vs 3000 | -2738 | 5476.7502 | Insignificant |
| 2250 vs 3250 | -1846 | 5476.7502 | Insignificant |
| 2250 vs 3500 | 5863 | 5476.7502 | Significant |
| 2250 vs 3750 | 10661 | 5476.7502 | Significant |
| 2750 vs 3000 | 4732 | 5476.7502 | Insignificant |
| 2750 vs 3250 | 5624 | 5476.7502 | Significant |
| 2750 vs 3500 | 13332 | 5476.7502 | Significant |
| 2750 vs 3750 | 18131 | 5476.7502 | Significant |
| 3000 vs 3250 | 892 | 5476.7502 | Insignificant |
| 3000 vs 3500 | 8600 | 5476.7502 | Significant |
| 3000 vs 3750 | 13399 | 5476.7502 | Significant |
| 3250 vs 3500 | 7709 | 5476.7502 | Significant |
| 3250 vs 3750 | 12507 | 5476.7502 | Significant |
| 3500 vs 3750 | 4798 | 5476.7502 | Insignificant |
| | | | |

Table 19 Raw data of LSD test for the effect of spray voltage on integration area of E1.

| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|--------------|-------------------------------------|----------------------------|--------------------------------|
| Levels | $t_{calculated}$ | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| 2000 vs 2250 | -958 | 1603 | Insignificant |
| 2000 vs 2750 | -3384 | 1603 | Significant |
| 2000 vs 3000 | -1515 | 1603 | Insignificant |
| 2000 vs 3250 | -1104 | 1603 | Insignificant |
| 2000 vs 3500 | 280 | 1603 | Insignificant |
| 2000 vs 3750 | 1557 | 1603 | Insignificant |
| 2250 vs 2750 | -2426 | 1603 | Significant |
| 2250 vs 3000 | -557 | 1603 | Insignificant |
| 2250 vs 3250 | -146 | 1603 | Insignificant |
| 2250 vs 3500 | 1238 | 1603 | Insignificant |
| 2250 vs 3750 | 2515 | 1603 | Significant |
| 2750 vs 3000 | 1869 | 1603 | Significant |
| 2750 vs 3250 | 2280 | 1603 | Significant |
| 2750 vs 3500 | 3664 | 1603 | Significant |
| 2750 vs 3750 | 4942 | 1603 | Significant |
| 3000 vs 3250 | 411 | 1603 | Insignificant |
| 3000 vs 3500 | 1795 | 1603 | Significant |
| 3000 vs 3750 | 3072 | 1603 | Significant |
| 3250 vs 3500 | 1384 | 1603 | Insignificant |
| 3250 vs 3750 | 2661 | 1603 | Significant |
| 3500 vs 3750 | 1277 | 1603 | Insignificant |

| Table 20 Raw data | CIOD (| C = 1 | | | |
|---|-------------|----------------|------------------|----------------|-------------------|
| \mathbf{I} and \mathbf{I} \mathbf{I} \mathbf{K} aw data | OT L NUTEST | tor the effect | of shray voltage | On integration | area or E7 |
| 1000 20 100 uuu | | 101 the chieve | or spray vonage | on mogration | $arca or L_{2}$. |
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| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|--------------|-------------------------------------|----------------------------|--------------------------------|
| Levels | t _{calculated} | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| 2000 vs 2250 | -3900 | 2237 | Significant |
| 2000 vs 2750 | -6274 | 2237 | Significant |
| 2000 vs 3000 | -5165 | 2237 | Significant |
| 2000 vs 3250 | -4301 | 2237 | Significant |
| 2000 vs 3500 | -2611 | 2237 | Significant |
| 2000 vs 3750 | -592 | 2237 | Insignificant |
| 2250 vs 2750 | -2374 | 2237 | Significant |
| 2250 vs 3000 | -1265 | 2237 | Insignificant |
| 2250 vs 3250 | -401 | 2237 | Insignificant |
| 2250 vs 3500 | 1288 | 2237 | Insignificant |
| 2250 vs 3750 | 3308 | 2237 | Significant |
| 2750 vs 3000 | 1109 | 2237 | Insignificant |
| 2750 vs 3250 | 1973 | 2237 | Insignificant |
| 2750 vs 3500 | 3663 | 2237 | Significant |
| 2750 vs 3750 | 5682 | 2237 | Significant |
| 3000 vs 3250 | 864 | 2237 | Insignificant |
| 3000 vs 3500 | 2553 | 2237 | Significant |
| 3000 vs 3750 | 4573 | 2237 | Significant |
| 3250 vs 3500 | 1690 | 2237 | Insignificant |
| 3250 vs 3750 | 3709 | 2237 | Significant |
| 3500 vs 3750 | 2019 | 2237 | Insignificant |

Table 21 Raw data of LSD test for the effect of spray voltage on integration area of E3.

Source vs 3/5020192237Insignificant*If $|t_{calculated}| > t_{critic}$, The difference between the means of the levels is significant.

| | T = | | |
|--------------|-------------------------------------|----------------------------|--------------------------------|
| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
| Levels | t _{calculated} | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| 2000 vs 2250 | -1193 | 788 | Significant |
| 2000 vs 2750 | -800 | 788 | Significant |
| 2000 vs 3000 | -467 | 788 | Insignificant |
| 2000 vs 3250 | -539 | 788 | Insignificant |
| 2000 vs 3500 | -43 | 788 | Insignificant |
| 2000 vs 3750 | 564 | 788 | Insignificant |
| 2250 vs 2750 | 392 | 788 | Insignificant |
| 2250 vs 3000 | 726 | 788 | Insignificant |
| 2250 vs 3250 | 653 | 788 | Insignificant |
| 2250 vs 3500 | 1150 | 788 | Significant |
| 2250 vs 3750 | 1757 | 788 | Significant |
| 2750 vs 3000 | 333 | 788 | Insignificant |
| 2750 vs 3250 | 261 | 788 | Insignificant |
| 2750 vs 3500 | 758 | 788 | Insignificant |
| 2750 vs 3750 | 1365 | 788 | Significant |
| 3000 vs 3250 | -72 | 788 | Insignificant |
| 3000 vs 3500 | 424 | 788 | Insignificant |
| 3000 vs 3750 | 1031 | 788 | Significant |
| 3250 vs 3500 | 497 | 788 | Insignificant |
| 3250 vs 3750 | 1104 | 788 | Significant |
| 3500 vs 3750 | 607 | 788 | Insignificant |

| Table 22 Raw data of LS | D test for the effect of | of sprav voltage on | integration area of EE2. |
|-------------------------|--------------------------|---------------------|--------------------------|
| | | | |

3500 vs 3750607788Insignificant*If $|t_{calculated}| > t_{critic}$, The difference between the means of the levels is significant.

| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|-------------|-------------------------------------|----------------------------|--------------------------------|
| Levels | t _{calculated} | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
| 200 vs 250 | -4789 | 9853 | Insignificant |
| 200 vs 300 | -11183 | 9853 | Significant |
| 200 vs 350 | -13946 | 9853 | Significant |
| 200 vs 375 | -43559 | 9853 | Significant |
| 200 vs 400 | -32218 | 9853 | Significant |
| 200 vs 425 | -15376 | 9853 | Significant |
| 200 vs 450 | -20542 | 9853 | Significant |
| 250 vs 300 | -6395 | 9853 | Insignificant |
| 250 vs 350 | -9158 | 9853 | Insignificant |
| 250 vs 375. | -38771 | 9853 | Significant |
| 250 vs 400 | -27429 | 9853 | Significant |
| 250 vs 425 | -10587 | 9853 | Significant |
| 250 vs 450 | -15753 | 9853 | Significant |
| 300 vs 350 | -2763 | 9853 | Insignificant |
| 300 vs 375 | -32376 | 9853 | Significant |
| 300 vs 400 | -21035 | 9853 | Significant |
| 300 vs 425 | -4193 | 9853 | Insignificant |
| 300 vs 450 | -9359 | 9853 | Insignificant |
| 350 vs 375 | -29613 | 9853 | Significant |
| 350 vs 400 | -18271 | 9853 | Significant |
| 350 vs 425 | -1430 | 9853 | Insignificant |
| 350 vs 450 | -6595 | 9853 | Insignificant |
| 375 vs 400 | 11342 | 9853 | Significant |
| 375 vs 425 | 28183 | 9853 | Significant |
| 375 vs 450 | 23018 | 9853 | Significant |
| 400 vs 425 | 16842 | 9853 | Significant |
| 400 vs 450 | 11676 | 9853 | Significant |
| 425 vs 450 | -5166 | 9853 | Insignificant |

Table 23 Raw data of LSD test for the vaporizer temperature on integration area of E1.

| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|-------------|-------------------------------------|----------------------------|--------------------------------|
| Levels | $t_{calculated}$ | t _{critic} (α.05) | $t_{calulated} > t_{critic} *$ |
| 200 vs 250 | -1687.13 | 1771.15 | Insignificant |
| 200 vs 300 | -1448.93 | 1771.15 | Insignificant |
| 200 vs 350 | -3058.80 | 1771.15 | Significant |
| 200 vs 375 | -4327.57 | 1771.15 | Significant |
| 200 vs 400 | -3764.42 | 1771.15 | Significant |
| 200 vs 425 | -2509.15 | 1771.15 | Significant |
| 200 vs 450 | -1623.38 | 1771.15 | Insignificant |
| 250 vs 300 | 238.20 | 1771.15 | Insignificant |
| 250 vs 350 | -1371.66 | 1771.15 | Insignificant |
| 250 vs 375. | -2640.44 | 1771.15 | Significant |
| 250 vs 400 | -2077.28 | 1771.15 | Significant |
| 250 vs 425 | -822.02 | 1771.15 | Insignificant |
| 250 vs 450 | 63.75 | 1771.15 | Insignificant |
| 300 vs 350 | -1609.86 | 1771.15 | Insignificant |
| 300 vs 375 | -2878.64 | 1771.15 | Significant |
| 300 vs 400 | -2315.48 | 1771.15 | Significant |
| 300 vs 425 | -1060.22 | 1771.15 | Insignificant |
| 300 vs 450 | -174.45 | 1771.15 | Insignificant |
| 350 vs 375 | -1268.78 | 1771.15 | Insignificant |
| 350 vs 400 | -705.62 | 1771.15 | Insignificant |
| 350 vs 425 | 549.64 | 1771.15 | Insignificant |
| 350 vs 450 | 1435.41 | 1771.15 | Insignificant |
| 375 vs 400 | 563.16 | 1771.15 | Insignificant |
| 375 vs 425 | 1818.42 | 1771.15 | Significant |
| 375 vs 450 | 2704.19 | 1771.15 | Significant |
| 400 vs 425 | 1255.27 | 1771.15 | Insignificant |
| 400 vs 450 | 2141.03 | 1771.15 | Significant |
| 425 vs 450 | 885.77 | 1771.15 | Insignificant |

| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|-------------|-------------------------------------|----------------------------|--------------------------------|
| Levels | t _{calculated} | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| 200 vs 250 | -1901 | 3510 | Insignificant |
| 200 vs 300 | -5542 | 3510 | Significant |
| 200 vs 350 | -6713 | 3510 | Significant |
| 200 vs 375 | -18944 | 3510 | Significant |
| 200 vs 400 | -15064 | 3510 | Significant |
| 200 vs 425 | -8888 | 3510 | Significant |
| 200 vs 450 | -8774 | 3510 | Significant |
| 250 vs 300 | -3641 | 3510 | Significant |
| 250 vs 350 | -4811 | 3510 | Significant |
| 250 vs 375. | -17042 | 3510 | Significant |
| 250 vs 400 | -13162 | 3510 | Significant |
| 250 vs 425 | -6986 | 3510 | Significant |
| 250 vs 450 | -6873 | 3510 | Significant |
| 300 vs 350 | -1171 | 3510 | Significant |
| 300 vs 375 | -13402 | 3510 | Significant |
| 300 vs 400 | -9522 | 3510 | Significant |
| 300 vs 425 | -3346 | 3510 | Insignificant |
| 300 vs 450 | -3232 | 3510 | Insignificant |
| 350 vs 375 | -12231 | 3510 | Significant |
| 350 vs 400 | -8351 | 3510 | Significant |
| 350 vs 425 | -2175 | 3510 | Insignificant |
| 350 vs 450 | -2061 | 3510 | Insignificant |
| 375 vs 400 | 3880 | 3510 | Significant |
| 375 vs 425 | 10056 | 3510 | Significant |
| 375 vs 450 | 10170 | 3510 | Significant |
| 400 vs 425 | 6176 | 3510 | Significant |
| 400 vs 450 | 6290 | 3510 | Significant |
| 425 vs 450 | 114 | 3510 | Insignificant |

Table 25 Raw data of LSD test for the vaporizer temperature on integration area of E3.

| | $(\overline{Y}_i - \overline{Y}_j)$ | | |
|-------------|-------------------------------------|----------------------------|--------------------------------|
| Levels | $t_{calculated}$ | t _{critic (α.05)} | $t_{calulated} > t_{critic} *$ |
| 200 vs 250 | -262 | 884 | Insignificant |
| 200 vs 300 | -1779 | 884 | Significant |
| 200 vs 350 | -2056 | 884 | Significant |
| 200 vs 375 | -2742 | 884 | Significant |
| 200 vs 400 | -2067 | 884 | Significant |
| 200 vs 425 | -1407 | 884 | Significant |
| 200 vs 450 | -757 | 884 | Insignificant |
| 250 vs 300 | -1517 | 884 | Significant |
| 250 vs 350 | -1794 | 884 | Significant |
| 250 vs 375. | -2479 | 884 | Significant |
| 250 vs 400 | -1804 | 884 | Significant |
| 250 vs 425 | -1145 | 884 | Significant |
| 250 vs 450 | -494 | 884 | Insignificant |
| 300 vs 350 | -277 | 884 | Insignificant |
| 300 vs 375 | -963 | 884 | Significant |
| 300 vs 400 | -288 | 884 | Insignificant |
| 300 vs 425 | 372 | 884 | Insignificant |
| 300 vs 450 | 1022 | 884 | Significant |
| 350 vs 375 | -686 | 884 | Insignificant |
| 350 vs 400 | -11 | 884 | Insignificant |
| 350 vs 425 | 649 | 884 | Insignificant |
| 350 vs 450 | 1299 | 884 | Significant |
| 375 vs 400 | 675 | 884 | Insignificant |
| 375 vs 425 | 1335 | 884 | Significant |
| 375 vs 450 | 1985 | 884 | Significant |
| 400 vs 425 | 659 | 884 | Insignificant |
| 400 vs 450 | 1310 | 884 | Significant |
| 425 vs 450 | 651 | 884 | Insignificant |

| Table 76 Pow date of INT | toot tor the yenergor tem | poroture on integration area of HHU |
|-----------------------------|---------------------------|--------------------------------------|
| | | perature on integration area of EE2. |
| Tuelle 20 Hunn dulla of 202 | | perature on megration area of 222 |

^{*}If $|t_{calculated}| > t_{critic}$, The difference between the means of the levels is significant.